

ARROWSTREET Architecture Urban Design Planning

212 Elm Street Somerville MA 02144 617.623.5555 fax:617.625.4646 www.arrowstreet.com

Graphics and Interiors

RJO'CONNELL & ASSOCIATES, INC.

Civil Engineers & Land Planners 80 MONTVALE AVE. PHONE: 781 279 0180 STONEHAM, MA 02180 FAX: 781 279 0173

SHESKEY ARCHITECTS 14 Franklin Street Quincy, MA 02169

Proponent:

Twenty Wayland, LLC 260 Boston Post Road, Suite 9 Wayland, MA 02109

RJOC 06032 Project No: Drawn By: Checked By: CAD/BPD Issue Date: 2 JUNE 2008 Revision: Date: REISSUED FOR SITE 9/29/08 PLAN APPROVAL

Project:

Wayland Town Center

400 Boston Post Road Wayland, Massachusetts

Site Plan II Phase I Site Plan Application

Drawing Title: SUBSURFACE SEWAGE DISPOSAL SYSTEM DETAILS

Drawing Number

SCALE N.T.S.

SHALL INCLUDE BUOYANCY CALCULATIONS.

2. EXCAVATION SHALL BE KEPT DEWATERED UNTIL ALL BACKFILL HAS BEEN PLACED AND COMPACTED.

3. CONTRACTOR SHALL COORDINATE

MANUFACTURER/INSTALLER'S SCOPE OF WORK WITH CONTRACTOR'S SCOPE OF WORK.

4. ALL MACHINERY, EQUIPMENT, PIPING AND WIRING SHALL BE SECURED IN PLACE.

#### MEDIA TANK VENT

1. IF THE MEDIA TANK IS COVERED, VENT TO ATMOSPHERE THROUGH THE TANK COVER. DO NOT VENT THROUGH THE SIDE OF THE TANK.
2. DO NOT COMBINE THE MEDIA TANK VENT WITH ANY OTHER VENT. (EXCEPT RECYCLE AIRLIFT VENT)
3. MANWAYS, HATCHES AND OTHER PENETRATIONS ABOVE THE WATERLINE SHALL BE DESIGNED TO SEAL AGAINST A MAXIMUM VENT BACKPRESSURE OF 3"

4. VENTED AIR IS WARMER THAN SURROUNDING AIR

AND WILL TEND TO RISE. LOCATE VENT TERMINATION HIGH RATHER THAN LOW.

5. VENT TERMINATION SHALL BE NOT LESS THAN 10' FROM ANY WALKWAY, DOOR, WINDOW, VENTILATION AIR INLET OR POTENTIAL SOURCE OF IGNITION.

6. DO NOT EMPLOY A FLAME SCREEN AT THE VENT TERMINATION. IT WILL PLUG WITH LINT AND REQUIRE REGULAR MAINTENANCE.

7. HORIZONTAL OFFSETS IN THE VENT PIPE SHALL SLOPE UP AND AWAY FROM THE MEDIA TANK AT NOT LESS THAN 1/4" PER FOOT, SO THAT CONDENSED MOISTURE WILL DRAIN BACK TO THE MEDIA TANK.

#### **INLET TRAP**

1. IF SEWAGE FLOWS TO THE MEDIA TANK BY GRAVITY, THE GRAVITY DRAIN LEADING TO THE MEDIA TANK SHALL PASS THROUGH A TRAP BEFORE ENTERING THE MEDIA TANK. IF TWO OR MORE DRAINS ARE EMPLOYED, THEY SHALL BE COMBINED BEFORE ENTERING THE TRAP.

2. TRAP WATER SEAL SHALL BE NOT LESS THAN 3".

THE TRAP PIPING SHALL BE CAPPED AT GROUND LEVEL.

3. THE CLEANOUT SHALL BE ON THE INLET SIDE OF THE TRAP. MAXIMUM TRAP ARM LENGTH SHALL NOT EXCEED 10'.

4. IF SEWAGE IS PUMPED TO THE MEDIA TANK, A TRAP IS NOT REQUIRED. BUT, EACH PUMP SHALL BE FITTED WITH A DISCHARGE CHECK VALVE AND THE DISCHARGE PIPING SHALL PROVIDE NOT LESS THAN 3" IWG WATER SEAL WHEN THE PUMP IS OFF.

#### AIRLIFT SHELLS

INSTALL AIRLIFT SHELLS DIRECTLY UNDER AIRLIFTS AS SHOWN TO PREVENT DAMAGE ON INSTALLATION. CONNECT SHELL TO TANK FLOOR USING (3) ½" SS ANCHORS.

#### MEDIA TANK CONSTRUCTION

1. INTERIOR SURFACES OF BOTTOM AND SIDE WALLS SHALL BE PLUMB, SQUARE AND FLAT WITHIN

WALLS SHALL BE PLUMB, SQUARE AND FLAT WITHIN ± 1".

2. FOR COVERED MEDIA TANKS, PROVIDE ACCESS THROUGH THE TANK COVER FOR EACH AIRLIFT AND FOR EACH SLUDGE REMOVAL PIPE. TANK SEAMS AND PENETRATIONS ABOVE WATER LEVEL MUST SEAL AGAINST AIR LEAKAGE WITH 3" IWG INTERNAL PRESSURE.

3. MEDIA TANK WATER LEVELS ARE CRITICAL. HOLD INLET AND OUTLET INVERT HEIGHTS AS SHOWN ON INSTALLATION DRAWINGS.

#### MEDIA MODULE

1. LIFT THE MODULE AND INSTALL THE MODULE PEDESTALS (LEGS).

DANGER: SECURE THE MODULE IN PLACE WITH BLOCKS OR OTHER SUITABLE MEANS BEFORE

INSTALLING PEDESTALS (LEGS) OR WORKING UNDERNEATH THE MODULE FOR ANY REASON.

2. INSTALL THE MODULE IN THE BASIN WITH A GAP OF APPROXIMATELY 1-1/4"ALL AROUND.

3. VERIFY THAT THE MODULE IS LEVEL.

4. THE MODULE IS PROVIDED WITH NEOPRENE SEALING STRIPS (1/4" X 6-1/2") ALONG ALL 4

5. INSTALL THE BAFFLE ASSEMBLY AND THE AIRLIFT DROP PIPE / SPLASH PLATE ASSEMBLIES.
6. COAT THE OUTSIDE SURFACE OF EACH SLUDGE REMOVAL / WATER DECANTING PIPE (BELOW THE STOP PLATE) WITH SCHEDULE 40 PVC PIPE SOLVENT CEMENT. ALLOW THE CEMENT TO BECOME TACKY BEFORE INSTALLING.

PRESS EACH PIPE INTO THE HOLE PROVIDED IN THE MEDIA UNTIL THE STOP PLATE RESTS FIRMLY ON TOP

#### AIR PIPING

1. FIELD CUT EACH HOSE TO THE REQUIRED LENGTH FOR EACH RUN. DO NOT CUT HOSE TOO SHORT.
2. SECURE EACH HOSE END TO ITS FITTING WITH 2 HOSE CLAMPS.
3. SECURE HOSES TO STRUCTURE SO THAT HOSE END FITTINGS DO NOT CARRY THE WEIGHT OF THE

#### INAL CHECK

BEFORE INSTALLING THE TANK COVER:

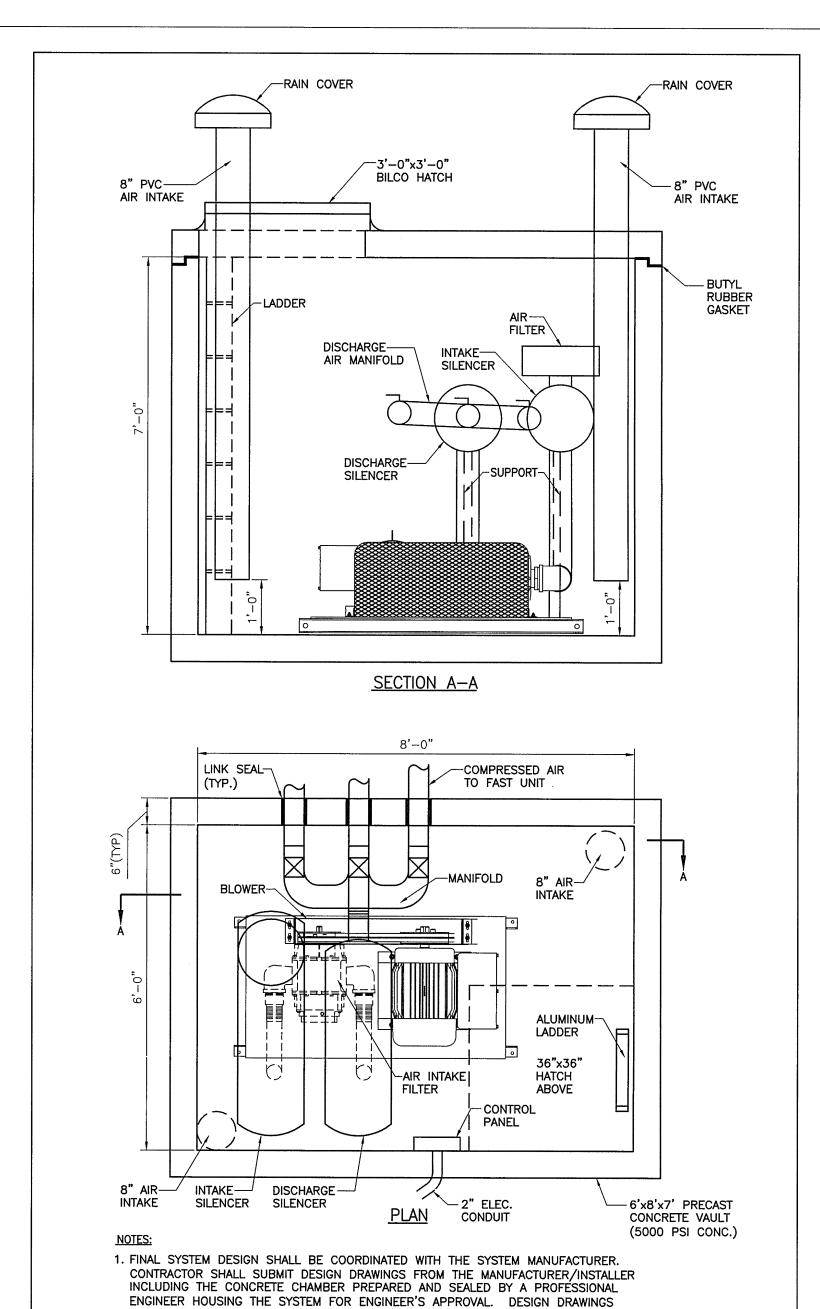
. VERIFY THAT THE MODULE IS LEVEL. 2. FILL THE BASIN WITH WATER UP TO OR SLIGHTLY ABOVE THE LEVEL OF THE EFFLUENT PIPE INVERT. WHEN THE WATER LEVEL STABILIZES, VERIFY THAT THE WATER LEVEL IS CORRECT. 3. OPERATE THE AIRLIFTS. THEY SHOULD BE PUMPING EQUALLY AND AT A HIGH RATE. ALL OF THE AIR SHOULD BE COMING UP THE AIRLIFT DRAFT TUBES AND NO AIR SHOULD BE BUBBLING UP ANYWHERE ELSE. 4. OPERATE THE AIR SCOURS. VERIFY A UNIFORM PATTERN OF BUBBLES ACROSS THE ENTIRE SURFACE OF THE BASIN. 5. CHECK THAT ALL PIPING AND HOSE CONNECTIONS ARE TIGHT AND SECURE AND THAT ALL HOSES ARE PROPERLY SUPPORTED.

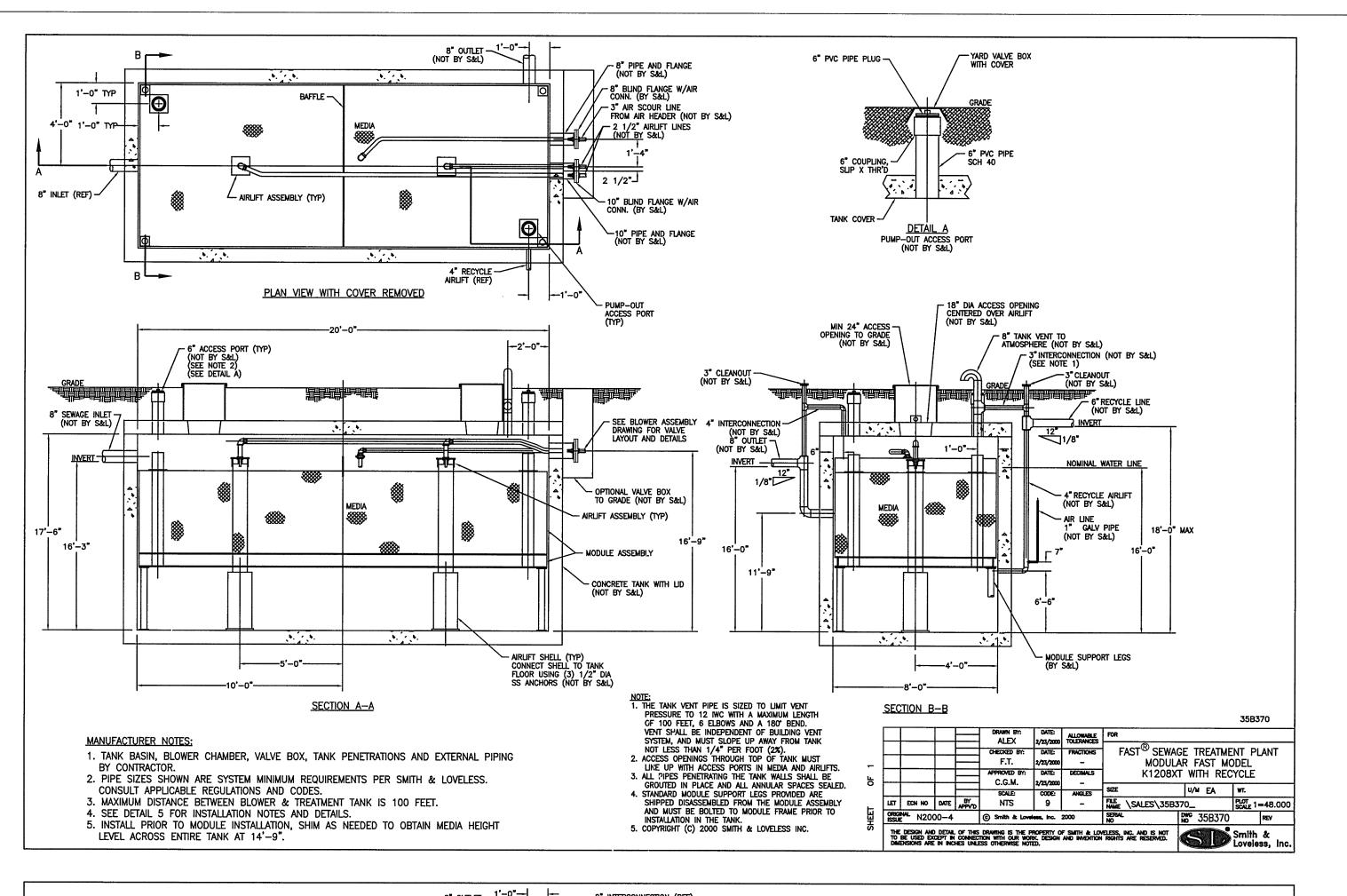
6. NO HOSE END FITTING SHOULD BE IN TENSION

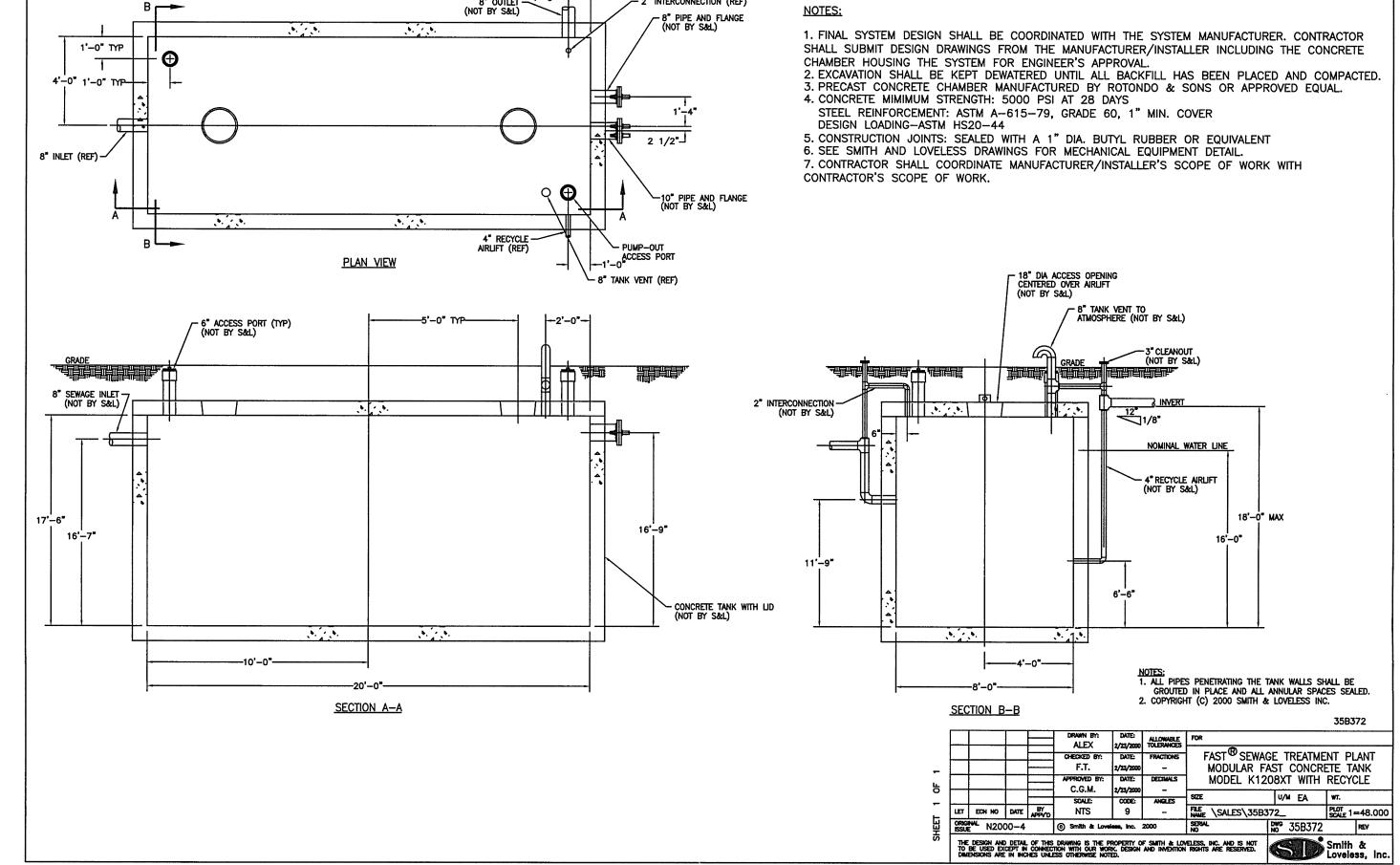
BECAUSE THE HOSE IS NOT PROPERLY SUPPORTED.

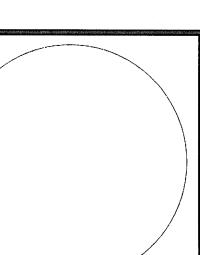
BECAUSE THE HOSE WAS CUT TOO SHORT OR

MODULAR FAST® SYSTEM CONSTRUCTION NOTES









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SHESKEY ARCHITECTS

14 Franklin Street

Quincy, MA 02169

Proponent:

SHALL INCLUDE BUOYANCY CALCULATIONS.

BLOWER VAULT

SCALE: N.T.S.

Twenty Wayland, LLC 260 Boston Post Road, Suite 9 Wayland, MA 02109 Project No: RJOC 06032

Drawn By: WJH

Checked By: CAD/BPD

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REISSUED FOR SITE 9/29/08

PLAN APPROVAL

Project:

# Wayland Town Center

400 Boston Post Road Wayland, Massachusetts

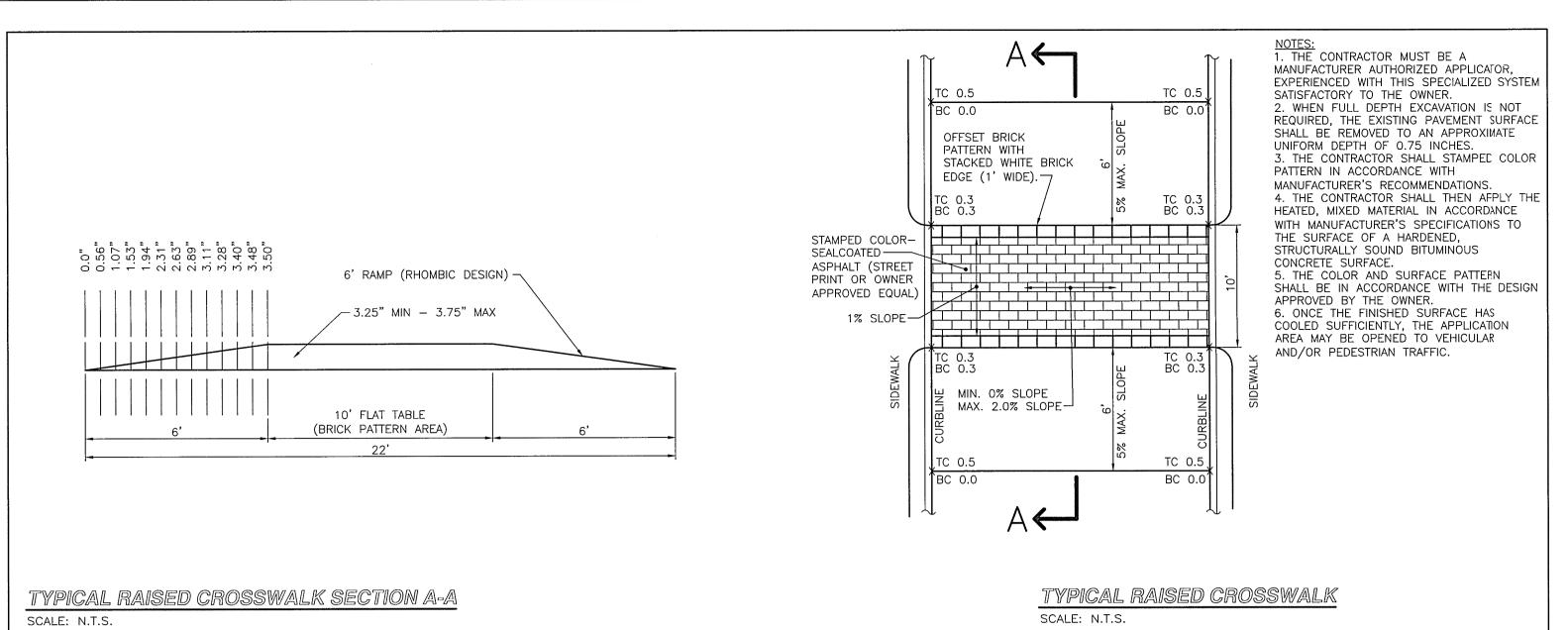
Site Plan II
Phase I Site Plan Application

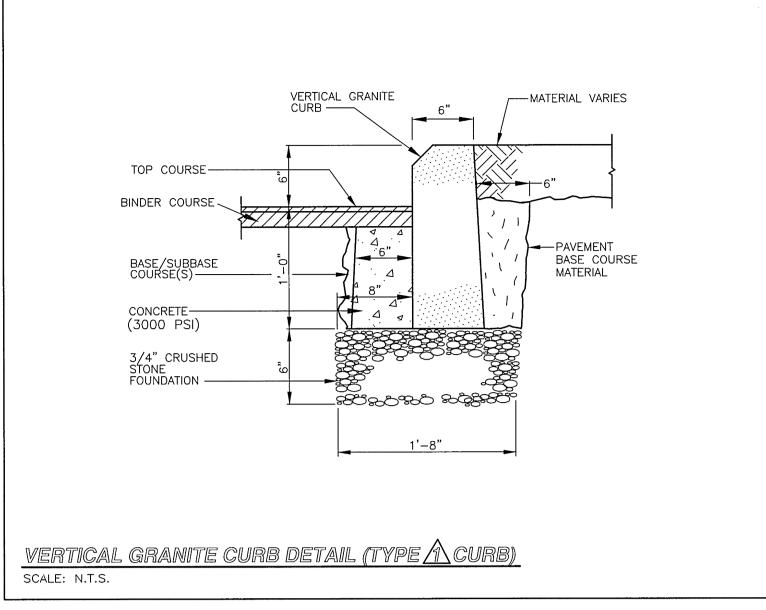
FAST SYSTEM DETAILS

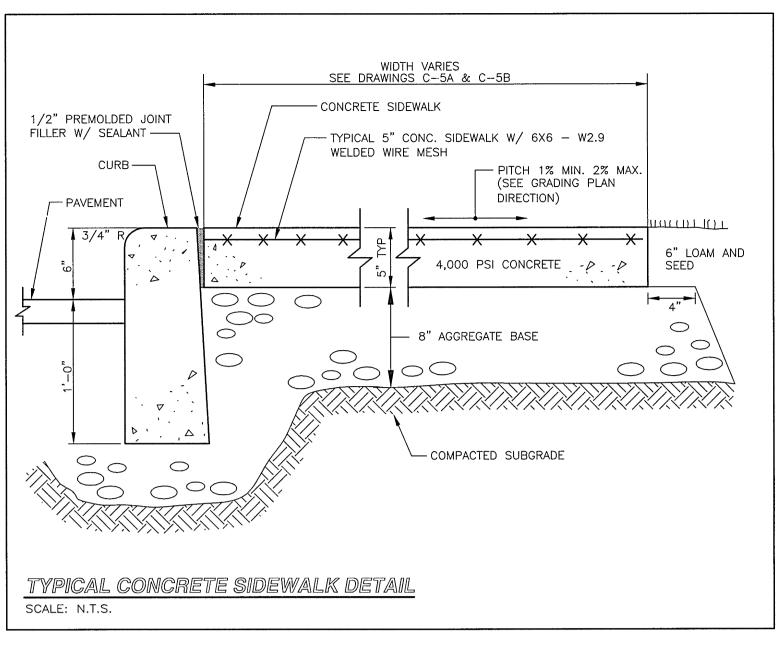
Drawing Number

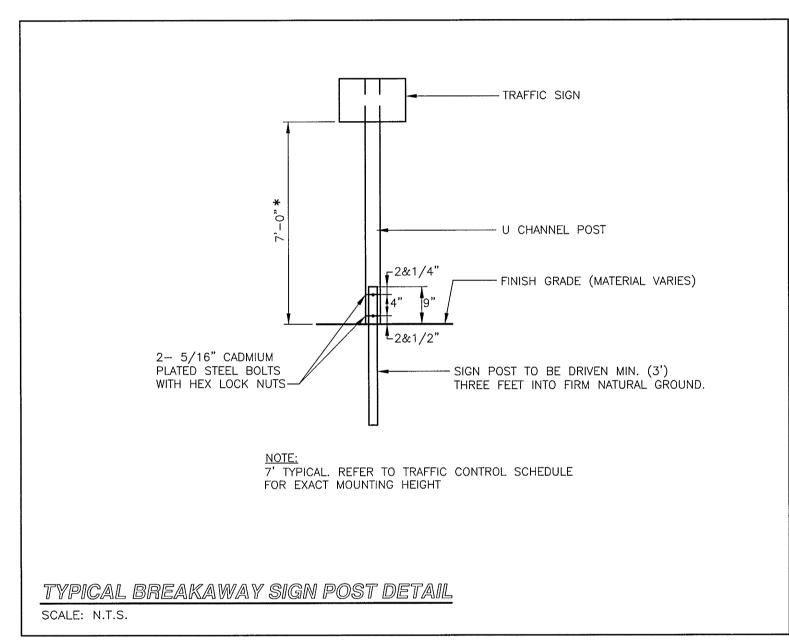
SCALE N.T.S.

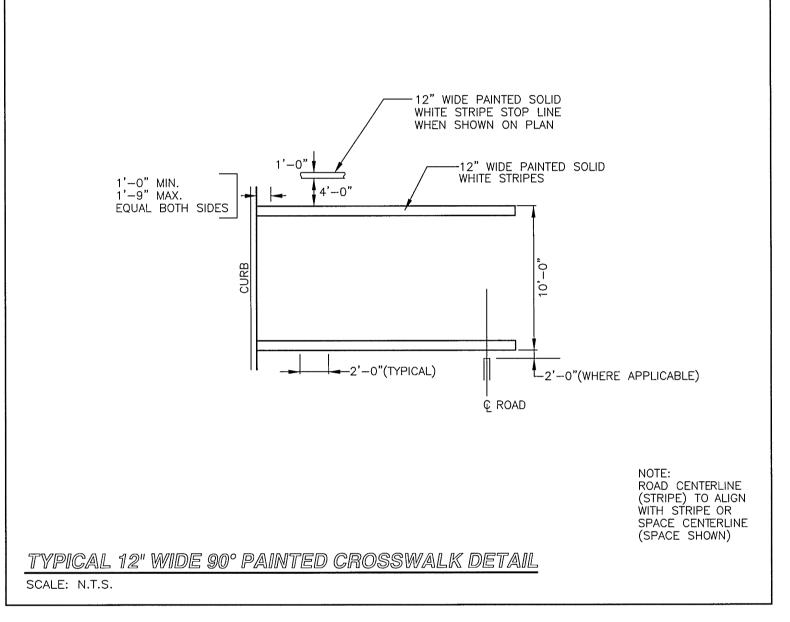
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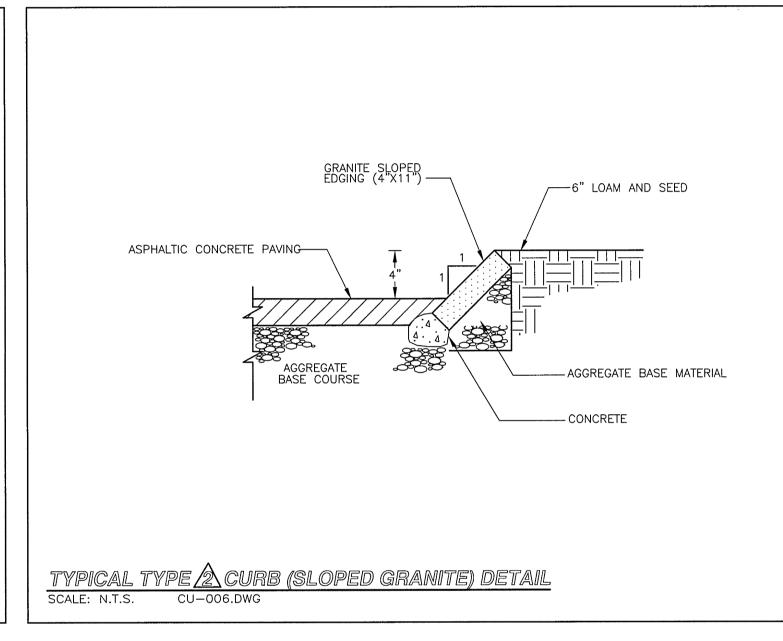


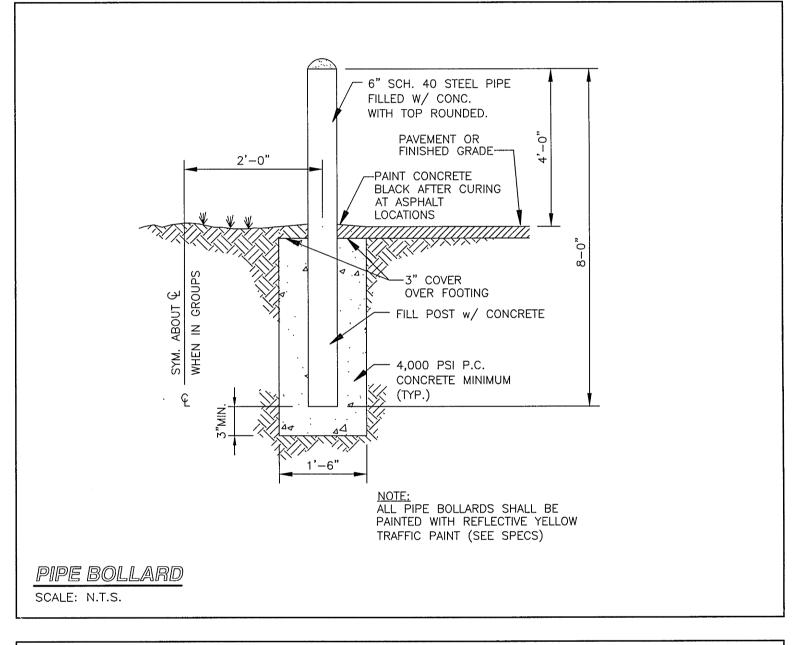


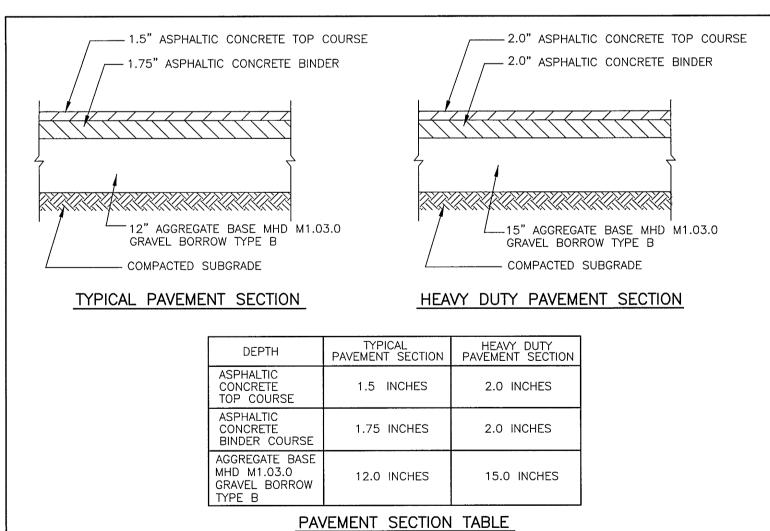


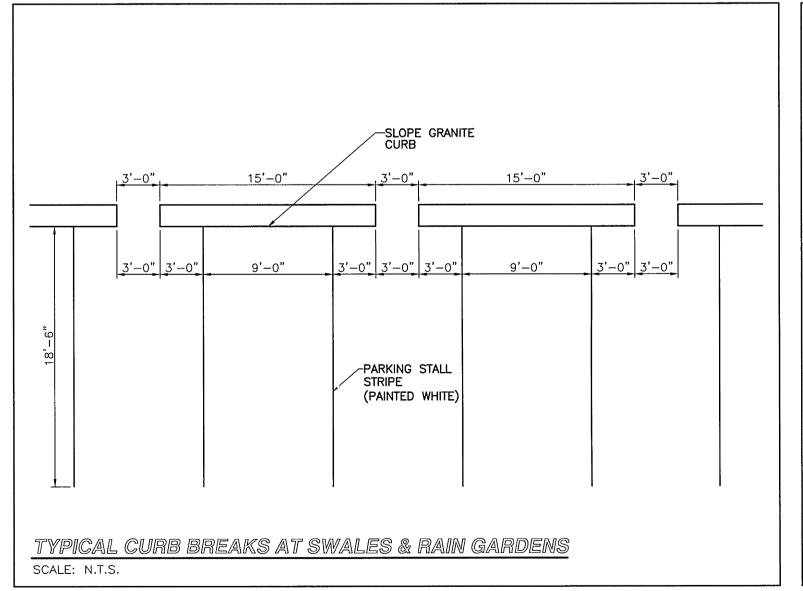


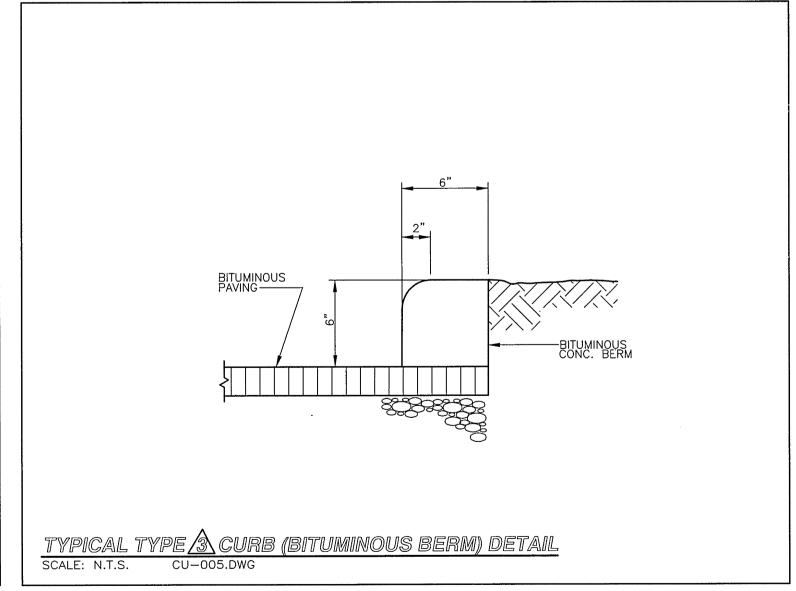


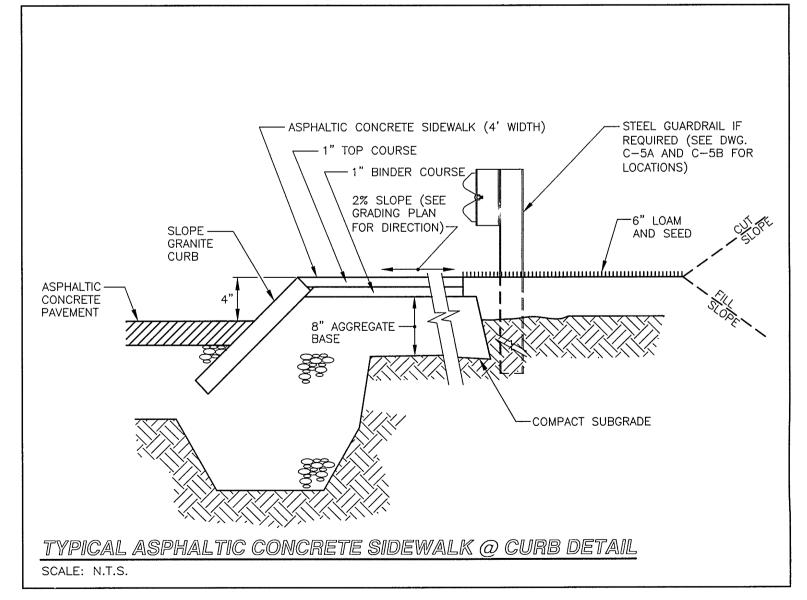


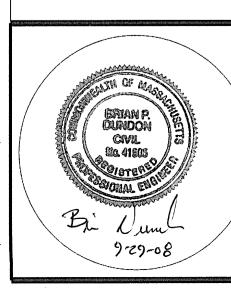












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TYPICAL PAVEMENT DETAIL

SCALE: N.T.S. PVMT-001PT.DWG

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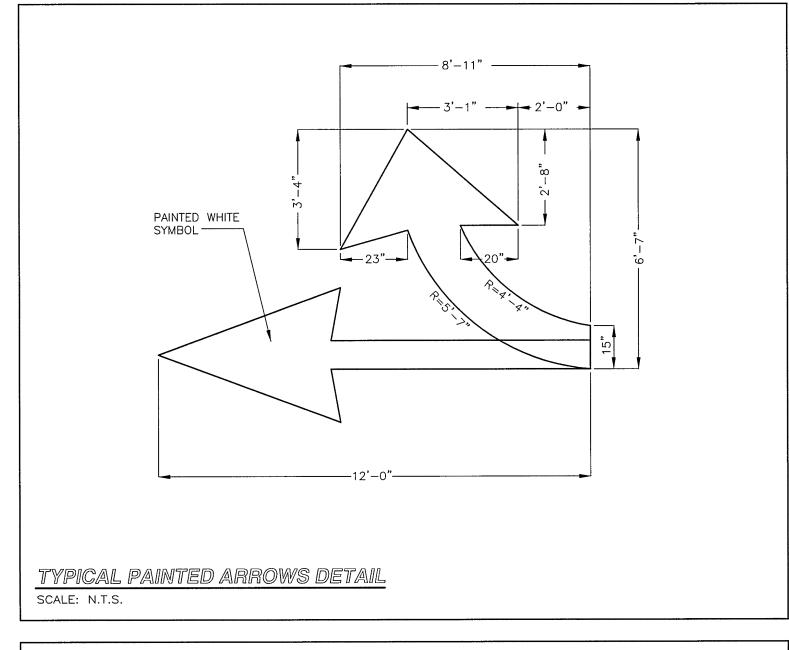
400 Boston Post Road Wayland, Massachusetts

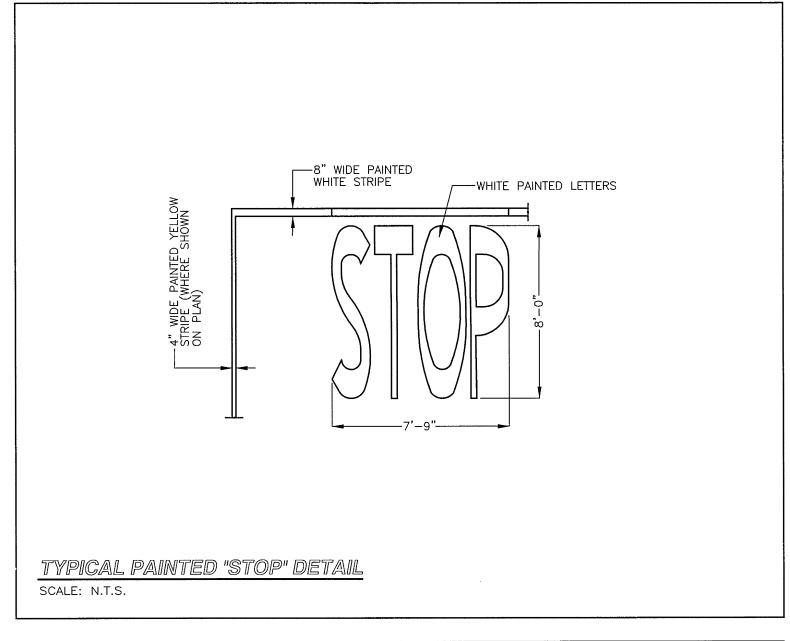
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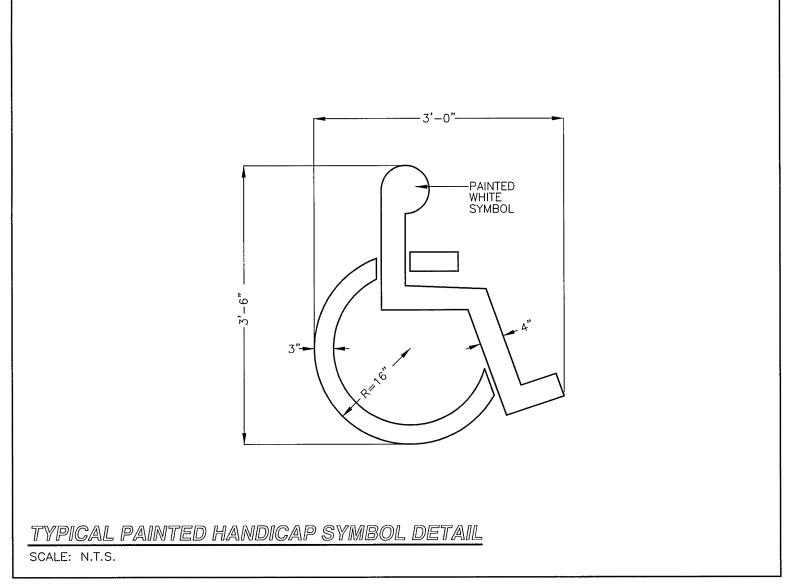
LAYOUT AND
MATERIALS DETAILS I

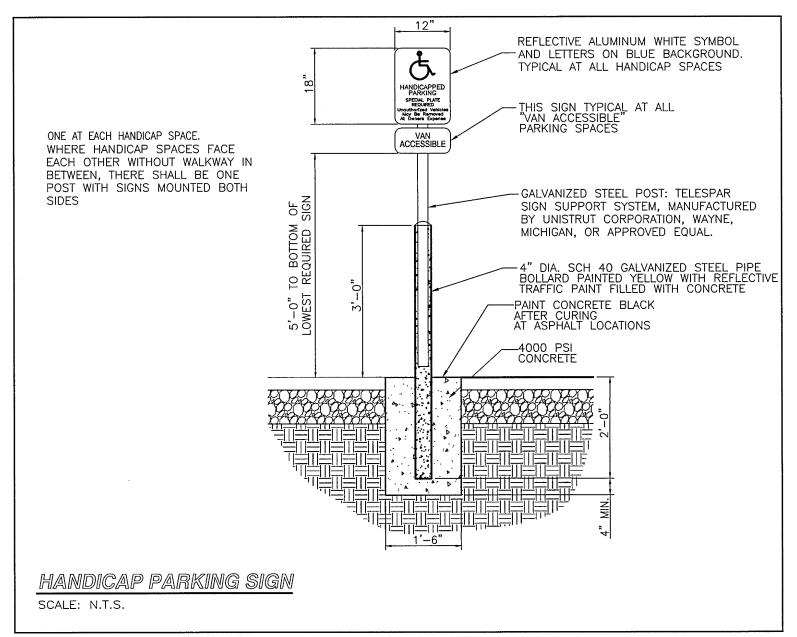
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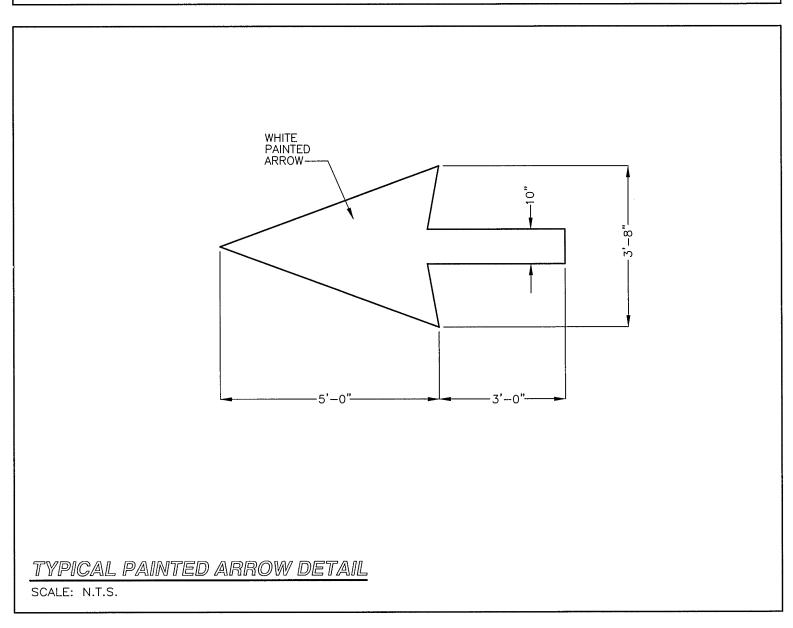
SCALE N.T.S.

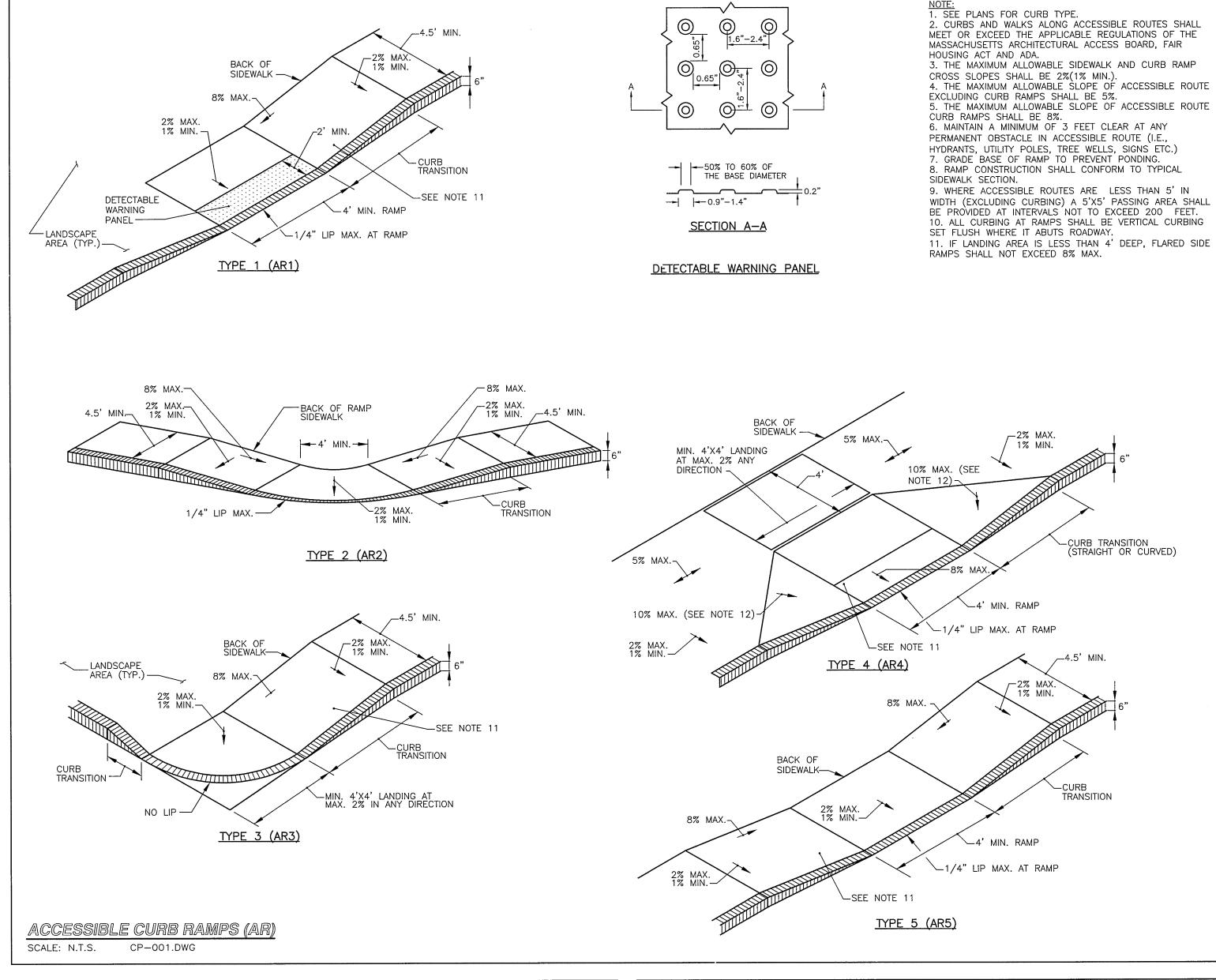


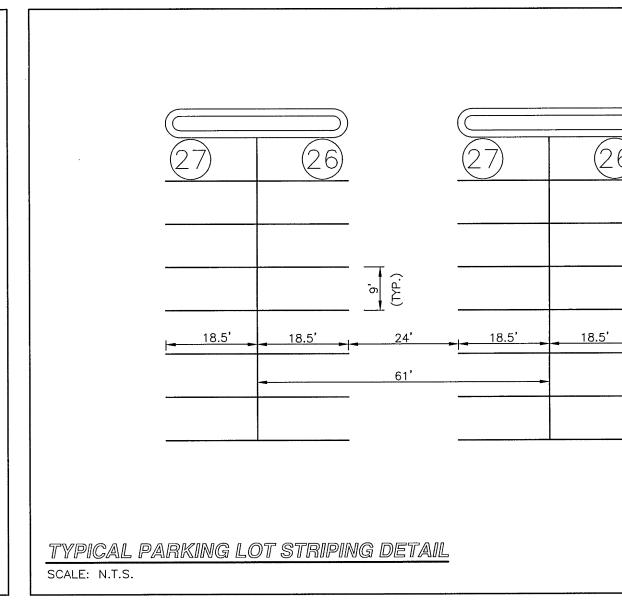




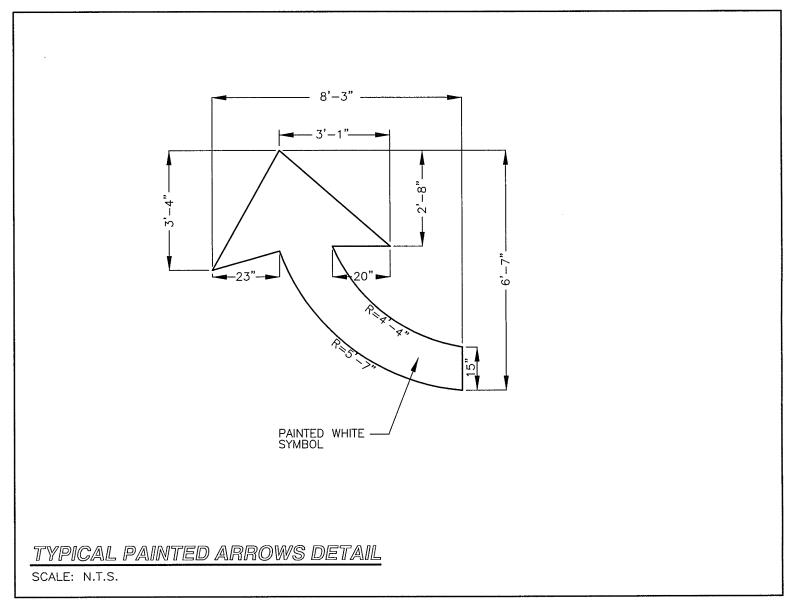


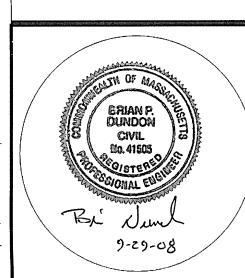






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Phase I Site Plan Application

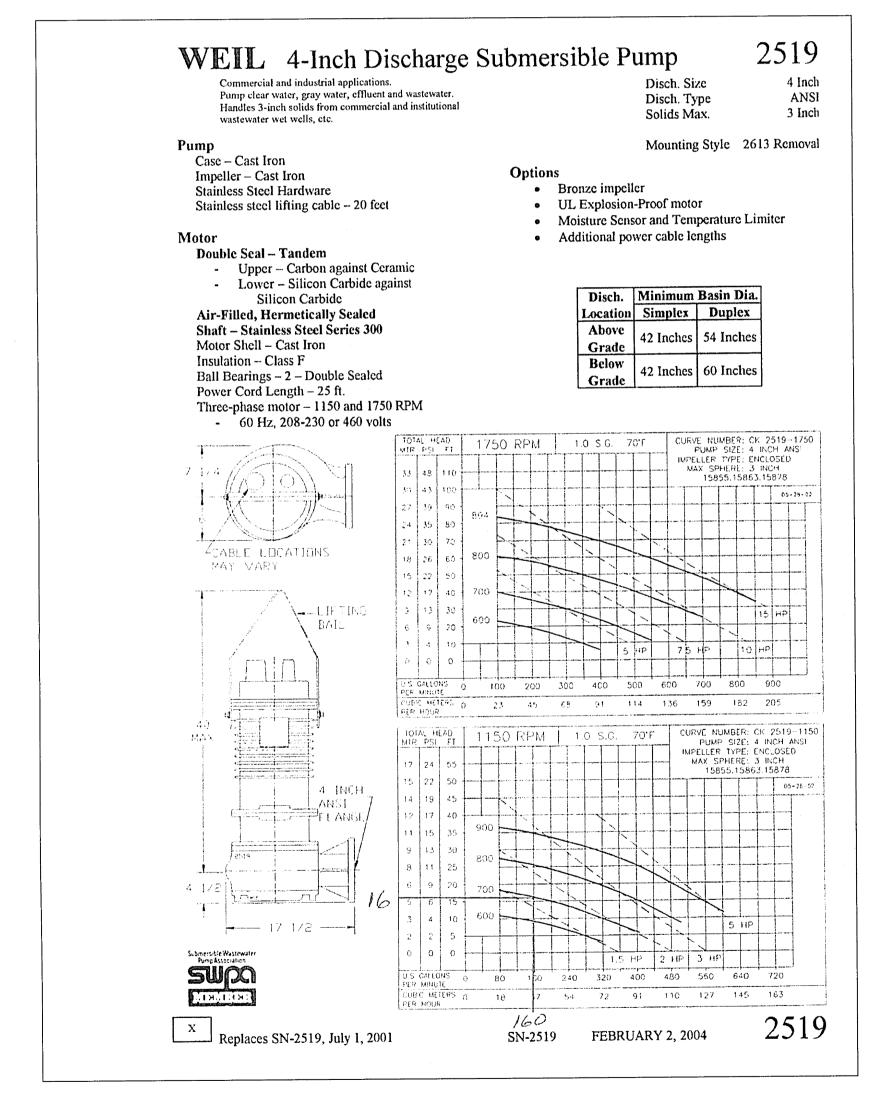
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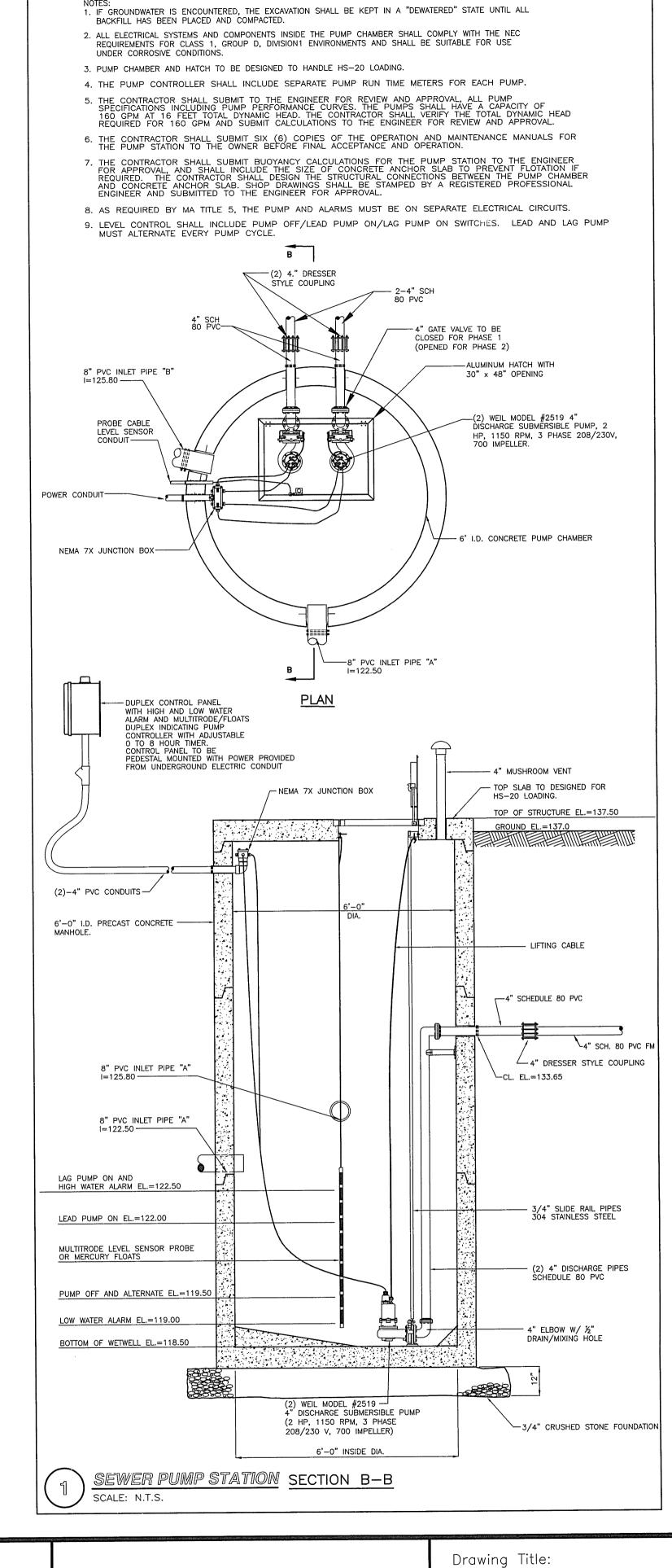
LAYOUT AND

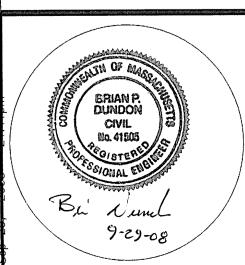
MATERIALS DETAILS II

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PLAN APPROVAL

# Wayland Town Center

400 Boston Post Road Wayland, Massachusetts

Site Plan II
Phase I Site Plan Application

SEWER PUMP STATION #1 DESIGN

Drawing Number

SCALE N.T.S.

SEWAGE DISPOSAL SYSTEM CALCULATIONS DESIGN FLOW 45,000 S.F. SUPERMARKET @ 97 GPD/1,000 S.F. = 4,365 GPD 112,500 S.F. (MAX) RETAIL @ 50 GPD/1,000 S.F. = 5,625 GPD TOTAL (MAXIMUM) DESIGN FLOW: 4,365 + 5,634 = 9,990 GPD LEACHING FIELD SIZING SLOWEST PERCOLATION RATE IN LEACHING FIELD AREA = 15 MINUTES/INCH; FIELDS ARE DESIGNED FOR 15 MINUTES/INCH EFFLUENT LOADING RATE FOR PRESSURE DISTRIBUTION = 0.61 GPD/S.F. REQUIRED LEACHING AREA: ---PROVIDED LEACHING AREA: 16,480 SF (2 BEDS @ 8,240 SF EACH) DISTRIBUTION SYSTEM FOR 80 FT x 103 FT BEDS 13 LATERALS @ 6 FT O.C. 12 SPACES @ 6 FT PLUS 2 SIDES @ 4 FT 24 - 1/2" HOLES @ 4 FT O.C. EACH LATERAL 312 TOTAL HOLES 1.17 GPM/HOLE @ 2.5 FT HEAD = 365 GPM PUMPS TO BE SIZED TO PUMP 365 GPM (MIN) DESIGN VOLUME MAXIMUM DOSE = 8,240 SF x 1IN/FT x .5 VOID RATIO x 7.48 G/CF = 2568 GAL FOUR DOSES/DAY = 9,990 GAL/2 BEDS/4 = 1,249 GAL (4 DOSES EACH BED) RUN TIME 1249 GAL/365 GPM = 3.43 MIN

RESERVE VOLUME PROVIDED BETWEEN ELEV. 132.60 - 130.80 = 1.8 FT (1.8 FT x 376 G/FT = 677 GAL\*)

\*BACKUP GENERATOR POWER TO BE PROVIDED

7. EXCEPT IN PAVED AREAS, FILL OVER THE LEACHING AREAS SHALL BE ORDINARY FILL , CLEAN AND FREE OF BOULDERS AND STONES GREATER THAN SIX INCHES. 8. FINAL COVER OF TOPSOIL SHALL BE GRADED TO A MINIMUM SLOPE OF 2%. 9. INSPECTIONS SHALL BE COORDINATED WITH RJ O'CONNELL & ASSOCIATES AND THE BOARD OF HEALTH AGENT. ALL INSTALLATION, INSPECTIONS, AND AS-BUILT PLANS SHALL BE DONE IN ACCORDANCE WITH FOXBORO BOARD OF HEALTH ON-SITE SEWAGE DISPOSAL SYSTEM 10. CONTRACTOR SHALL INSTALL ONE PERMANENT BENCHMARK WITHIN 50 TO 75 FEET OF THE SEWAGE DISPOSAL SYSTEM. LOCATION AND ELEVATION OF BENCHMARK SHALL BE SHOWN ON 11. PUMPS, ALARMS AND OTHER EQUIPMENT REQUIRING PERIODIC OR ROUTINE INSPECTION AND MAINTENANCE SHALL BE OPERATED, INSPECTED AND MAINTAINED IN ACCORDANCE WITH THE MANUFACTURER'S AND DESIGNER'S SPECIFICATIONS AND DEPARTMENT GUIDANCE. IN NO INSTANCE SHALL INSPECTION BE PERFORMED LESS FREQUENTLY THAN ONCE EVERY THREE MONTHS FOR A SYSTEM SERVING A FACILITY WITH A DESIGN FLOW OF 2,000 GALLONS PER DAY OR GREATER...THE SYSTEM OWNER SHALL SUBMIT THE RESULTS OF SUCH INSPECTIONS TO THE LOCAL APPROVING AUTHORITY ANNUALLY BY JANUARY 31 OF EACH YEAR FOR THE PREVIOUS CALENDAR YEAR. (310 CMR 15.254, 2.d.)

SIEVE ANALYSIS ALSO SHALL BE PERFORMED ON

4.75 mm

0.30 mm

0.15 mm

0.075 mm

SIEVE SIZE

#100

#200

THE FRACTION OF THE FILL SAMPLE PASSING THE #4 SIEVE, SUCH ANALYSIS MUST DEMONSTRATE THAT THE MATERIAL MEETS EACH OF THE FOLLOWING SPECIFICATIONS:

EFFECTIVE PARTICLE SIZE % THAT MUST PASS SIEVE

5. PRIOR TO PLACEMENT OF THE FILL, THE BOTTOM SURFACE OF THE EXCAVATION SHALL BE

SCARIFIED AND RELATIVELY DRY. FILL SHALL NOT BE PLACED DURING RAIN OR SNOW STORMS. IF THE WATER TABLE ELEVATION IS ABOVE THE EXCAVATION ELEVATION, THE EXCAVATION SHALL

6. FILL SHALL BE SUFFICIENTLY COMPACTED TO PREVENT DEPRESSIONS DUE TO SETTLING (85%

MODIFIED PROCTOR) EXCEPT IN PAVED AREAS WHERE COMPACTION SHALL BE AS SPECIFIED FOR

10% - 100%

0% - 20%

0% - 5%

FRICTION LOSSES: F=0.002083L(\frac{140}{C}) X \frac{Q}{D4.8655} WHERE: L = LENGTHC = FRICTION FACTOR (140)D = FORCE MAIN OR LATERAL DIAMETER Q = PUMP DISCHARGE RATE (365 GPM)6" FORCE MAIN (L=235') = 4.4'6" MANIFOLD = 0.1' 2" LATERALS = 0.1'2" RISER = 0.2' CHECK VALVE = 4'GATE VALVES = 2'MINOR PUMP STATION LOSSES = 2' TOTAL FRICTION LOSSES = 12.8 ≈ 13' TOTAL DYNAMIC HEAD (TDH): 2' LATERAL INVERT: 136.80 PUMP OFF ELEVATION: 127.00

130.80

130.30

127.00

126.50

126.00

PUMP ON ELEVATION: 130.30 ELEVATION HEAD:  $136.8 - 127.00 = 10^{\circ}$ TOTAL DYNAMIC HEAD (TDH): STATIC HEAD = 10' HEAD LOSS DUE TO FRICTION = 13'

DOSING PUMP CHAMBER SIZING:

INVERT INTO CHAMBER! LAG PUMP & ALARM:

BOTTOM OF CHAMBER:

LEAD PUMP ON:

LOW WATER ALARM:

PUMP OFF:

USE 8' DIAMETER ROUND CHAMBER

VOLUME = 376 GALLONS / VERTICAL FOOT

DOSE VOLUME: (1249/376) = 3.33 FT

RESIDUAL = 2.5' $TDH = 25.5' \approx 26'$ PUMP MUST PROVIDE DISCHARGE RATE OF 365 GPM @ 26 FT. TDH

USE WEIL MODEL #1620 3-INCH SUBMERSIBLE PUMP (5 HP, 1150 RPM, 3 PHASE, 208/230V, 1050 IMPELLER)

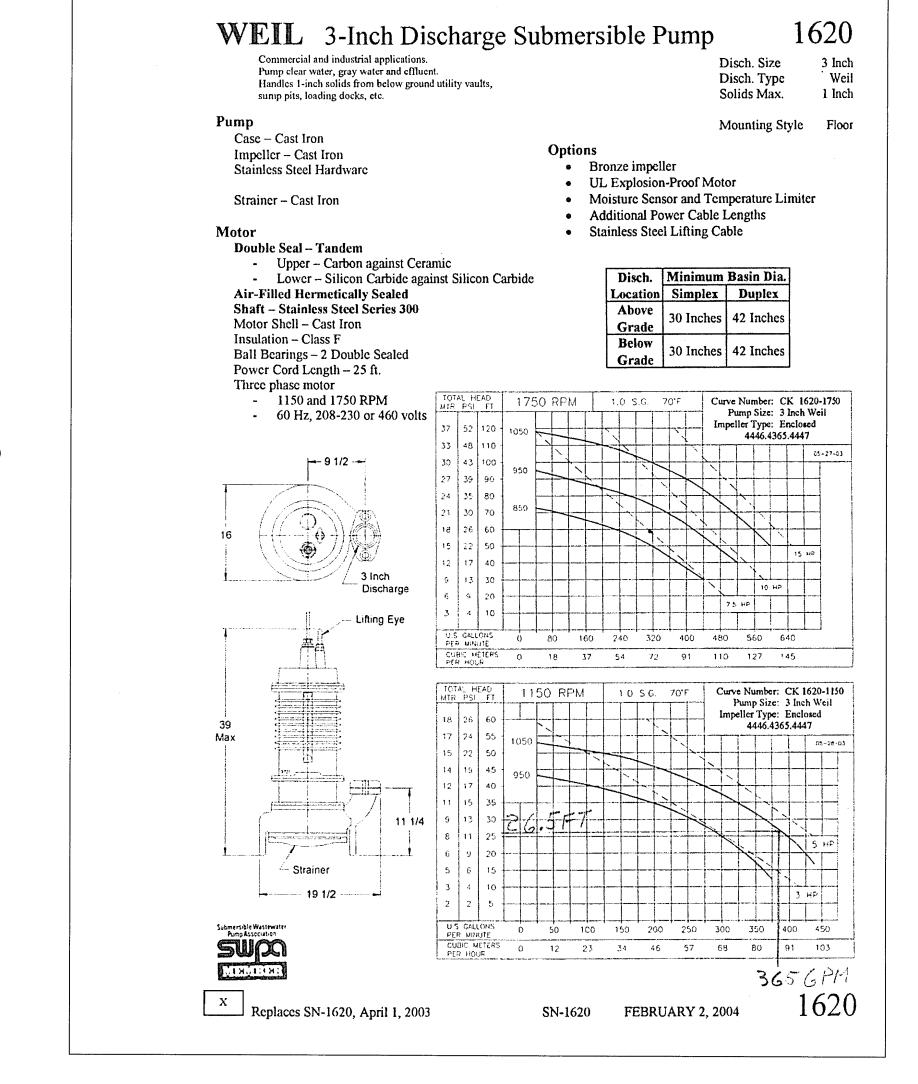
SEPTIC SYSTEM NOTES

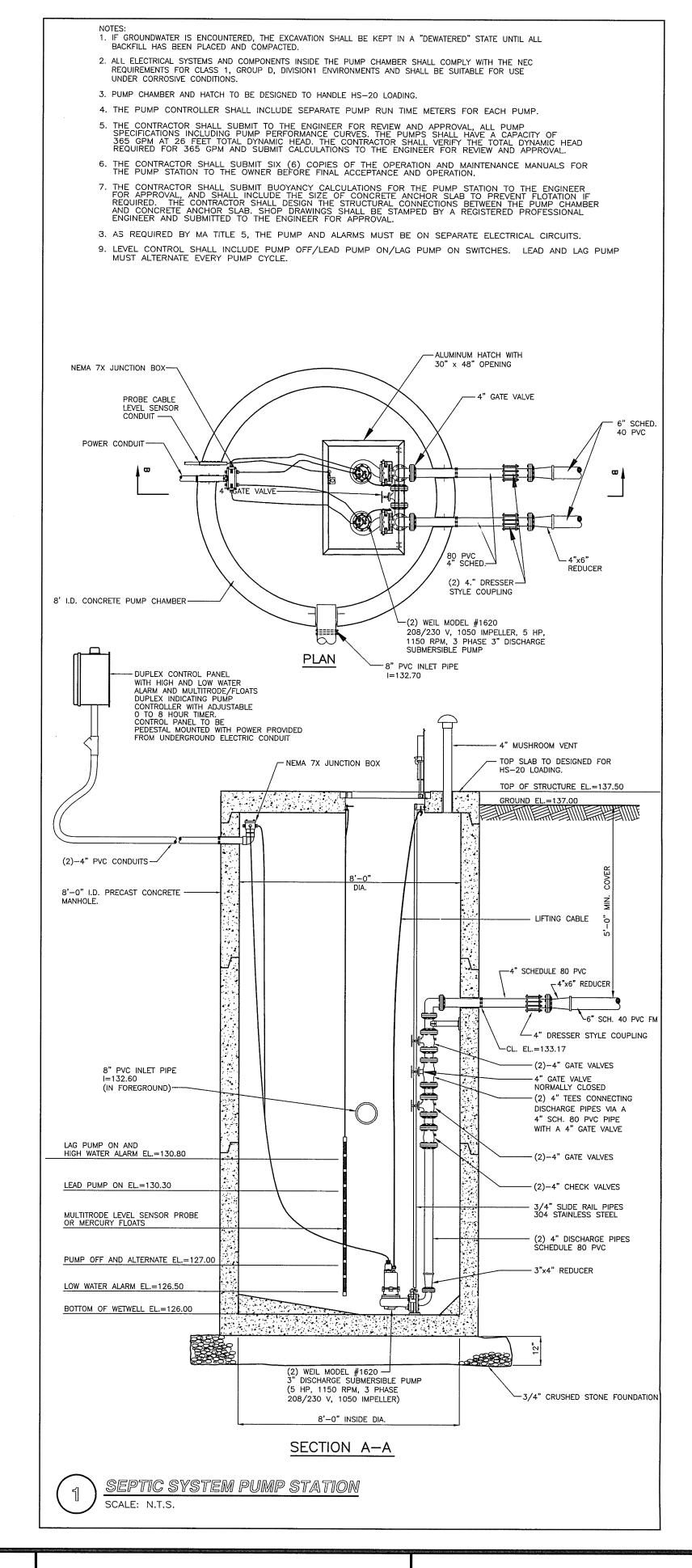
1. ALL COMPONENTS OF THE SEPTIC SYSTEM, INCLUDING BUT NOT LIMITED TO PIPING, TANKS. PUMPS AND SOIL ABSORPTION SYSTEM SHALL BE INSTALLED IN ACCORDANCE WITH MASSACHUSETTS ENVIRONMENTAL CODE 310 CMR 15.00 (TITLE 5).

2. CONTRACTOR SHALL EXCAVATE ALL UNSUITABLE MATERIAL WITHIN THE LIMITS OF FILL BENEATH THE SOIL ABSORPTION (LEACHING) SYSTEMS. UNSUITABLE MATERIAL SHALL INCLUDE BUT NOT BE LIMITED TO VEGETATION, TOPSOIL, SUBSOIL, ORGANIC MATTER, OR ANY MATERIAL DEEMED UNSUITABLE BY THE SOILS ENGINEER. UNSUITABLE MATERIAL SHALL BE EXCAVATED A MINIMUM OF 5 FEET LATERALLY IN ALL DIRECTIONS BEYOND THE OUTER PERIMETER OF THE LEACHING AREA TO THE DEPTH OF NATURALLY OCCURRING PERVIOUS SOIL LAYER IN WHICH THE PERCOLATION TEST WAS PERFORMED AS REQUIRED BY 310 CMR 15.240.

3. CONTRACTOR SHALL TAKE PRECAUTIONS NOT TO COMPACT THE SUBGRADE OF THE LEACHING AREAS THAT ARE LOCATED OUTSIDE OF PAVED AREAS. VEHICULAR TRAFFIC AND PARKING OF VEHICLES OR EQUIPMENT IN OR ON THE AREA OF THE LEACHING SYSTEM SHALL BE AVOIDED DURING AND AFTER CONSTRUCTION OF THE SYSTEM. UNTIL RECEIPT OF A CERTIFICATE OF COMPLIANCE, THE LEACHING AREA SHALL BE STAKED AND FLAGGED TO PREVENT THE USE OF THE AREA FOR ACTIVITIES WHICH MIGHT DAMAGE THE SYSTEM. STOCKPILING OF MATERIALS OR EQUIPMENT WITHIN THE AREA IS PROHIBITED.

4. IN ACCORDANCE WITH 310 CMR 15.255 (3) AND EXCEPT WHERE OTHER MATERIALS ARE SPECIFIED, FILL MATERIAL WITHIN THE LEACHING AREA AND UP TO THE TOP OF THE PEA STONE SHALL CONSIST OF SELECT ON-SITE OR IMPORTED SOIL MATERIAL. THE FILL SHALL BE COMPRISED OF CLEAN GRANULAR SAND, FREE FROM ORGANIC MATTER AND DELETERIOUS SUBSTANCES. THE FILL SHALL NOT CONTAIN ANY FILL MATERIAL LARGER THAN 2-INCHES. SIEVE ANALYSIS, USING A #4 SIEVE, SHALL BE PERFORMED ON A REPRESENTATIVE SAMPLE OF THE FILL. UP TO 45% BY WEIGHT OF THE FILL SAMPLE MAY BE RETAINED ON THE #4 SIEVE







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Project No:

Wayland Town Center

400 Boston Post Road Wayland, Massachusetts

Site Plan II Phase I Site Plan Application Drawing Title:

SEPTIC SYSTEM PUMP STATION #2 DESIGN

Drawing Number

SCALE N.T.S.

C-15

RJO'CONNELL

STONEHAM, MA 02180

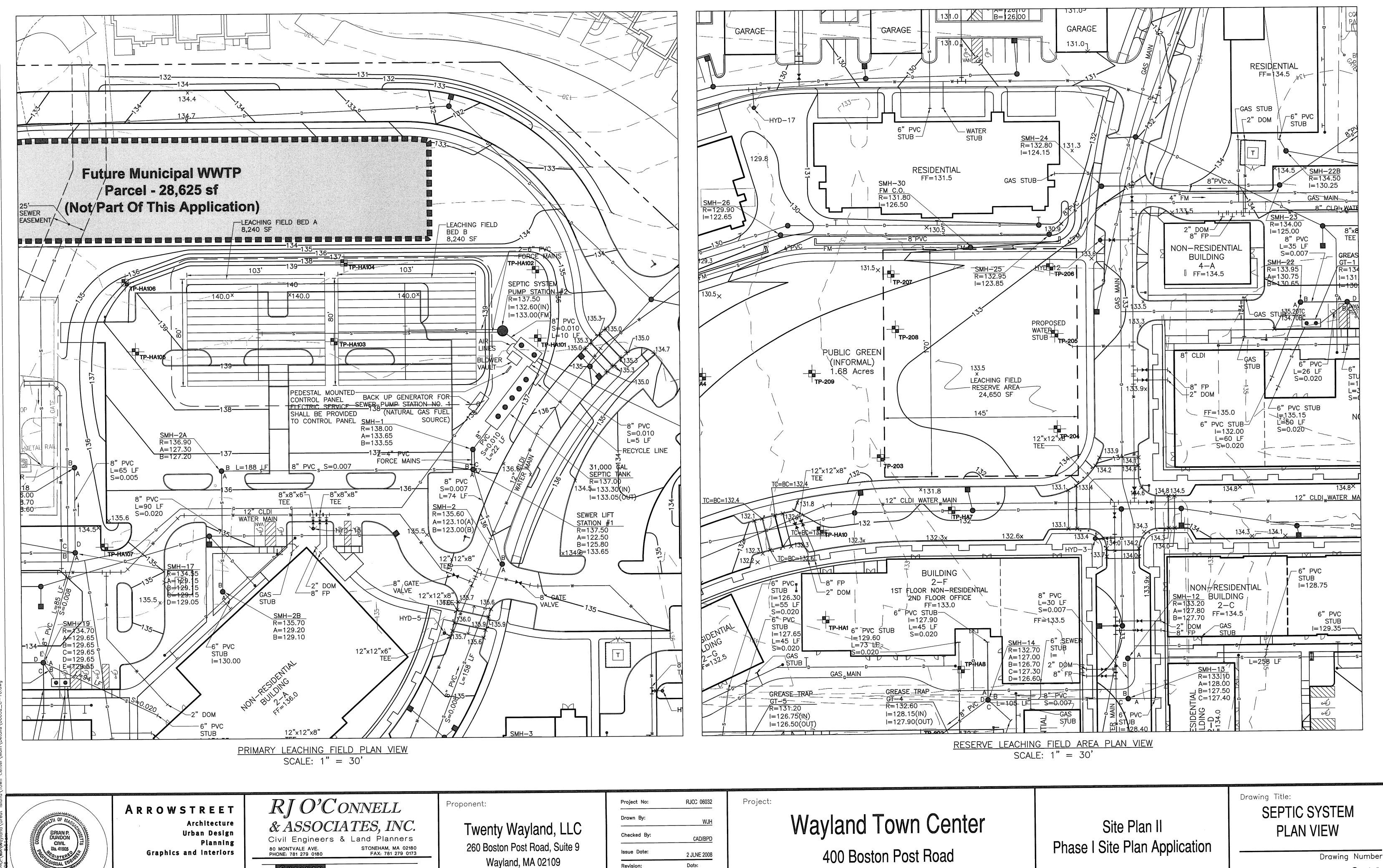
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CAD/BPD

2 JUNE 2008

9/29/08



REISSUED FOR SITE

PLAN APPROVAL

Wayland, Massachusetts

C-16

SCALE N.T.S.

Drawing name: G:\MA\Wayland\Great Island\Tow

ARCHITECTS

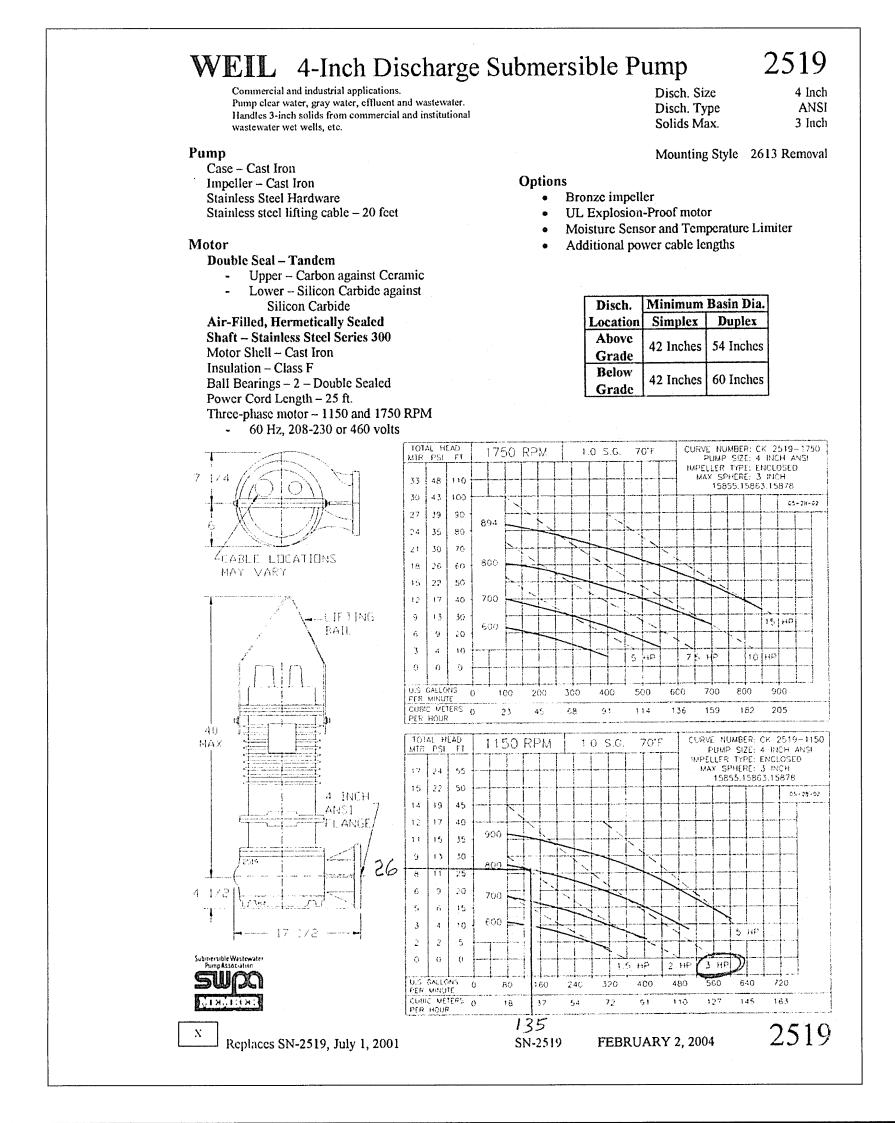
14 Franklin Street

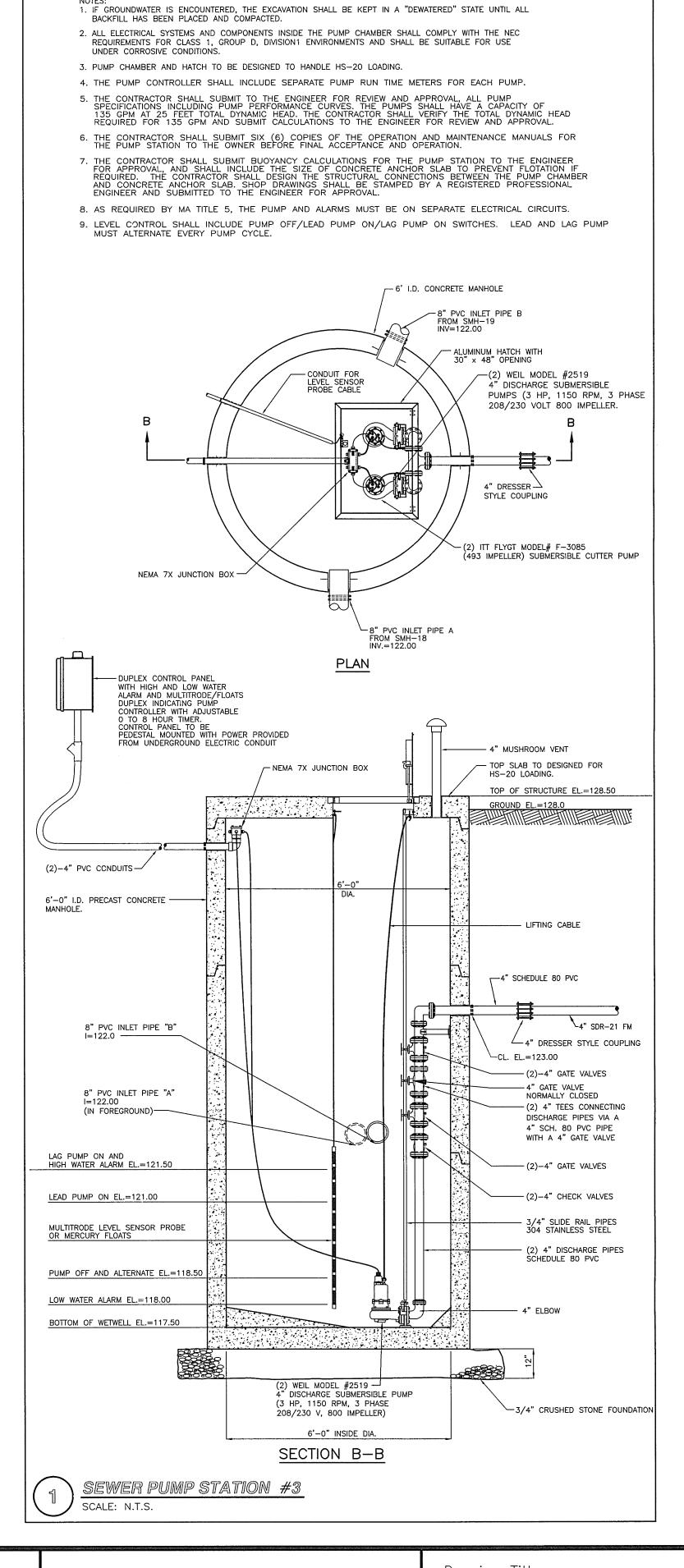
Quincy, MA 02169

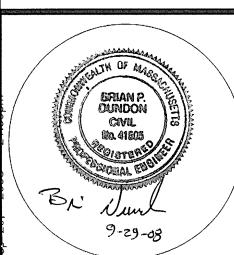
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Project No:	RJOC 06032
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Checked By:	CAD/BPD
Issue Date:	2 JUNE 2008
Revision:	Date:
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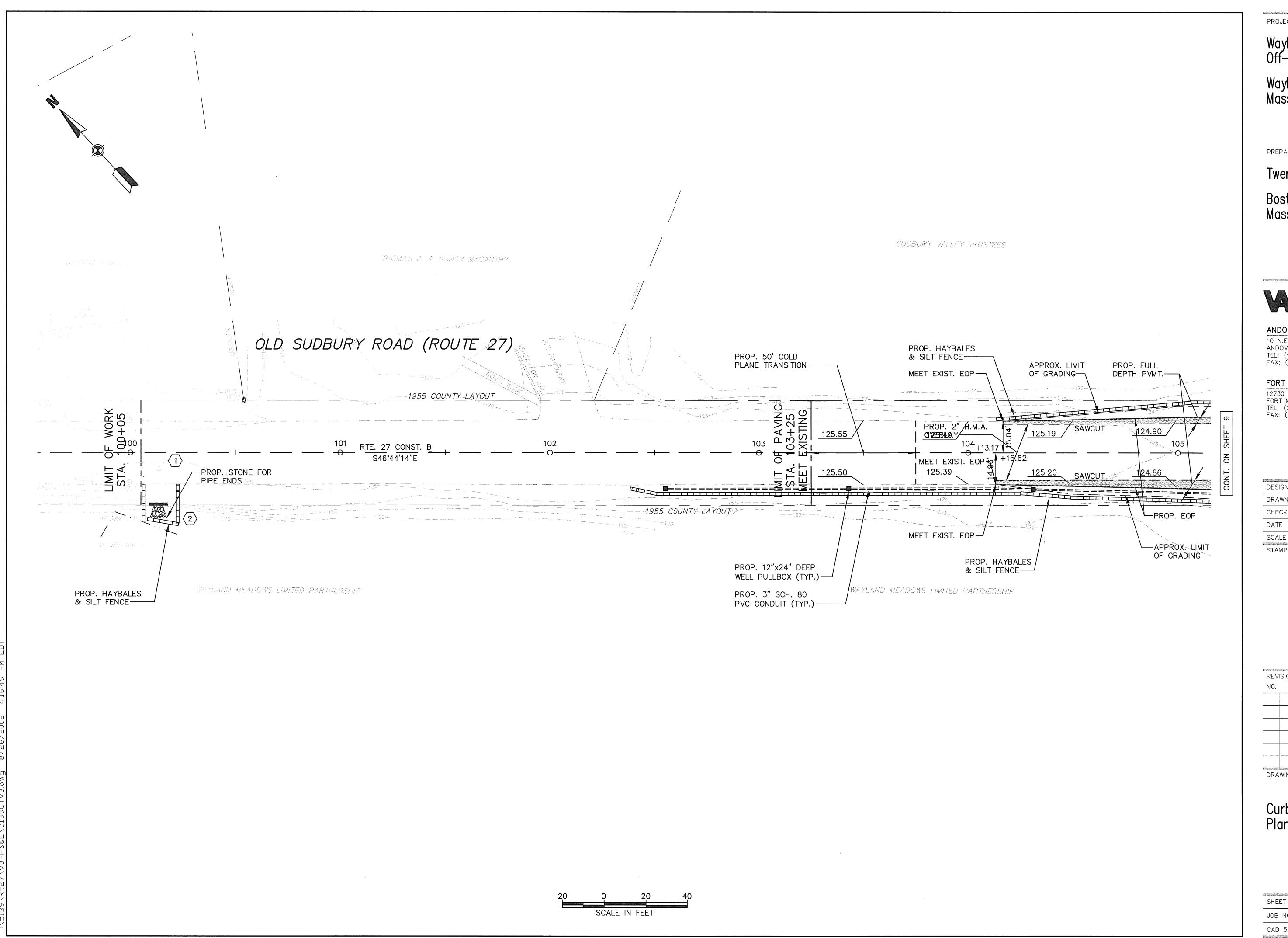
# Project: Wayland Town Center

400 Boston Post Road Wayland, Massachusetts

Site Plan II Phase I Site Plan Application Drawing Title: SEWER PUMP STATION # 3 DESIGN

Drawing Number

SCALE N.T.S.



PROJECT TITLE

Wayland Town Center Off-Site Improvements

Wayland, Massachusetts

PREPARED FOR

Twenty Wayland, LLC

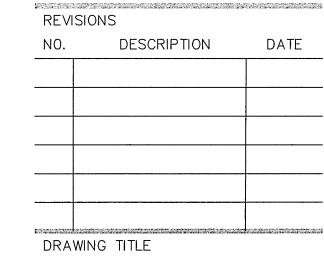
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# **Stormwater Management Study**

Wayland Town Center Wayland, MA

Applicant: Twenty Wayland, LLC 260 Boston Post Road, Suite 9 Wayland, MA 02109

Prepared by: R.J. O'Connell & Associates, Inc. 80 Montvale Avenue Stoneham, MA 02180

**Date:** June 2, 2008

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#### I. STORMWATER MANAGEMENT NARRATIVE

#### 1.0 Project Location and Description

The project site has an area of approximately 56.9 acres and is located at 400 Boston Post Road, in Wayland, MA (See Figure 1 - Locus Map). The site is bound by Route 20 (Boston Post Road) to the south, the Wayland Business Center property to the North, Sudbury River to the west and the Wayland meadows property and Route 27 (Old Sudbury Road) to the East. There are wetland areas on the site. The larger wetland is located at the western portion of the site adjacent to Sudbury River, two smaller wetland areas are at the north east portion of the site adjacent to the Wayland Business Center property, and on the south east portion of site adjacent to Route 20.

Approximately 25 acres of the site is currently developed. The existing development contains a building formerly occupied by Raytheon with a footprint area of  $\pm 272,700$  square feet and a  $\pm 10,500$  square foot building formerly utilized as a daycare center and associated parking. There is a Wastewater Treatment facility on site which is owned and operated by the Town of Wayland. The existing topography of the project site generally slopes east to west and ranges from elevation  $\pm 146$  at the eastern property line adjacent to the Wayland Meadows Property to elevation  $\pm 116$  at the western side of the site in the large wetland area adjacent to Sudbury River.

The proposed development program consists of demolishing the existing ±272,700 square foot building and constructing a mixed use development consisting of residential, municipal and retail use buildings, with associated parking facilities, utilities, and stormwater collection system (See Figure 2 - Site Plan). The stormwater management system for the proposed project has been designed in accordance with the MADEP's Stormwater Management Policy and Standards and the Town of Wayland's Wetlands and Water Resources Bylaw Chapter 194 Rules and Regulations.

Stormwater quality control will be achieved through a program of Best Management Practices (BMP's). The proposed stormwater management system will significantly improve the quality of the stormwater runoff. The existing pavement runoff drains to catch basins which direct runoff to wetland resource areas without additional water quality treatment. The proposed stormwater management system for the project will include new catch basins with deep sumps and hoods, and the use of innovative low impact development (LID) techniques.

Low Impact Development is a stormwater management approach with the goal to mimic the site's predevelopment hydrology. This is done by using design techniques that infiltrate, filter, store, and detain water throughout the site using decentralized micro-scale controls. LID includes structural and non-structural strategies such as retention areas, reduction of impervious surfaces, lengthening of flow paths, and the preservation of existing vegetation and landscape features. Redevelopment and improving stormwater quality of existing sites, and energy and water conservation are also examples of LID techniques.

LID techniques proposed for the project include the use of water quality swales, rain gardens, and bioretention basins to increase times of concentration, promote groundwater recharge, and enhance water quality. The water quality swales will be planted with grass on the bottom and sides to slow the runoff velocity and filter pollutants. The rain gardens and bio-retention basins will be planted with a combination of grasses, perennials, shrubs, and small trees. The clean stormwater runoff from the building rooftops will be directed to the water quality swales and bio-retention basins to provide additional groundwater recharge.

Based on a review of The National Flood Hazard Insurance Rate Map for the Town of Wayland, Massachusetts, Community Panel No 250224 0002 C, Dated (Revised) February 19,1986, the project site is located within the following zones:

Zone A - Area of 100 year flood

Zone B – Area between 100 year and 500 year floods

Zone C - Area of Minimal Flooding

#### 2.0 Design Objectives and Methodologies

The stormwater management system was designed to control post-development peak runoff from the site by keeping it at or below the levels of pre-development. This was done by analyzing the 2-year, 10-year, and 100-year 24-hour storm events using the Hydraflow Hydrographs 2004 computer program. Hydraflow uses TR-20, the SCS Unit Hydrograph method (an industry accepted method) capable of developing runoff hydrographs for both simple and complex drainage basins. Hydraflow computes SCS Method Runoff Hydrographs by convoluting a rainfall hyetograph through a unit hydrograph.

Utilizing the TR-20 method in Hydraflow, the following data is necessary for input:

Watershed Area: Areas of each watershed are calculated and expressed in acres for these calculations. SCS Curve Number (CN): Based on the cover type and hydrologic soil group, a weighted curve number (CN) was determined for each of the existing watersheds utilizing Table 2-2a- Runoff Curve Numbers For Urban Areas and Worksheet 2, Runoff Curve Number and Runoff from the Soil Conservation Service Technical Release 55 – Urban Hydrology for Small Watersheds

**Time Interval (Minutes)**: For the most compatible results with the existing conditions, this value is defined at 2 minutes.

**Time of Concentration, Tc (Minutes)**: The time of concentration for each watershed was determined by finding the time necessary for runoff to travel from the hydraulically most distant point in the watershed to the point of concentration. Time of concentrations were calculated using TR-55 worksheets with a minimum recommended time of concentration of 6 minutes.

SCS 24-Hour Storm Type: For the greater New England region, a Type III storm is recommended for drainage calculations.

Rainfall Precipitation: Rainfall precipitations for the 2, 10, and 25 year, 24-hour storm events were obtained using Figure B-1 from Technical Paper No. 40 (TP-40) Rainfall Frequency Atlas of the United States and are as follows for Wayland, MA:

2-year storm event: 3.1 inches 10-year storm event: 4.5 inches

As per Town of Wayland Wetland regulations, a 24 hour storm event with a depth of 1 inch will be required as part of the analysis. The minimum depth for a 24 hour 100 year storm depth will be 7 inches as per the Town of Wayland Wetland Regulations.

An on-site subsurface storm drainage collection system was designed to carry a minimum 25-year storm event through the site using the Hydraflow Storm Sewers Program. This program uses the Rational Method for estimating runoff and storm drainage pipes are sized based on calculated flows using Manning's Equation (See Appendix C for Pipe Sizing Calculations).

The site was divided into sub-areas, each contributing runoff to an individual catch basin inlet or roof drain. A value for area, time of concentration, and a runoff coefficient were calculated for each contributing sub-area. Rainfall intensities are calculated based on regional precipitation values provided in Technical Memorandum Hydro-35.

#### 3.0 Existing Soils

The Soil Survey of Middlesex County, Massachusetts, completed by the National Resource Conservation Service (NRCS, formerly the Soil Conservation Service), was reviewed for general information on the soils within the site area (See Figure 3 - Soil Map). The mapped soils shown within the site limits are identified as follows:

Soil Number	Soil Type	Hydrologic Group
255A 256A 602 36A	Windsor Loamy Sand, 0 to 3 percent slopes Deerfield Loamy Sand, 0 to 3 percent slopes Urban Land Saco Mucky Silt Loam, 0 to 1 percent slopes	A B Null
3011	Suco Wideky Shi Louin, o to 1 percent stopes	D

The soils surrounding the mapped urban land consists primarily of consist primarily of Windsor Loamy Sand (hydrologic group A). Borings done on site in the areas mapped as urban land indicate that the soils consist of loamy sands which are consistent with hydrologic group A soils. For hydrology calculations, the soils mapped as urban land was assumed to be hydrologic group A soil.

#### 4.0 Existing Conditions Runoff

The existing topography and land cover has been analyzed and 6 watershed areas were delineated with a combined area of  $\pm 43$  acres for stormwater runoff. The watershed areas consist of the project site as well as any contributing off-site areas that direct runoff onto the project site. Six analysis points corresponding to the watersheds were used for determining the existing runoff leaving the site. The same points were used for the proposed runoff leaving the site to ensure that there will be no increase in peak runoff rates for the 2, 10, 25, and 100 year, 24 hour design storms (see Figure 4 – Pre-development watershed).

<u>Watershed EW-1</u> is 17.05 acres and is predominantly impervious, consisting of the 6.26 acres of roof area of the existing Raytheon building, sidewalks and landscaped islands, a small area of runoff from offsite and a large portion of the existing parking lot. Runoff currently travels east to west and is captured by a number of catch basins and piped to a 36"combined sewer and storm pipe which discharges into the large wetland.

<u>Watershed EW-2</u> has an area of 4.11 acres and consists mainly of paved areas with a small portion of a landscaped island and the roof runoff from the existing 10,500 square foot building. Runoff sheet flows northwest and is collected by catch basins and discharges directly into the wetland through an existing 18" storm pipe.

<u>Watershed EW-3</u> is 12.31 acres in size and groundcover is predominantly previous consisting of grass, brush, woods and a small portion of the existing paved area. Runoff from this watershed is overland flow,

which travels east to west directly into the existing wetland without any stormwater collection system capturing the runoff.

<u>Watershed EW-4</u> has an area of 1.58 acres and is made up of the existing paved area and grass lawn area. Runoff currently sheet flows southwest into two ponds which are separated by the existing driveway entrance from Route 20 (Boston Post Road). These two ponds are connected by a culvert under the driveway and have no outlet, therefore during a large storm event, the ponds will overflow into Route 20.

Watershed EW-5 (EW-5A and EW-5B) is 8.08 acres in size and is consists of pavement, lawn, and brush areas. The existing Wayland Wastewater treatment plant is part of this watershed and a portion of runoff from off-site areas contributes to this watershed. Runoff from Watershed EW-5A is sheet flow which eventually flows north to the Wayland Commons property. Runoff from EW-5B consists of the Route 27 driveway and off-site areas. This runoff is collected in swales and a drainage culvert and flows to the wetland system north of the site.

<u>Watershed EW-6</u> has an area of 2.83 acres, and is made up of the existing access driveway at the south east corner of the Raytheon Building and thick brush along the south east corner of the property. Runoff sheet flows south directly into the existing wetland located at the south-east corner of the property.

**Table 4.1**: The existing peak rates of stormwater runoff leaving the site are summarized as follows:

Analysis Point	Contributing Watersheds	1-inch (CFS)	2-YEAR (CFS	10-YEAR (CFS)	100-YEAR (CFS)	Receiving Watershed
Analysis Point 1 Existing 36" CMP combined storm/sewer culvert at Wetland	EW-1	3.3	31.7	53.1	91.5	Wetland
Analysis Point 2 Existing Culvert at Wetland	EW-2	<1.0	8.3	13.8	23.8	system west of site
Analysis Point 3	EW-1, EW2, EW-3	4.1	39.4	66.8	120.3	
Analysis Point 4 Overland flow southeast to Boston Post Road	EW-4	0	0	0	0	Boston Post Road
Analysis Point 5 Overland flow to wetland system north of site	EW-5	0	<1.0	1.4	8.6	Wetland system north of site
Analysis Point 6 Overland flow southeast to existing wetland	EW-6	0	1.1	4.0	10.7	Wetland system south of site

#### 5.0 Proposed Conditions Runoff

The proposed site was also broken up into five watersheds with a combined area of ±43 acres (See Figure 5 – Proposed Watershed Plan). Proposed watershed 4 was removed as there is no proposed runoff to Route 20. Catch basins and water quality swales and rain gardens have been designed to collect runoff and discharge into bio-retention basins which will discharge the runoff at a controlled rate. Six analysis points corresponding to the watersheds were used for determining the proposed runoff that will leave the site. The same points were used for the existing runoff leaving the site to ensure that there will be no increase in runoff rates for the 2, 10, 25, and 100 year, 24 hour design storms. A curve number and time of concentration were calculated for each watershed using Soil Conservation Service TR-55 methods (See Appendix C for Proposed Conditions Hydrology Calculations). The recommended minimum time of concentration of 6 minutes was used for watersheds PW-1, PW-2B, PW-5B, and PW-6B.

<u>Watershed PW-1</u> (PW-1A and PW-1B) is made up of the proposed paved areas, sidewalks, landscaped islands, roof areas and the proposed town green area. The runoff from this watershed is collected in catch basins rain gardens and water quality swales and directed to Basin 2. Runoff from Basin 2 is discharged into the large wetland located at the western portion of the site (Analysis Point 1).

<u>Watershed PW-2</u> is made up of paved areas, sidewalks, one roof area and landscaped areas located at the southern portion of the site. The total area of the watershed is 1.31 acres. The majority of the runoff from PW-2 is collected in the existing basins located at the southern portion of the site adjacent to Rte 20. Runoff is discharged into an existing drain pipe which discharges into the large wetland located at the western portion of the site (Analysis Point 2).

<u>Watershed PW-3</u> is made up of undisturbed area consisting of grass, brush, and woods. The total area of the watershed is 7.25 acres and is located in the western portion of the site. Runoff from this watershed will continue to runoff as it does presently, which is overland flow into the large wetland (Analysis Point 3).

<u>Watershed PW-5</u> (PW-5A and 5B) is made up of paved areas and grass. The total area of all watersheds in PW-5 is 10.46 acres and is located at the north-eastern portion of the site. Runoff from PW-5A is predominately sheet flow into catch basins and a water quality swale which outlets into Bio-retention Basin 3.Infiltration is the primary outlet for both basins, however overflow from these basins is discharged into the large wetland area located at the western part of the site. Runoff from PW-5B is collected in swales and catch basins and is discharged to the wetland system via overland flow and a drainage culvert.

<u>Watershed PW-6</u> (PW-6A and PW-6B) is made up of paved areas, landscaped islands, rooftop, sidewalks and a small undisturbed area consisting of grass, and brush. The total area of all watersheds in PW-6 is 1.95 acres and it is located at the south eastern portion of the site. Runoff from the developed area (PW-6A) is collected in roof drains and catch basins, which outlet into Bio-retention basin 4. Runoff from the undisturbed area (PW-6B) will continue to runoff as it does presently, which is overland flow into the small wetland located at the south eastern corner of the property.

**Table 5.1:** The peak rates of stormwater runoff leaving the site from the proposed development are summarized as follows:

Analysis Point	Contributing Watersheds	1 inch (CFS)	2-YEAR (CFS)	10-YEAR (CFS)	100- YEAR (CFS)	Receiving Watershed
Analysis Point 1 Existing CMP combined storm/sewer culvert at Wetland	PW-1	0	16.0	33.4	64.8	Wetland
Analysis Point 2 Existing Culvert at Wetland	PW-2	0	0	0	<1.0	system west of site
Analysis Point 3 Wetlands West of Site	PW-1, PW2, PW-3	0	16.6	39.3	80.6	
Analysis Point 4 Overland flow southeast to Boston Post Road	PW-4	0	0	0	0	Boston Post Road
Analysis Point 5 Overland flow north to Wayland Meadows	PW-5	0	<1.0	1.0	2.0	Wetland system north of site
Analysis Point 6 Overland flow southeast to existing wetland	PW-6	0	1.1	2.7	5.2	Wetland system south of site

#### 6.0 Water Quality

Stormwater quality control will be achieved through a program of Best Management Practices (BMP's). The proposed development is designed to achieve a minimum 80% total suspended solids (TSS) removal in accordance with the MA DEP Stormwater Management Standards. The development includes high-intensity use parking lots, which classify the development as a land use with higher potential pollutant loads, and the water quality volume required to be treated is equal to 1-inch times the total impervious area. The total impervious area of the site is 22.2 acres, and the water quality volume is as follows:

$$WQV = \left(22.2 \, acres\right) \left(\frac{43,560 \, sf}{1 \, acre}\right) \left(1 \, inch\right) \left(\frac{1 \, ft}{12 \, inches}\right) = 80,586 \, cf$$

The stormwater management system has been designed to treat the entire water quality volume. This is indicated in Table 5.1, which shows that the entire 1-inch storm is treated and there is no discharge to any of the analysis points for the 1-inch storm.

Effective stormwater management practices include the use of curbing along all pavement edges, catch basins with deep sumps and hoods, and detention/infiltration devices, which will treat stormwater runoff from the proposed development and minimize potential indirect, long term impacts to down gradient resources. In addition, a sediment and erosion control plan will be implemented to protect these areas during and after construction of the proposed development.

#### Catch Basins:

The proposed catch basins will be equipped with deep sumps and hoods. The sumps capture sediments and coarse particles, and the hoods prevent hydrocarbons and other floatable debris from entering the drainage system, which will improve the performance of subsequent BMP's. The sump will be no less than 4' in depth and a regular maintenance schedule will be followed. A regular inspection and cleaning will ensure optimal effectiveness.

#### Water Quality Swales:

Water quality swales are used to provide peak runoff control as well as enhanced water quality. The swales will be planted with grass on the bottom and sides to slow the runoff velocity and filter pollutants. Runoff volume is controlled by reducing runoff velocity and promoting infiltration. Pollutant removal is achieved through sedimentation, filtration, nutrient uptake, and infiltration.

#### Rain Gardens:

Rain gardens are low impact development techniques that serve to promote groundwater recharge and enhance water quality. The proposed rain gardens will be located within parking lot areas and will be planted with a combination of grasses, perennials, shrubs, and wetland plantings. Rain gardens are designed to maximize the removal of pollutants from stormwater runoff through vegetation uptake, retention, and settling.

#### **Bioretention Basins:**

Bioretention basins are low impact development techniques that serve to promote groundwater recharge and enhance water quality, but at a larger scale and are designed to handle larger runoff volumes than rain gardens. The proposed bioretention basins are essentially extended detention basins that are planted with a combination of grasses, perennials, shrubs, and wetland plantings, and are designed to maximize the removal of pollutants from stormwater runoff through vegetation uptake, retention, and settling.

#### TSS Removal:

There are three different treatment paths that stormwater runoff can take before being discharged off-site. The first two paths include runoff that is collected in water quality swales and rain gardens. All runoff collected in water quality swales and rain gardens will then be routed to a bioretention basin. The third path is runoff that is collected in catch basins. This runoff will then be routed to either a water quality swale or forebay for pretreatment and then to a bioretention basin. Parking lot sweeping will also be provided, but no credit for sweeping was included in TSS removal calculations.

The following tables provide the design TSS removal rates as set forth in the Massachusetts Stormwater Management Policy for the various BMP's utilized in this project:

Runoff collected in rain gardens:

BMP	Design Rate	Cumulative TSS Removal
Rain Garden	80%	80%
Bio-retention Basin	80%	96%

Runoff collected in water quality swales:

BMP	Design Rate	Cumulative TSS Removal
Water Quality Swale	70%	70%
Bio-retention Basin	80%	94%

#### Runoff collected in catch basins:

BMP	Design Rate	Cumulative TSS Removal
Catch Basin w/ Deep Sumps (off-line only)	25%	25%
Forebay (pretreatment calculation only)	25%	44%
Bio-retention Basin (including forebay)	80%	89%

As shown above, the proposed development will provide water quality treatment that exceeds 80% TSS removal required by the DEP Stormwater Management Standards. In addition, 44% TSS removal will be achieved prior to stormwater entering the bio-retention basins.

#### 7.0 Groundwater Recharge

Groundwater recharge for the proposed development will be provided in accordance with the MA DEP Stormwater Management Standards. These standards require that the annual recharge from the post-development site shall approximate the annual recharge from pre-development site conditions based on soil types. For hydrologic group A soil types, the volume that is required to be recharged is equal to 0.60 inches multiplied by the increase in impervious area. The proposed development is located within hydrologic group A soils, therefore the volume required to be recharged is as follows:

Existing impervious area: ±21.8 acres Proposed impervious area: ±22.2 acres Increase in impervious area: ±0.4 acres

$$V = 0.4 \ acres \ x \ 0.60 \ inches \ x \ \frac{43,560 \ s.f.}{1 \ acre} \ x \ \frac{1 \ ft.}{12 \ inches} = 871 \ cubic \ ft.$$

The stormwater management system will provide groundwater recharge through the use of water quality swales, rain gardens, and bio-retention basins. The static method was used to calculate recharge volumes for the bio-retention basins by determining the volume of water stored in each basin that is located below the system outlet. The recharge volumes provided in each BMP are as follows:

BMP	Recharge Volume
	(cubic ft.)
Basin 1	3,750
Basin 2	8,540
Basin 3	4,230
Basin 4	1,660
Total	18,180

As shown above, the proposed development provides a recharge volume of 18,180 cubic ft. which exceeds the 871 cubic feet required by DEP Stormwater Management Standards.

#### 72-hour Drawdown Analysis:

As per the Massachusetts Stormwater Handbook, the recharge volume should infiltrate within 72 hours. The drawdown analysis for the static method is performed by selecting a Rawls infiltration rate (provided by the Handbook) for the existing site soils in the areas where recharge is proposed. Based on the site soils and review of the Rawls table, an infiltration rate of 2.41 inches per hour was used to determine the drawdown time for the infiltration BMP's. The drawdown time is calculated as follows:

$$DrawdownTime = \frac{\text{Re } ch \arg e Volume}{\left(Infiltration \, Rate\right)\left(1 \, ft \, / \, 12 \, inches\right)\left(Bottom \, Area\right)}$$

The following table shows the calculated drawdown rate for the infiltration BMP's:

BMP	Recharge Volume (c.f.)	Bottom Area (s.f.)	Drawdown Time (hrs)
Basin 1	3,750	1,828	10.2
Basin 2	8,540	1,690	25.2
Basin 3	4,230	2,172	9.7
Basin 4	1,660	458	18.0

As indicated above, the recharge volume will infiltrate within 72 hours for the proposed infiltration BMP's.

#### 8.0 Summary

The stormwater collection and management system for the proposed development will provide mitigation of post-development stormwater runoff conditions utilizing a combination of detention basins and Low Impact Development techniques and "Best Management Practices" to reduce pollutant loadings within the stormwater prior to discharging it off site.

As shown in the following summary, the proposed stormwater management system has been designed to match or reduce post development peak discharges to less than the existing rates for all modeled storms.

Analysis Point 1 - Existing 36" CMP Summary Existing vs. Proposed Peak Discharge Rates			
Storm Event:			
1-inch	3.3	0	
2-year	31.7	16.0	
10-year	53.1	33.4	
100-year	91.5	64.8	

Analysis	<b>Analysis Point 2 – Existing Culvert</b>		
	(Behind Daycare Building)		
Summary I	Summary Existing vs. Proposed Peak Discharge Rates		
Storm Event:	Existing Flow (CFS)	Proposed Flow (CFS)	
1-inch	<1.0	0	
2-year	8.3	0	
10-year	13.8	0	
100-year	23.8	<1.0	

Analysis Point 3 –Wetlands West of Site		
(Sudbury River)		
Summary Existing vs. Proposed Peak Discharge Rates		
		Proposed Flow (CFS)
1-inch	4.1	0
2-year 39.4		16.6
10-year 66.8 39.3		39.3
100-year 120.3 80.6		80.6

Analysis Point 4 - Boston Post Road Summary Existing vs. Proposed Peak Discharge Rates		
Storm Event:	Existing Flow (CFS)	Proposed Flow (CFS)
1-inch	0	0
2-year	0	0
10-year	0	0
100-year	0	0

Analysis Point 5 – Wetlands North of Site		
(Adjacent to Wayland Meadows)		
Summary Existing vs. Proposed Peak Discharge Rates		
Storm Event:	Existing Flow (CFS)	Proposed Flow (CFS)
1-inch	0	0
2-year	<1.0	<1.0
10-year	1.4	1.0
100-year	8.6	2.0

Analysis Point 6 – Wetlands South of Site Summary Existing vs. Proposed Peak Discharge Rates		
Storm Event: Existing Flow (CFS) Proposed Flow (CFS)		
1-inch	0	0
2-year	1.1	1.1
10-year	4.0	2.7
100-year	10.7	5.2

#### 9.0 Compliance with Stormwater Management Standards

**Standard 1:** No new stormwater conveyances (e.g. outfalls) may discharge untreated stormwater directly to or cause erosion in wetlands or waters of the Commonwealth.

The stormwater management system has been designed such that no new stormwater conveyances will discharge untreated stormwater directly to or cause erosion in wetlands or waters of the Commonwealth. Refer to section 6.0 Water Quality for more information about stormwater treatment.

**Standard 2:** Stormwater management systems shall be designed so that post-development peak discharge rates do not exceed pre-development peak discharge rates.

The stormwater management system has been designed to mitigate peak rates of runoff for the 1-inch, 2-year, 10-year, 25-year, and 100-year 24 hour storm event. Please refer to the tables in Section 9 Summary and the Hydrology Calculations for more information.

**Standard 3:** Loss of annual recharge to groundwater shall be eliminated or minimized through the use of infiltration measures including environmentally sensitive site design, low impact development techniques, stormwater best management practices, and good operation and maintenance.

Groundwater recharge will be provided through the use of low-impact development techniques such as rain gardens, water quality swales, and bioretention basins. Please refer to section 7.0 Groundwater Recharge for supporting calculations.

**Standard 4:** Stormwater management systems shall be designed to remove 80% of the average annual post-construction load of Total Suspended Solids (TSS).

The stormwater management system has been designed to remove 80% of the average annual post-construction load of TSS. BMP's have been sized to handle the water quality volume, and pretreatment is provided prior to infiltration in accordance with the Stormwater Management Handbook. Please refer to section 6.0 Water Quality for additional information and supporting calculations. A long term pollution prevention plan identifying suitable practices for source control and pollution prevention is included in Appendix E.

**Standard 5:** For land uses with higher potential pollutant loads, source control and pollution prevention shall be implemented in accordance with the Massachusetts Stormwater Handbook to eliminate or reduce the discharge of stormwater runoff from such land uses to the maximum extent practicable.

The project is considered a land use with higher potential pollutant loads due to the parking lots with high-intensity useand is subject to the requirement of Standard 5. BMP's selected for the project are consistent with the stormwater BMP's determined by DEP to be suitable for land uses with higher potential pollutant loads (i.e. deep sump catch basins, forebays, water quality swales, rain gardens, and bioretention areas).

**Standard 6:** Stormwater discharges within the Zone II or Interim Wellhead Protection Area of a public water supply, and stormwater discharges near or to any other critical area, require the use of the specific

source control and pollution prevention measures and the specific structural stormwater best management practices determined by the Department to be suitable for managing discharges to such areas, as provided in the Massachusetts Stormwater Handbook.

The project will be discharging treated stormwater to a Zone II and is subject to the requirements of Standard 6. BMP's selected for the project are consistent with the stormwater BMP's determined by DEP to be suitable for discharge to a Zone II (i.e. deep sump catch basins, forebays, water quality swales, rain gardens, and bioretention areas) and 44% TSS removal will be achieved prior to any infiltration BMP.

**Standard** 7: A redevelopment project is required to meet the following Stormwater Management Standards only to the maximum extent practicable: Standard 2, Standard 3, and the pretreatment and structural best management practice requirements of Standards 4, 5, and 6. Existing stormwater discharges shall comply with Standard 1 only to the maximum extent practicable. A redevelopment project shall also comply with all other requirements of the Stormwater Management Standards and improve existing conditions.

Although the project is a redevelopment and only required to meet the Stormwater Management Standards to the maximum extent practicable, the stormwater management system has been designed to meet all of the Stormwater Management Standards.

**Standard 8:** A plan to control construction-related impacts including erosion, sedimentation and other pollutant sources during construction and land disturbance activities (construction period erosion, sedimentation, and pollution prevention plan) shall be developed and implemented.

A plan to control construction-related impacts including erosion, sedimentation, and other pollutant sources during construction has been included in Appendix F.

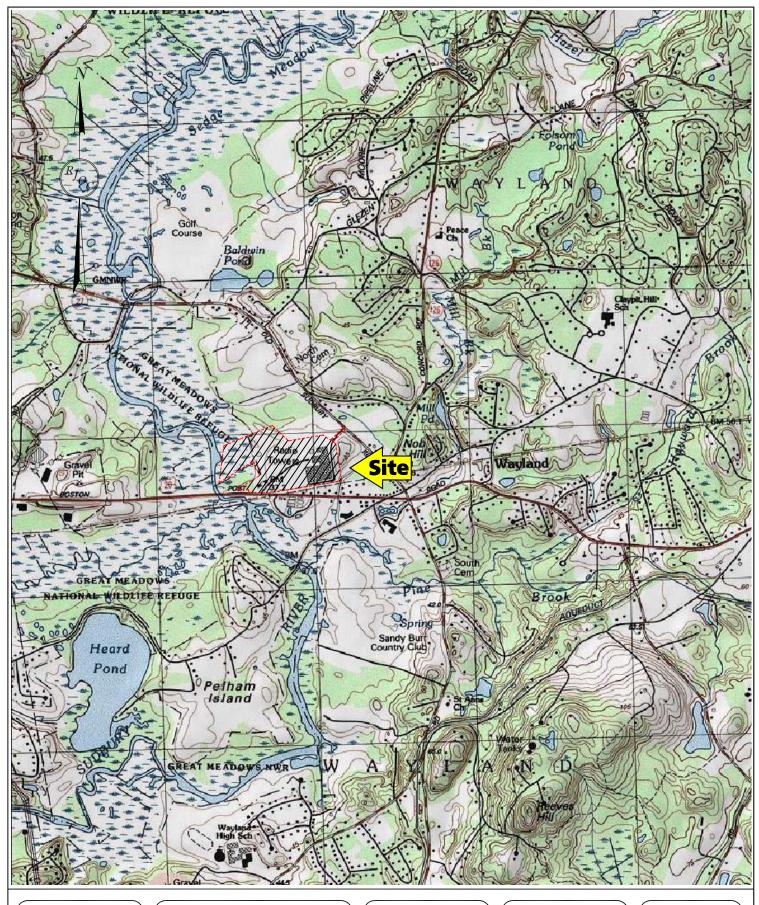
**Standard 9**: A long-term operation and maintenance plan shall be developed and implemented to ensure that stormwater management systems function as designed.

A long term operation and maintenance plan is included in Appendix G.

Standard 10: All illicit discharges to the stormwater management system are prohibited.

There will not be any illicit discharges to the stormwater management system.

### II. FIGURES



Designed by: Drawn by: Checked by: 1"=1,200' Scale: Date: 5/08/2007

Prepared by:

RJO'CONNELL
& ASSOCIATES, INC.

Civil Engineers & Land Planners 600 UNICORN PARK DRIVE WOBURN, MA 01801 781-938-0570 / FAX: 781-938-0031

Project Name:

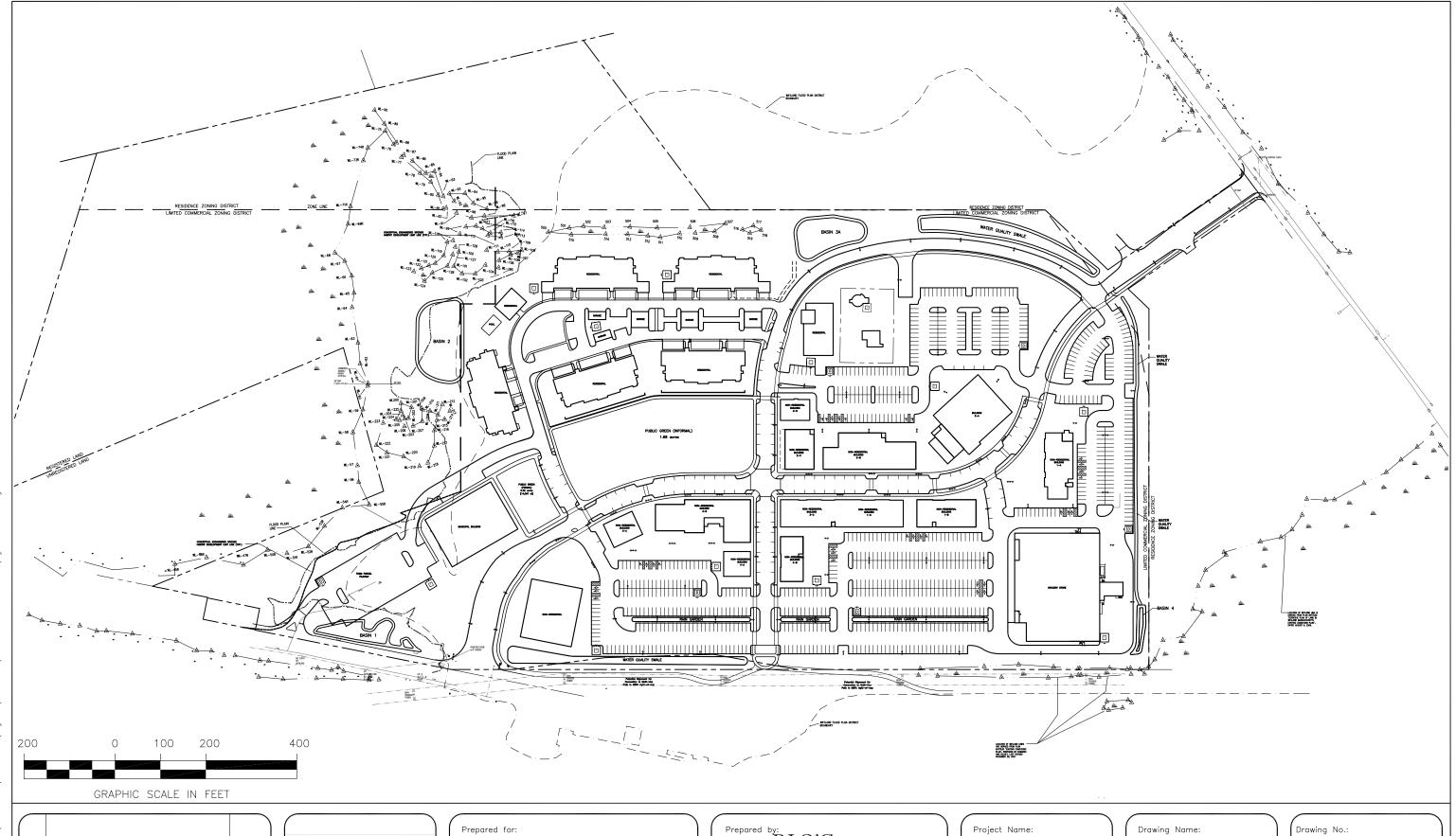
WAYLAND TOWN **CENTER** WAYLAND, MA

Drawing Name: SITE LOCUS MAP

WAYLAND, MA **QUADRANGLE MAP DATE: 1977**  Drawing No.:

FIG. 1

Project No.: 06032



No. Revision Date

Designed by:	SS
Drawn by:	LT/WJH
Checked by:	SS
Scale:	1"=200'
Date:	06/02/2008

#### TWENTY WAYLAND, LLC

45 BROAD STREET, 4TH FLOOR BOSTON, MA 02109

# Prepared by: RJ O'CONNELL & ASSOCIATES, INC

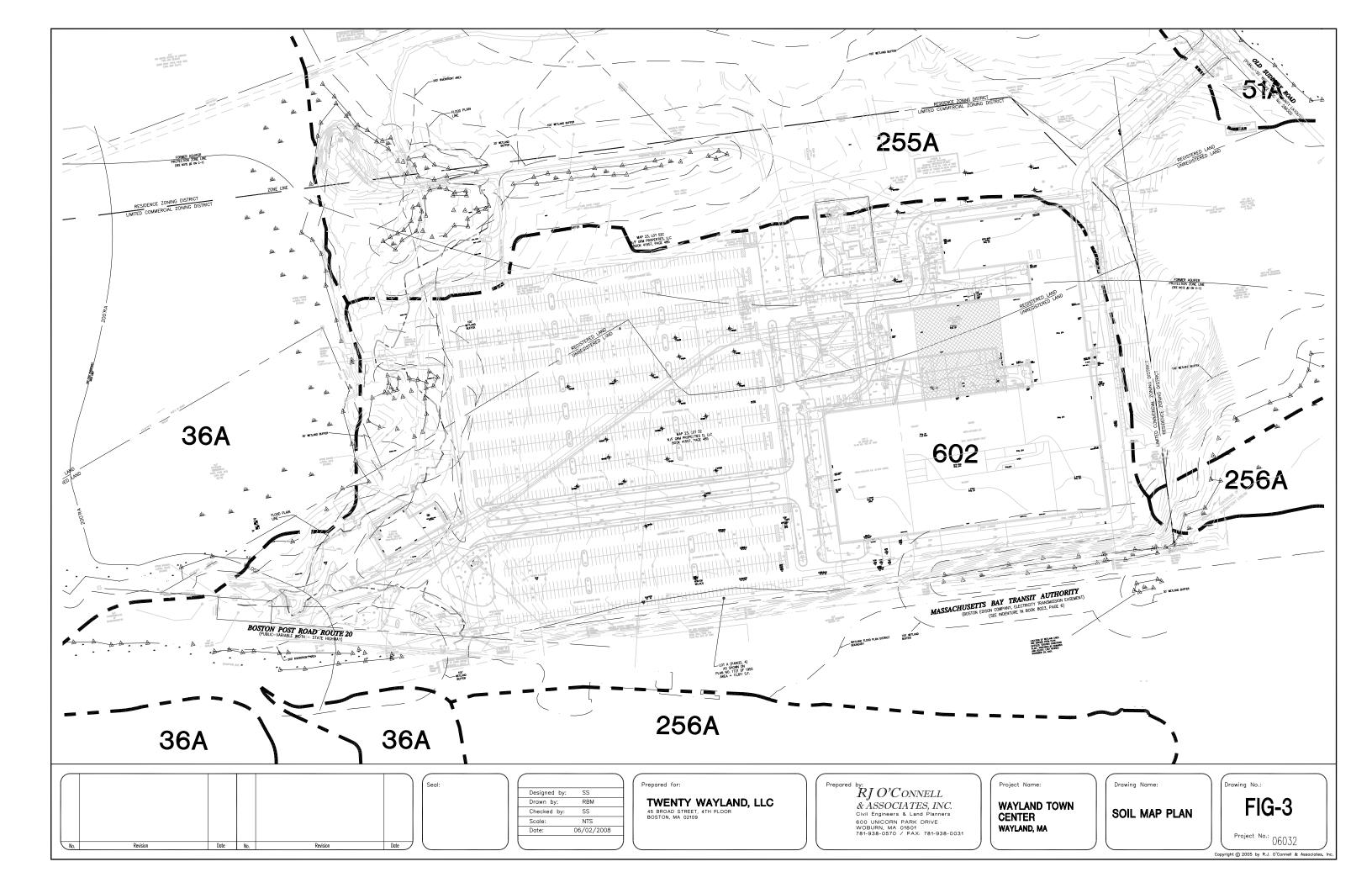
& ASSOCIATES, INC.
Civil Engineers & Land Planners
600 UNICORN PARK DRIVE
WOBURN, MA 01801
781-938-0570 / FAX: 781-938-0031

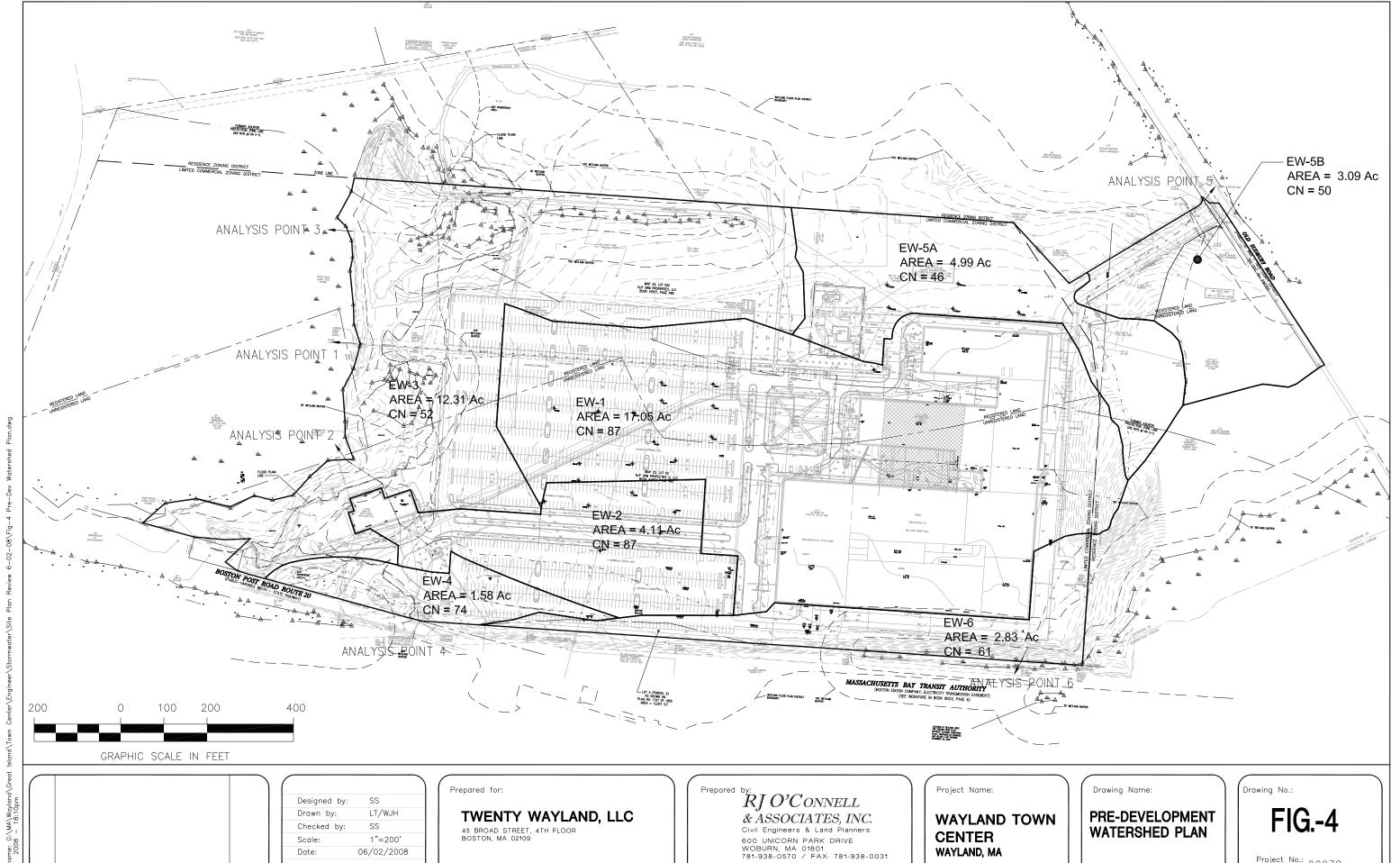
WAYLAND TOWN CENTER WAYLAND, MA SITE PLAN

FIG.-2

oject No.: 06032

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WAYLAND, MA

Project No.: 06032

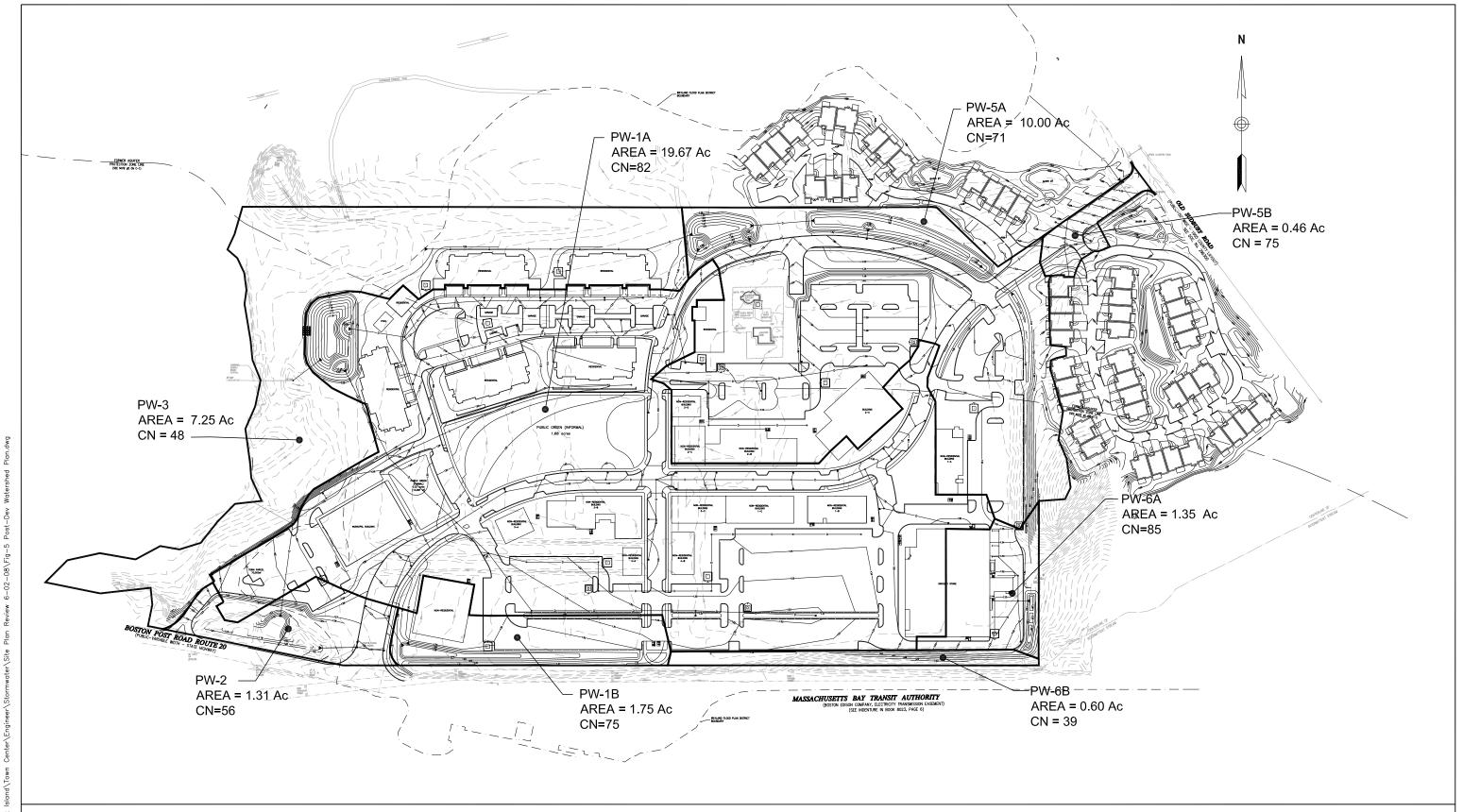
Copyright © 2005 by R.J. O'Connell & Associates, Inc.

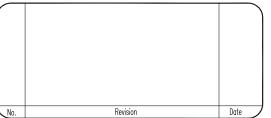
Revision

06/02/2008

Date:

Date





Designed by:	SS
Drawn by:	LT/WJH
Checked by:	SS
Scale:	N.T.S.
Date:	06/02/08

Prepared for:

#### TWENTY WAYLAND, LLC

45 BROAD STREET, 4TH FLOOR BOSTON, MA 02109

# Prepared by: RJO'CONNELL TES IN & ASSOCIATES, INC. Civil Engineers & Land Planners

80 MONTVALE AVE STONEHAM, MA 02180 781-938-0570 / FAX: 781-938-0031

Project Name:

**WAYLAND TOWN** CENTER WAYLAND, MA

Drawing Name:

POST-DEVELOPMENT WATERSHED PLAN

Drawing No.:

FIG.-5

Project No.: 06032

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### III. APPENDICES

#### APPENDIX A: CHECKLIST FOR STORMWATER REPORT



### Massachusetts Department of Environmental Protection

Bureau of Resource Protection - Wetlands Program

# **Checklist for Stormwater Report**

#### A. Introduction

Important: When filling out forms on the computer, use only the tab key to move your cursor - do not use the return key.





A Stormwater Report must be submitted with the Notice of Intent permit application to document compliance with the Stormwater Management Standards. The following checklist is NOT a substitute for the Stormwater Report (which should provide more substantive and detailed information) but is offered here as a tool to help the applicant organize their Stormwater Management documentation for their Report and for the reviewer to assess this information in a consistent format. As noted in the Checklist, the Stormwater Report must contain the engineering computations and supporting information set forth in Volume 3 of the Massachusetts Stormwater Handbook. The Stormwater Report must be prepared and certified by a Registered Professional Engineer (RPE) licensed in the Commonwealth.

The Stormwater Report must include:

- The Stormwater Checklist completed and stamped by a Registered Professional Engineer (see page 2) that certifies that the Stormwater Report contains all required submittals. This Checklist is to be used as the cover for the completed Stormwater Report.
- Applicant/Project Name
- Project Address
- Name of Firm and Registered Professional Engineer that prepared the Report
- Long-Term Pollution Prevention Plan required by Standards 4-6
- Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan required by Standard 8<sup>2</sup>
- Operation and Maintenance Plan required by Standard 9

In addition to all plans and supporting information, the Stormwater Report must include a brief narrative describing stormwater management practices, including environmentally sensitive site design and LID techniques, along with a diagram depicting runoff through the proposed BMP treatment train. Plans are required to show existing and proposed conditions, identify all wetland resource areas, NRCS soil types, critical areas, Land Uses with Higher Potential Pollutant Loads (LUHPPL), and any areas on the site where infiltration rate is greater than 2.4 inches per hour. The Plans shall identify the drainage areas for both existing and proposed conditions at a scale that enables verification of supporting calculations.

As noted in the Checklist, the Stormwater Management Report shall document compliance with each of the Stormwater Management Standards as provided in the Massachusetts Stormwater Handbook. The soils evaluation and calculations shall be done using the methodologies set forth in Volume 3 of the Massachusetts Stormwater Handbook.

To ensure that the Stormwater Report is complete, applicants are required to fill in the Stormwater Report Checklist by checking the box to indicate that the specified information has been included in the Stormwater Report. If any of the information specified in the checklist has not been submitted, the applicant must provide an explanation. The completed Stormwater Report Checklist and Certification must be submitted with the Stormwater Report.

<sup>&</sup>lt;sup>1</sup> The Stormwater Report may also include the Illicit Discharge Compliance Statement required by Standard 10. If not included in the Stormwater Report, the Illicit Discharge Compliance Statement must be submitted prior to the discharge of stormwater runoff to the post-construction best management practices.

<sup>&</sup>lt;sup>2</sup> For some complex projects, it may not be possible to include the Construction Period Erosion and Sedimentation Control Plan in the Stormwater Report. In that event, the issuing authority has the discretion to issue an Order of Conditions that approves the project and includes a condition requiring the proponent to submit the Construction Period Erosion and Sedimentation Control Plan before commencing any land disturbance activity on the site.



### Massachusetts Department of Environmental Protection

Bureau of Resource Protection - Wetlands Program

# **Checklist for Stormwater Report**

#### B. Stormwater Checklist and Certification

The following checklist is intended to serve as a guide for applicants as to the elements that ordinarily need to be addressed in a complete Stormwater Report. The checklist is also intended to provide conservation commissions and other reviewing authorities with a summary of the components necessary for a comprehensive Stormwater Report that addresses the ten Stormwater Standards.

*Note:* Because stormwater requirements vary from project to project, it is possible that a complete Stormwater Report may not include information on some of the subjects specified in the Checklist. If it is determined that a specific item does not apply to the project under review, please note that the item is not applicable (N.A.) and provide the reasons for that determination.

A complete checklist must include the Certification set forth below signed by the Registered Professional Engineer who prepared the Stormwater Report.

#### Registered Professional Engineer's Certification

I have reviewed the Stormwater Report, including the soil evaluation, computations, Long-term Pollution Prevention Plan, the Construction Period Erosion and Sedimentation Control Plan (if included), the Long-term Post-Construction Operation and Maintenance Plan, the Illicit Discharge Compliance Statement (if included) and the plans showing the stormwater management system, and have determined that they have been prepared in accordance with the requirements of the Stormwater Management Standards as further elaborated by the Massachusetts Stormwater Handbook. I have also determined that the information presented in the Stormwater Checklist is accurate and that the information presented in the Stormwater Report accurately reflects conditions at the site as of the date of this permit application.

Registered Professional Engineer Block and Signature



Challe a- Willy 6/02/08
Signature and Date

#### Checklist

	<b>pject Type:</b> Is the application for new development, redevelopment, or a mix of new and evelopment?
	New development
$\boxtimes$	Redevelopment
	Mix of New Development and Redevelopment



#### Massachusetts Department of Environmental Protection

Bureau of Resource Protection - Wetlands Program

## **Checklist for Stormwater Report**

## Checklist (continued) LID Measures: Stormwater Standards require LID measures to be considered. Document what environmentally sensitive design and LID Techniques were considered during the planning and design of the project: ☐ No disturbance to any Wetland Resource Areas ☐ Site Design Practices (e.g. clustered development, reduced frontage setbacks) Reduced Impervious Area (Redevelopment Only) Minimizing disturbance to existing trees and shrubs ☐ LID Site Design Credit Requested: Credit 1 Credit 2 Credit 3 Use of "country drainage" versus curb and gutter conveyance and pipe ⊠ Bioretention Cells (includes Rain Gardens) ☐ Constructed Stormwater Wetlands (includes Gravel Wetlands designs) Treebox Filter ☐ Grass Channel ☐ Green Roof Other (describe): Standard 1: No New Untreated Discharges No new untreated discharges Outlets have been designed so there is no erosion or scour to wetlands and waters of the Commonwealth

Supporting calculations specified in Volume 3 of the Massachusetts Stormwater Handbook included.



# **Massachusetts Department of Environmental Protection**Bureau of Resource Protection - Wetlands Program

# **Checklist for Stormwater Report**

Checklist	(continued)
-----------	-------------

Sta	ndard 2: Peak Rate Attenuation		
	Standard 2 waiver requested because the project is located in land subject to coastal storm flowage and stormwater discharge is to a wetland subject to coastal flooding.  Evaluation provided to determine whether off-site flooding increases during the 100-year 24-hour storm.		
	Calculations provided to show that post-development peak discharge rates do not exceed pre- development rates for the 2-year and 10-year 24-hour storms. If evaluation shows that off-site flooding increases during the 100-year 24-hour storm, calculations are also provided to show that post-development peak discharge rates do not exceed pre-development rates for the 100-year 24- hour storm.		
Sta	ındard 3: Recharge		
	Soil Analysis provided.		
$\boxtimes$	Required Recharge Volume calculation provided.		
	Required Recharge volume reduced through use of the LID site Design Credits.		
$\boxtimes$	Sizing the infiltration, BMPs is based on the following	ng method: Check the method used.	
		☐ Dynamic Field <sup>1</sup>	
	Runoff from all impervious areas at the site dischar	ging to the infiltration BMP.	
$\boxtimes$	Runoff from all impervious areas at the site is <i>not</i> d are provided showing that the drainage area contribution generate the required recharge volume.		
$\boxtimes$	Recharge BMPs have been sized to infiltrate the Re	equired Recharge Volume.	
	Recharge BMPs have been sized to infiltrate the Reextent practicable for the following reason:	equired Recharge Volume <i>only</i> to the maximum	
	☐ Site is comprised solely of C and D soils and/or	bedrock at the land surface	
	M.G.L. c. 21E sites pursuant to 310 CMR 40.00	000	
	☐ Solid Waste Landfill pursuant to 310 CMR 19.0	00	
	Project is otherwise subject to Stormwater Man practicable.	agement Standards only to the maximum extent	
$\boxtimes$	Calculations showing that the infiltration BMPs will	drain in 72 hours are provided.	
	Property includes a M.G.L. c. 21E site or a solid wa	iste landfill and a mounding analysis is included.	

<sup>&</sup>lt;sup>1</sup> 80% TSS removal is required prior to discharge to infiltration BMP if Dynamic Field method is used.



## **Massachusetts Department of Environmental Protection**Bureau of Resource Protection - Wetlands Program

## **Checklist for Stormwater Report**

_	
C	hecklist (continued)
Sta	andard 3: Recharge (continued)
	The infiltration BMP is used to attenuate peak flows during storms greater than or equal to the 10-year 24-hour storm and separation to seasonal high groundwater is less than 4 feet and a mounding analysis is provided.
	Documentation is provided showing that infiltration BMPs do not adversely impact nearby wetland resource areas.
Sta	andard 4: Water Quality
	e Long-Term Pollution Prevention Plan typically includes the following: Good housekeeping practices; Provisions for storing materials and waste products inside or under cover; Vehicle washing controls; Requirements for routine inspections and maintenance of stormwater BMPs; Spill prevention and response plans; Provisions for maintenance of lawns, gardens, and other landscaped areas; Requirements for storage and use of fertilizers, herbicides, and pesticides; Pet waste management provisions; Provisions for operation and management of septic systems; Provisions for solid waste management; Snow disposal and plowing plans relative to Wetland Resource Areas; Winter Road Salt and/or Sand Use and Storage restrictions; Street sweeping schedules; Provisions for prevention of illicit discharges to the stormwater management system; Documentation that Stormwater BMPs are designed to provide for shutdown and containment in the event of a spill or discharges to or near critical areas or from LUHPPL; Training for staff or personnel involved with implementing Long-Term Pollution Prevention Plan; List of Emergency contacts for implementing Long-Term Pollution Prevention Plan. A Long-Term Pollution Prevention Plan is attached to Stormwater Report and is included as an attachment to the Wetlands Notice of Intent. Treatment BMPs subject to the 44% TSS removal pretreatment requirement and the one inch rule for calculating the water quality volume are included, and discharge:  is within the Zone II or Interim Wellhead Protection Area  is near or to other critical areas  is within solls with a rapid infiltration rate (greater than 2.4 inches per hour)  involves runoff from land uses with higher potential pollutant loads.
	The Required Water Quality Volume is reduced through use of the LID site Design Credits.
$\boxtimes$	Calculations documenting that the treatment train meets the 80% TSS removal requirement and, if applicable, the 44% TSS removal pretreatment requirement, are provided.



# **Massachusetts Department of Environmental Protection**Bureau of Resource Protection - Wetlands Program

## **Checklist for Stormwater Report**

Checklist (continued)

Sta	andard 4: Water Quality (continued)
$\boxtimes$	The BMP is sized (and calculations provided) based on:
	☐ The ½" or 1" Water Quality Volume or
	☐ The equivalent flow rate associated with the Water Quality Volume and documentation is provided showing that the BMP treats the required water quality volume.
	The applicant proposes to use proprietary BMPs, and documentation supporting use of proprietary BMP and proposed TSS removal rate is provided. This documentation may be in the form of the propriety BMP checklist found in Volume 2, Chapter 4 of the Massachusetts Stormwater Handbook and submitting copies of the TARP Report, STEP Report, and/or other third party studies verifying performance of the proprietary BMPs.
	A TMDL exists that indicates a need to reduce pollutants other than TSS and documentation showing that the BMPs selected are consistent with the TMDL is provided.
Sta	ndard 5: Land Uses With Higher Potential Pollutant Loads (LUHPPLs)
	The NPDES Multi-Sector General Permit covers the land use and the Stormwater Pollution Prevention Plan (SWPPP) has been included with the Stormwater Report.  The NPDES Multi-Sector General Permit covers the land use and the SWPPP will be submitted <i>prior</i> .
	to the discharge of stormwater to the post-construction stormwater BMPs.
	The NPDES Multi-Sector General Permit does <i>not</i> cover the land use.
	LUHPPLs are located at the site and industry specific source control and pollution prevention measures have been proposed to reduce or eliminate the exposure of LUHPPLs to rain, snow, snow melt and runoff, and been included in the long term Pollution Prevention Plan.
	All exposure has been eliminated.
	All exposure has <i>not</i> been eliminated and all BMPs selected are on MassDEP LUHPPL list.
$\boxtimes$	The LUHPPL has the potential to generate runoff with moderate to higher concentrations of oil and grease (e.g. all parking lots with >1000 vehicle trips per day) and the treatment train includes an oil grit separator, a filtering bioretention area, a sand filter or equivalent.
Sta	ndard 6: Critical Areas
$\boxtimes$	The discharge is near or to a critical area and the treatment train includes only BMPs that MassDEP has approved for stormwater discharges to or near that particular class of critical area.
$\boxtimes$	Critical areas and BMPs are identified in the Stormwater Report.



#### Massachusetts Department of Environmental Protection

Bureau of Resource Protection - Wetlands Program

## **Checklist for Stormwater Report**

### Checklist (continued)

Redevelopment Project

Standard 7: Redevelopments and Other Projects Subject to the Standards only to the maximum extent practicable
 ☑ The project is subject to the Stormwater Management Standards only to the maximum Extent Practicable as a:
 ☐ Limited Project
 ☐ Small Residential Projects: 5-9 single family houses or 5-9 units in a multi-family development provided there is no discharge that may potentially affect a critical area.
 ☐ Small Residential Projects: 2-4 single family houses or 2-4 units in a multi-family development with a discharge to a critical area
 ☐ Marina and/or boatyard provided the hull painting, service and maintenance areas are protected from exposure to rain, snow, snow melt and runoff
 ☐ Bike Path and/or Foot Path

☐ Redevelopment portion of mix of new and redevelopment.
 ☐ Certain standards are not fully met (Standard No. 1, 8, 9, and 10 must always be fully met) and an explanation of why these standards are not met is contained in the Stormwater Report.

The project involves redevelopment and a description of all measures that have been taken to improve existing conditions is provided in the Stormwater Report. The redevelopment checklist found in Volume 2 Chapter 3 of the Massachusetts Stormwater Handbook may be used to document that the proposed stormwater management system (a) complies with Standards 2, 3 and the pretreatment and structural BMP requirements of Standards 4-6 to the maximum extent practicable and (b) improves existing conditions.

#### Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan must include the following information:

- Narrative;
- · Construction Period Operation and Maintenance Plan;
- Names of Persons or Entity Responsible for Plan Compliance;
- Construction Period Pollution Prevention Measures;
- Erosion and Sedimentation Control Plan Drawings;
- Detail drawings and specifications for erosion control BMPs, including sizing calculations;
- Vegetation Planning;
- Site Development Plan;
- Construction Sequencing Plan;
- Sequencing of Erosion and Sedimentation Controls;
- Operation and Maintenance of Erosion and Sedimentation Controls;
- Inspection Schedule;
- Maintenance Schedule;
- Inspection and Maintenance Log Form.
- A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan containing the information set forth above has been included in the Stormwater Report.



### Massachusetts Department of Environmental Protection

Bureau of Resource Protection - Wetlands Program

## **Checklist for Stormwater Report**

Checklist (continued) Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control (continued) ☐ The project is highly complex and information is included in the Stormwater Report that explains why it is not possible to submit the Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan with the application. A Construction Period Pollution Prevention and Erosion and Sedimentation Control has not been included in the Stormwater Report but will be submitted before land disturbance begins. ☐ The project is **not** covered by a NPDES Construction General Permit. ☐ The project is covered by a NPDES Construction General Permit and a copy of the SWPPP is in the Stormwater Report. The project is covered by a NPDES Construction General Permit but no SWPPP been submitted. The SWPPP will be submitted BEFORE land disturbance begins. Standard 9: Operation and Maintenance Plan The Post Construction Operation and Maintenance Plan is included in the Stormwater Report and includes the following information: Name of the stormwater management system owners; Party responsible for operation and maintenance; Schedule for implementation of routine and non-routine maintenance tasks: ☐ Plan showing the location of all stormwater BMPs maintenance access areas; Description and delineation of public safety features; Estimated operation and maintenance budget; and Operation and Maintenance Log Form. The responsible party is **not** the owner of the parcel where the BMP is located and the Stormwater Report includes the following submissions: A copy of the legal instrument (deed, homeowner's association, utility trust or other legal entity) that establishes the terms of and legal responsibility for the operation and maintenance of the project site stormwater BMPs; A plan and easement deed that allows site access for the legal entity to operate and maintain BMP functions. Standard 10: Prohibition of Illicit Discharges ☐ An Illicit Discharge Compliance Statement is attached; ☐ NO Illicit Discharge Compliance Statement is attached but will be submitted *prior to* the discharge of any stormwater to post-construction BMPs.

### APPENDIX B: EXISTING CONDITIONS HYDROLOGY CALCULATIONS

Runoff Curve Numbers and Runoff Time of Concentration Pond Reports Hydrograph Plots (2, 10, 25, 100 year storm events)

Project:

**Wayland Town Center** 

By:

CAD Date 06/02/08

Location:

Wayland, MA

Checked:

Date

Check One:

Present

Existing Watershed 1 (EW-1)

#### 1. Runoff curve number (CN)

Soil Name and	Cover Description		CN		Area	Product of
Hydrologic Group (appendix A)	(cover type, treatment, and hydrologic conditions percent impervious unconnected/connected impervious area ratio)	Table 2-2	Figure 2-3	Figure 2-4	X acres	CN x Area
А	Grass - good	39			3.24	126.36
Α	Impervious (pavement, roof)	98			13.81	1353.38
А						0.00
						0.00
						0.00
				,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		0.00
						0.00
						0.00
				li.		0.00
Use only one CN source per line.		Total	s =		17.05	1479.74

CN (weighted) =

total product total area

86.7883

Use CN=

87

#### 2. Runoff

	-	Storm #1	Storm #2	Storm #3	
Frequency	yr.	2	10	100	
Rainfall, P (24 hour)	in.	3.30	4.70	6.90	
Runoff, Q i	in.	2.00	3.29	5.38	

Project:

**Wayland Town Center** 

By:

**CAD** Date 06/02/08

Location:

Wayland, MA

Checked:

Date

Check One:

Present

**Existing Watershed 2 (EW-2)** 

#### 1. Runoff curve number (CN)

Soil Name and	Cover Description		CN		Area	Product of
Hydrologic Group (appendix A)	(cover type, treatment, and hydrologic conditions percent impervious unconnected/connected impervious area ratio)	Table 2-2	Figure 2-3	Figure 2-4	X acres	CN x Area
А	Grass - good	39			0.80	31.20
Α	Impervious (pavement, roof)	98			3.31	324.38
						0.00
						0.00
						0.00
						0.00
						0.00
						0.00
	- International Control of the Contr					0.00
Use only one CN source per line.		Total	s =		4.11	355.58

#### 2. Runoff

CN (weighted) =

	-	Storm #1	Storm #2	Storm #3	
Frequency	yr.	2	10	100	
Rainfall, P (24 hour)	in.	3.30	4.70	6.90	
Runoff, Q	in.	2.00	3.29	5.38	

86.5158

Use CN=

87

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

total product

total area

Project:

**Wayland Town Center** 

Ву:

CAD Date 06/02/08

Location:

Wayland, MA

Checked:

Date

Check One:

Present

**Existing Watershed 3 (EW-3)** 

#### 1. Runoff curve number (CN)

Soil Name and	Cover Description		CN		Area	Product of
Hydrologic Group (appendix A)	(cover type, treatment, and hydrologic conditions percent impervious unconnected/connected impervious area ratio)	Table 2-2	Figure 2-3	Figure 2-4	X acres	CN x Area
A	Grass - good	39			9.42	367.38
Α	Impervious (pavement, roof)	98			2.32	227.36
Α	Gravel	76			0.44	33.44
A	Wetland	83			0.13	10.79
						0.00
						0.00
					1	0.00
						0.00
						0.00
Use only one CN source per line.		Total	s =	ļ	12.31	638.97

CN (weighted) =

total product total area

51.9066

Use CN=

52

#### 2. Runoff

	,	Storm #1	Storm #2	Storm #3	
Frequency	yr.	2	10	100	
Rainfall, P (24 hour)	in.	3.30	4.70	6.90	
Runoff, Q	in.	0.20	0.67	1.79	

Project:

**Wayland Town Center** 

By:

CAD Date 06/02/08

Location:

Wayland, MA

Checked:

Date

Check One:

**Present** 

**Existing Watershed 4 (EW-4)** 

#### 1. Runoff curve number (CN)

Soil Name and	Cover Description		CN		Area	Product of
Hydrologic Group (appendix A)	(cover type, treatment, and hydrologic conditions percent impervious unconnected/connected impervious area ratio)	Table 2-2	Figure 2-3	Figure 2-4	X acres	CN x Area
А	Grass - good	39			0.63	24.57
А	Impervious (pavement, roof)	98			0.95	93.10
						0.00
						0.00
	==:					0.00
						0.00
						0.00
						0.00
						0.00
Use only one CN source per line.		Totals =			1.58	117.67

CN (weighted) =

total product total area

74.4747

Use CN=

74

#### 2. Runoff

		Storm #1	Storm #2	Storm #3	
Frequency	yr.	2	10	100	
Rainfall, P (24 hour)	in,	3.30	4.70	6.90	
Runoff, Q	in.	1.10	2.13	3.96	

Project:

**Wayland Town Center** 

By:

CAD Date 06/02/08

Location:

Wayland, MA

Checked:

Date

Check One:

Present

Existing Watershed 5A (EW-5A)

#### 1. Runoff curve number (CN)

Soil Name and	1		CN		Area	Product of
Hydrologic Group (appendix A)	(cover type, treatment, and hydrologic conditions percent impervious unconnected/connected impervious area ratio)		Figure 2-3	Figure 2-4	X acres	CN x Area
Α	Grass - good	39			4.43	172.77
А	Impervious (pavement, roof)	98			0.56	54.88
						0.00
						0.00
						0.00
						0.00
						0.00
	ve					0.00
						0.00
Use only one CN source per line.		Total	s =	,	4.99	227.65

CN (weighted) =

total product total area

45.6212

Use CN=

46

#### 2. Runoff

	ř	Storm #1	Storm #2	Storm #3	
Frequency	yr.	2	10	100	
Rainfall, P (24 hour)	in.	3.30	4.70	6.90	
Runoff, Q	in.	0.07	0.39	1.27	

Project: Wayland Town Center By: CAD Date 06/02/08

Location: Wayland, MA Checked: Date

Check One: Present Existing Watershed 5B (EW-5B)

#### 1. Runoff curve number (CN)

Soil Name and	Cover Description		CN		Area	Product of
Hydrologic Group (appendix A)	(cover type, treatment, and hydrologic conditions percent impervious unconnected/connected impervious area ratio)	Table 2-2	Figure 2-3	Figure 2-4	X acres mi² %	CN x Area
Α	Grass - good	39			2.53	98.67
Α	Impervious (pavement, roof)	98			0.56	54.88
						0.00
						0.00
						0.00
						0.00
						0.00
						0.00
						0.00
Use only one	CN source per line.	Total	s =		3.09	153.55

CN (weighted) = total product total area 49.6926 Use CN= 50

#### 2. Runoff

	-	Storm #1	Storm #2	Storm #3	
Frequency	yr.	2	10	100	
Rainfall, P (24 hour)	in.	3.30	4.70	6.90	
Runoff, Q	in.	0.15	0.57	1.61	

Project:

**Wayland Town Center** 

By:

CAD Date 06/02/08

Location:

Wayland, MA

Checked:

Date

Check One:

Present

Existing Watershed 6 (EW-6)

#### 1. Runoff curve number (CN)

Soil Name and	Cover Description		CN		Area	Product of
Hydrologic Group (appendix A)	(cover type, treatment, and hydrologic conditions percent impervious unconnected/connected impervious area ratio)	Table 2-2	Figure 2-3	Figure 2-4	X acres mi² %	CN x Area
А	Grass - good	39			1.79	69.81
A	Impervious (pavement, roof)	98			1.04	101.92
						0.00
						0.00
						0.00
						0.00
						0.00
						0.00
						0.00
Use only one	CN source per line.	Total	s =		2.83	171.73

### 2. Runoff

CN (weighted) =

	-	Storm #1	Storm #2	Storm #3	
Frequency	yr.	2	10	100	
Rainfall, P (24 hour)	in.	3.30	4.70	6.90	
Runoff, Q	in.	0.49	1.19	2.63	

60.6820

Use CN=

61

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

total product

total area

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Hyd. No. 1

EW-1 (PT. 1)

<u>Description</u>	A		<u>B</u>		<u>C</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.200 = 136.0 = 3.10 = 14.70		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	= 7.22	+	0.00	+	0.00	=	7.22
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 60.00 = 0.50 = Paved = 1.44		0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00		
Travel Time (min)	= 0.70	+	0.00	+	0.00	=	0.70
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	= 7.00 = 4.71 = 1.00 = 0.015 = 12.95 = 1800.0		0.00 0.00 0.00 0.015 0.00 0.0		0.00 0.00 0.00 0.015 0.00 0.0		
Travel Time (min)	= 2.32	+	0.00	+	0.00	=	2.32
Total Travel Time, Tc							

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### Hyd. No. 2

EW-2 (PT. 2)

<u>Description</u>	<u>A</u>		<u>B</u>		<u>c</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.011 = 100.0 = 3.10 = 0.50		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	= 2.14	+	0.00	+	0.00	=	2.14
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 673.0 = 1.20 = Pave = 2.23		0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00		
Travel Time (min)	= 5.04	+	0.00	+	0.00	=	5.04
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	= 1.22 = 1.96 = 1.00 = 0.015 = 7.23 = 275.0		0.00 0.00 0.00 0.015 0.00 0.0		0.00 0.00 0.00 0.015 0.00 0.0		
Travel Time (min)	= 0.63	+	0.00	+	0.00	=	0.63
Total Travel Time. Tc							

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### Hyd. No. 3

EW-3

<u>Description</u>		<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	=	0.200 100.0 3.10 0.50		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	=	21.82	+	0.00	+	0.00	=	21.82
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	=	972.00 1.30 Unpaved 1.84	d	148.00 2.70 Unpave 2.65	d	0.00 0.00 Paved 0.00		
Travel Time (min)	=	8.81	+	0.93	+	0.00	=	9.74
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	= =	0.00 0.00 0.00 0.015 0.00 0.0		0.00 0.00 0.00 0.015 0.00 0.0		0.00 0.00 0.00 0.015 0.00 0.0		
Travel Time (min)	=	0.00	+	0.00	+	0.00	=	0.00
Total Travel Time, Tc								31.55 min

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### Hyd. No. 5

EW-4

Description		A		<u>B</u>		<u>C</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	=	0.200 100.0 3.10 2.50		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	=	11.46	+	0.00	+	0.00	=	11.46
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)  Travel Time (min)	=======================================	100.00 3.50 Unpaved 3.02 <b>0.55</b>	i +	0.00 0.00 Unpave 0.00	ed +	0.00 0.00 Paved 0.00	=	0.55
, ,				0.00				
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	=======================================	0.00 0.00 0.00 0.015 0.00 0.0		0.00 0.00 0.00 0.015 0.00 0.0		0.00 0.00 0.00 0.015 0.00 0.0		
Travel Time (min)	=	0.00	+	0.00	+	0.00	=	0.00
Total Travel Time, Tc							12.01 min	

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Hyd. No. 7

EW-5A

<u>Description</u>		<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	=	0.200 100.0 3.10 1.50		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	=	14.06	+	0.00	+	0.00	=	14.06
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)  Travel Time (min)	=	130.00 2.50 Unpaved 2.55 <b>0.85</b>	<del>.</del>	0.00 0.00 Paved 0.00	+	0.00 0.00 Paved 0.00	=	0.85
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	=======================================	0.00 0.00 0.00 0.015 0.00 0.0		0.00 0.00 0.00 0.015 0.00 0.0		0.00 0.00 0.00 0.015 0.00 0.0		
Travel Time (min)	=	0.00	+	0.00	+	0.00	=	0.00
Total Travel Time, Tc								14.91 min

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### Hyd. No. 8

E-5B

<u>Description</u>	<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0. = 10 = 3. = 1.	00.0 10	0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	= 10	6.53 +	0.00	+	0.00	=	16.53
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 5.	npaved	0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00		
Travel Time (min)	= 1.	64 +	0.00	+	0.00	=	1.64
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	= 0. = 0. = 0. = 0. = 0.	00 00 015 00	0.00 0.00 0.00 0.015 0.00		0.00 0.00 0.00 0.015 0.00 0.0		
Travel Time (min)	= 0.	00 +	0.00	+	0.00	=	0.00
Total Travel Time, Tc							

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### Hyd. No. 10

EW-6 (PT. 6)

<u>Description</u>		<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>
Sheet Flow Manning's n-value	=	0.240		0.011		0.011		
Flow length (ft) Two-year 24-hr precip. (in)	=	100.0		0.0		0.0		
Land slope (%)		6.00		0.00		0.00		0.24
Travel Time (min)	=	9.34	+	0.00	+	0.00	=	9.34
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	=	240.00 0.85 Unpave 1.49	d	0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00		
Travel Time (min)	=	2.69	+	0.00	+	0.00	=	2.69
Channel Flow								
X sectional flow area (sqft)		0.00		0.00		0.00		
Wetted perimeter (ft)		0.00		0.00		0.00		
Channel slope (%)		0.00		0.00		0.00		
Manning's n-value		0.015		0.015		0.015		
Velocity (ft/s)		0.00		0.00		0.00		
Flow length (ft)	_	0.0		0.0		0.0		
Travel Time (min)	=	0.00	+	0.00	+	0.00	=	0.00
Total Travel Time, Tc								12.03 min

### **Pond Report**

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

Tuesday, Jun 3, 2008

#### Pond No. 7 - EX. BASIN

#### **Pond Data**

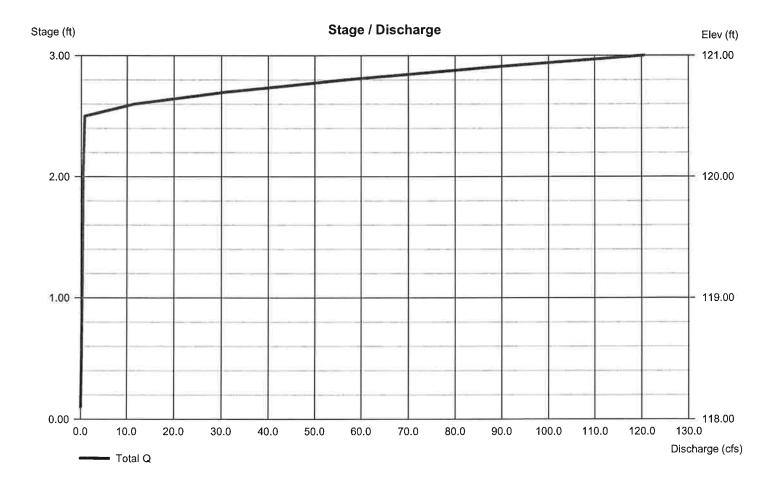
Contours - User-defined contour areas. Average end area method used for volume calculation. Begining Elevation = 118.00 ft

#### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	118.00	1,828	0	0
1.00	119.00	5,668	3,748	3,748
2.00	120.00	8,193	6,931	10,679
3.00	121.00	20,000	14,097	24,775

Culvert / Ori	fice Structı	ures			Weir Structures					
	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]	
Rise (in)	= 0.00	0.00	0.00	0.00	Crest Len (ft)	= 130.00	0.00	0.00	0.00	
Span (in)	= 0.00	0.00	0.00	0.00	Crest El. (ft)	= 120.50	0.00	0.00	0.00	
No. Barrels	= 0	0	0	0	Weir Coeff.	= 2.60	3.33	3.33	3.33	
Invert El. (ft)	= 0.00	0.00	0.00	0.00	Weir Type	= Broad				
Length (ft)	= 0.00	0.00	0.00	0.00	Multi-Stage	= No	No	No	No	
Slope (%)	= 0.00	0.00	0.00	n/a						
N-Value	= .013	.013	.013	n/a						
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 2.400 (by	Contour)			
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00				

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



# Hydrograph Summary Report Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	3.300	1	730	14,107	X <del>amena</del>			EW-1 (PT. 1)
2	SCS Runoff	0.864	1	727	3,257		******		EW-2 (PT. 2)
3	SCS Runoff	0.000	1	n/a	0	123511			EW-3
4	Combine	4.099	1	729	17,364	1, 2, 3		<del></del>	EXIST. TOTAL TO RIVER (PT. 3)
5	SCS Runoff	0.005	1	890	131	123200			EW-4
6	Reservoir	0.000	1	960	0	5	118.01	37.2	EXIST. BASIN (PT. 4)
7	SCS Runoff	0.000	1	n/a	0				EW-5A
8	SCS Runoff	0.000	1	n/a	0	OFFICERS.	*****		E-5B
9	Combine	0.000	1	n/a	0	7, 8	:=V1011=1		E-5A + E-5B (PT. 5)
10	SCS Runoff	0.000	1	n/a	0	******			EW-6 (PT. 6)
11	SCS Runoff	1.436	1	741	9,324				PW-1A
12	SCS Runoff	0.007	1	825	199	024000			PW-1B
13	Reservoir	0.000	1	893	0	12	126.02	61.1	WATER QUALITY SWALE
14	Combine	1.436	1	741	9,324	11, 13	******	( <del>=11212</del> )	TOTAL TO BASIN 2
15	Reservoir	0.000	1	1477	0	14	117.41	3,803	BASIN 2
16	Diversion1	0.289	1	1477	1,526	15			BASIN 2 INFILTRATION
17	Diversion2	0.000	1	n/a	-1,526	15	:=====		BASIN 2 OUTFLOW (PT. 1)
18	SCS Runoff	0.000	1	n/a	0				PW-2
19	Reservoir	0.000	1	n/a	0	18	118.00	0.000	BASIN 1 (PT.2)
20	SCS Runoff	0.000	1	n/a	0	Satress		STREET, STREET	PW-3
21	SCS Runoff	0.009	1	1337	283				PW-5A
22	Reservoir	0.000	1	1254	0	21	126.03	104	BASIN 3
23	Combine	0.000	1	1484	0	15, 19, 22	( <del>satulate</del> )		PROP. TOTAL TO RIVER (PT. 3)
24	SCS Runoff	0.002	1	827	51				PW-5B (PT. 5)
25	SCS Runoff	0.136	1	745	851	X444444		******	PW-6A
26	Reservoir	0.000	1	930	0	25	128.02	235	BASIN 4
27	SCS Runoff	0.000	1	n/a	0				PW-6B
28	Combine	0.000	1	930	0	26, 27	: 2000005:		TOTAL TO PT. 6
Hydro_SPR_REV.gpw			Return Period: 1 Year			Tuesday, c	lun 3, 2008		

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Tuesday, Jun 3, 2008

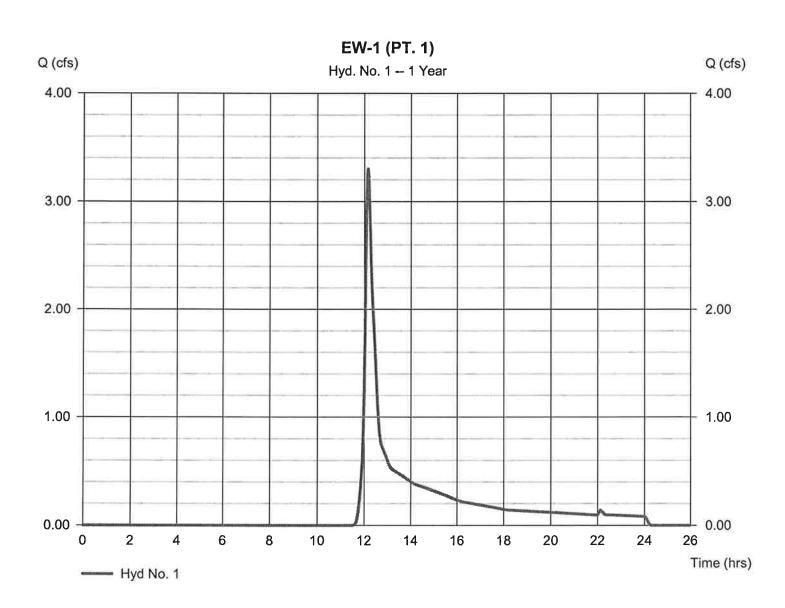
#### Hyd. No. 1

EW-1 (PT. 1)

Hydrograph type= SCS RunoffPeak discharge= 3.300 cfsStorm frequency= 1 yrsTime to peak= 12.17 hrsTime interval= 1 minHyd. volume= 14,107 cuft

Tc method = TR55 Time of conc. (Tc) = 10.23 min
Total precip. = 1.00 in Distribution = Type III
Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(3.240 x 39) + (14.180 x 98)] / 17.050



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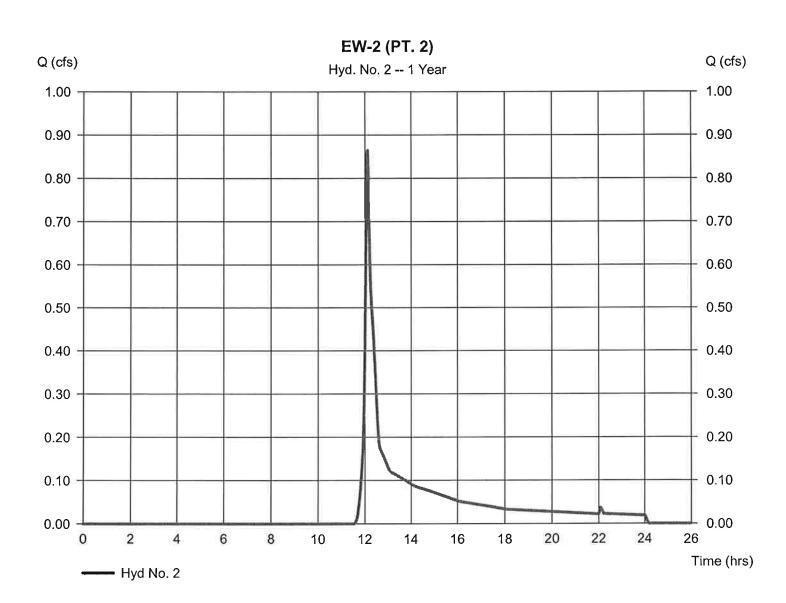
Tuesday, Jun 3, 2008

#### Hyd. No. 2

EW-2 (PT. 2)

Hydrograph type = SCS Runoff Peak discharge = 0.864 cfsStorm frequency = 1 yrs Time to peak = 12.12 hrs Hyd. volume Time interval = 3,257 cuft= 1 min Curve number = 87\*Drainage area = 4.110 acHydraulic length = 0 ftBasin Slope = 0.0 %Time of conc. (Tc) = 7.81 minTc method = TR55 Total precip. = 1.00 inDistribution = Type III = 484 Storm duration Shape factor = 24 hrs

<sup>\*</sup> Composite (Area/CN) =  $[(3.310 \times 98) + (0.800 \times 39)] / 4.110$ 



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Tuesday, Jun 3, 2008

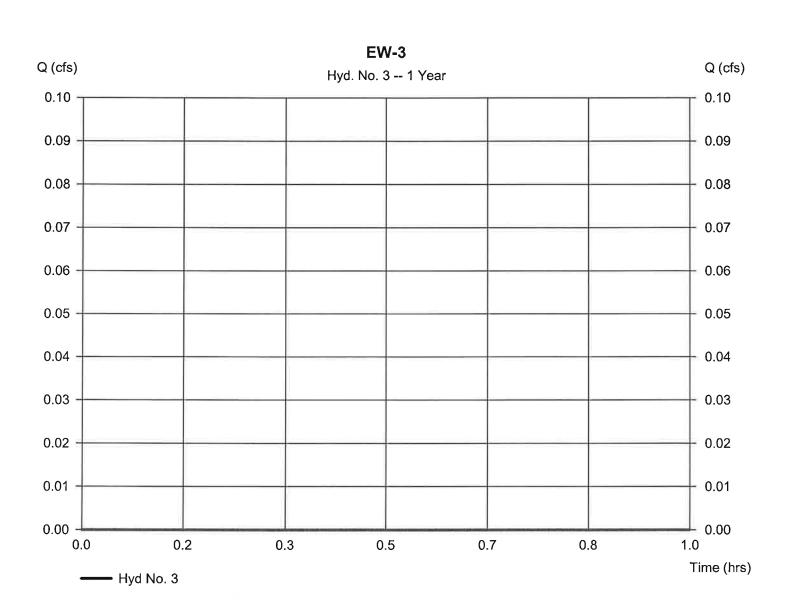
#### Hyd. No. 3

**EW-3** 

Hydrograph type = SCS Runoff
Storm frequency = 1 yrs
Time interval = 1 min
Peak discharge = 0.000 cfs
Time to peak = n/a
Hyd. volume = 0 cuft

Tc method = TR55 Time of conc. (Tc) = 31.55 min
Total precip. = 1.00 in Distribution = Type III
Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(2.280 x 98) + (0.440 x 76) + (0.130 x 83) + (14.090 x 39)] / 12.310



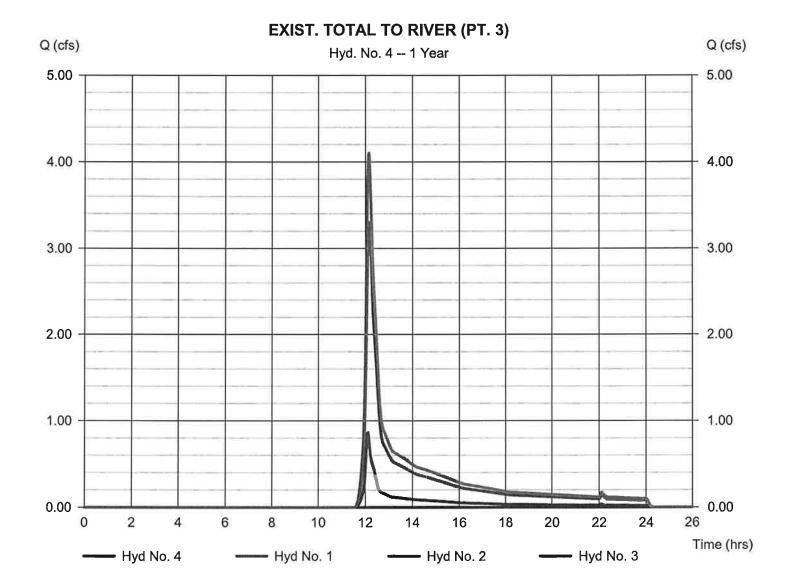
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Tuesday, Jun 3, 2008

#### Hyd. No. 4

EXIST. TOTAL TO RIVER (PT. 3)

Hydrograph type = Combine Storm frequency = 1 yrs Time interval = 1 min Inflow hyds. = 1, 2, 3 Peak discharge = 4.099 cfs Time to peak = 12.15 hrs Hyd. volume = 17,364 cuft Contrib. drain. area= 33.470 ac



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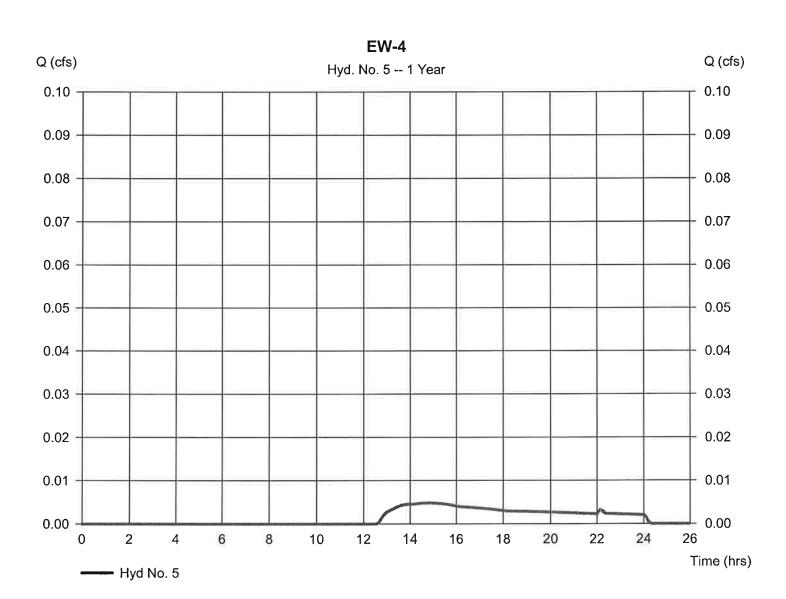
Tuesday, Jun 3, 2008

#### Hyd. No. 5

EW-4

Hydrograph type = SCS Runoff Peak discharge = 0.005 cfsTime to peak  $= 14.83 \, hrs$ Storm frequency = 1 yrsTime interval = 1 min Hyd. volume = 131 cuft Curve number = 74\* Drainage area = 1.580 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method = TR55 Time of conc. (Tc) = 12.01 minDistribution = Type III Total precip. = 1.00 inStorm duration Shape factor = 484 = 24 hrs

<sup>\*</sup> Composite (Area/CN) = [(0.950 x 98) + (0.630 x 39)] / 1.580



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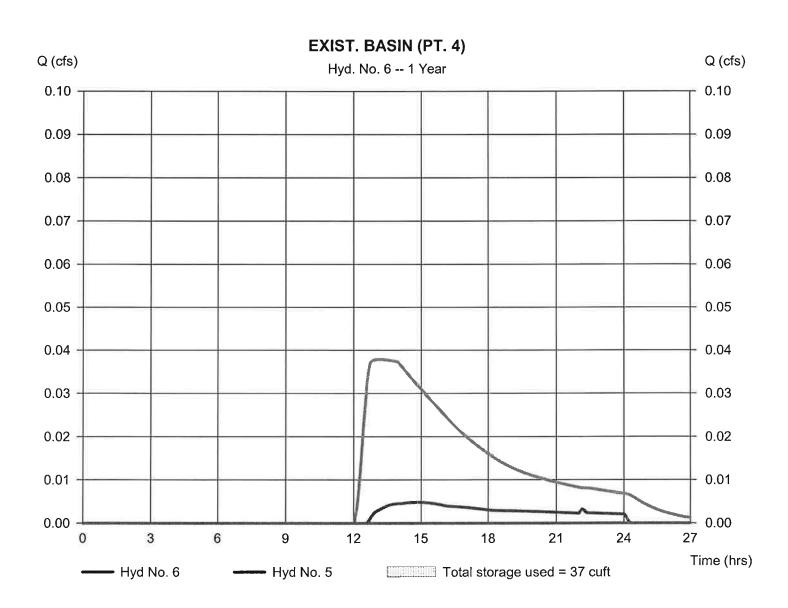
Tuesday, Jun 3, 2008

#### Hyd. No. 6

EXIST. BASIN (PT. 4)

Hydrograph type = Reservoir Peak discharge = 0.000 cfsStorm frequency Time to peak  $= 16.00 \, hrs$ = 1 yrsTime interval = 1 min Hyd. volume = 0 cuftMax. Elevation Inflow hyd. No. = 5 - EW-4 $= 118.01 \, \text{ft}$ Reservoir name Max. Storage = 37 cuft = EX. BASIN

Storage Indication method used. Exfiltration extracted from Outflow.



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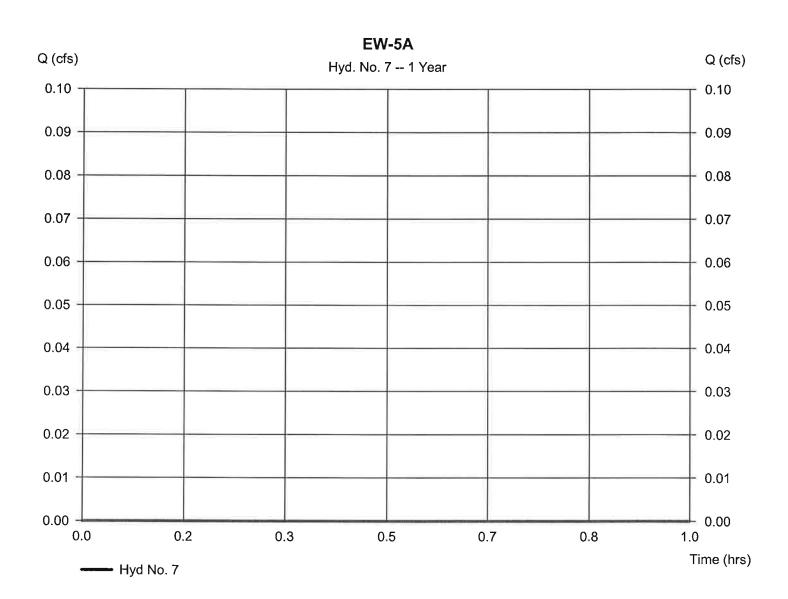
Tuesday, Jun 3, 2008

#### Hyd. No. 7

EW-5A

Hydrograph type = SCS Runoff Peak discharge = 0.000 cfsStorm frequency = 1 yrsTime to peak = n/aTime interval = 1 min Hvd. volume = 0 cuftDrainage area = 4.990 acCurve number = 46\* Basin Slope = 0.0 % Hydraulic length = 0 ftTc method = TR55 Time of conc. (Tc) = 14.91 minTotal precip. = 1.00 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(0.400 x 98) + (4.750 x 39)] / 4.990



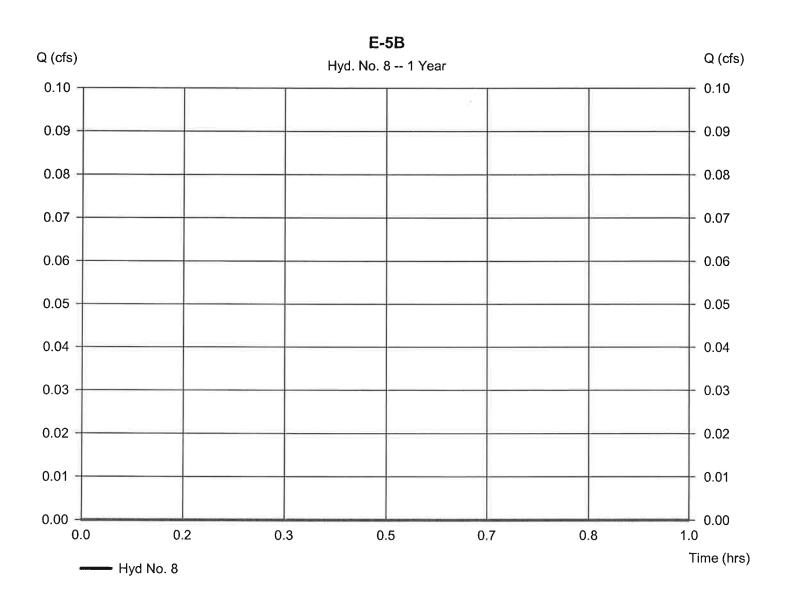
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Tuesday, Jun 3, 2008

#### Hyd. No. 8

E-5B

Hydrograph type = SCS Runoff Peak discharge = 0.000 cfsStorm frequency Time to peak = 1 yrs= n/aTime interval Hyd. volume = 1 min = 0 cuftDrainage area = 3.090 acCurve number = 50 Basin Slope = 0.0 % Hydraulic length = 0 ftTc method = TR55 Time of conc. (Tc) = 18.18 minTotal precip. = 1.00 inDistribution = Type III Storm duration = 24 hrs = 484 Shape factor



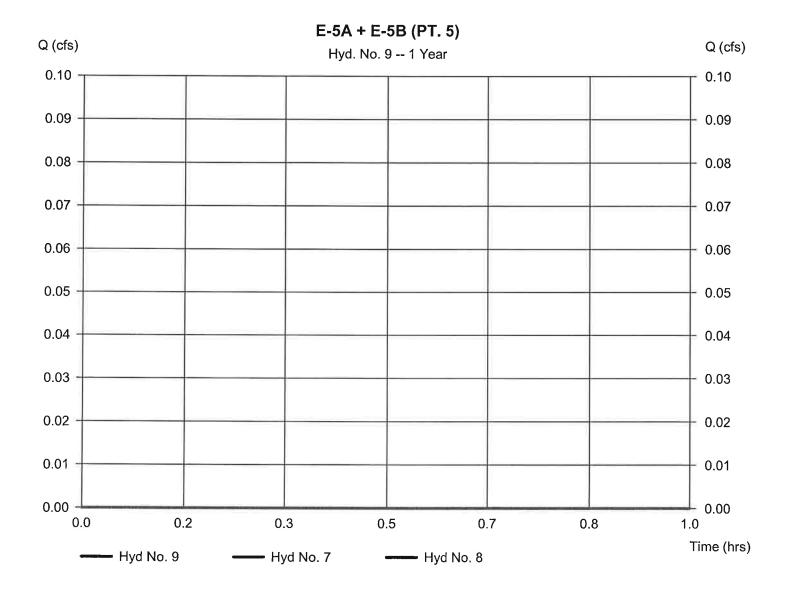
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Tuesday, Jun 3, 2008

#### Hyd. No. 9

E-5A + E-5B (PT. 5)

Hydrograph type = Combine Storm frequency = 1 yrs Time interval = 1 min Inflow hyds. = 7, 8 Peak discharge = 0.000 cfs
Time to peak = n/a
Hyd. volume = 0 cuft
Contrib. drain. area= 8.080 ac



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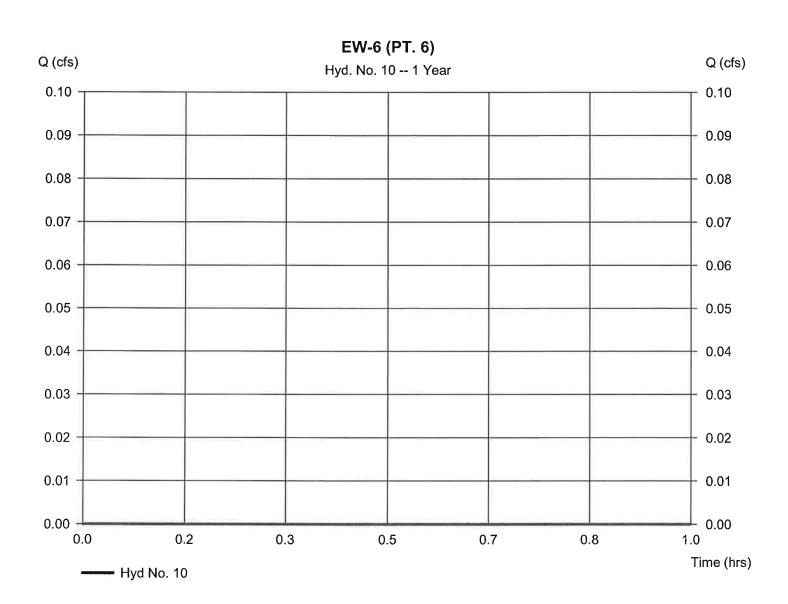
Tuesday, Jun 3, 2008

#### Hyd. No. 10

EW-6 (PT. 6)

Hydrograph type = SCS Runoff Peak discharge = 0.000 cfsStorm frequency = 1 yrsTime to peak = n/aTime interval = 1 min Hvd. volume = 0 cuftDrainage area = 2.830 acCurve number = 61\* Basin Slope = 0.0 % Hydraulic length = 0 ftTc method = TR55 Time of conc. (Tc) = 12.03 minTotal precip. Distribution = 1.00 in= Type II Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(0.660 x 98) + (1.790 x 39)] / 2.830



# Hydrograph Summary Report Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	31.68	1	728	115,076	( <del>*******</del>	•••••	*****	EW-1 (PT. 1)
2	SCS Runoff	8.251	1	726	26,572	054440	S <del>eppende</del> S	<del>201002</del> )	EW-2 (PT. 2)
3	SCS Runoff	0.352	1	773	6,744	X <del></del>		a	EW-3
4	Combine	39.44	1	727	148,392	1, 2, 3	*****	<del>Same</del> i	EXIST. TOTAL TO RIVER (PT. 3)
5	SCS Runoff	1.373	1	730	5,489	Resident	times:	SUPPRISE	EW-4
6	Reservoir	0.000	1	785	0	5	118.60	2,248	EXIST. BASIN (PT. 4)
7	SCS Runoff	0.029	1	922	820		:5000#4		EW-5A
8	SCS Runoff	0.047	1	825	1,209			244.45	E-5B
9	Combine	0.072	1	897	2,029	7, 8	*****		E-5A + E-5B (PT. 5)
10	SCS Runoff	1.095	1	724	4,083	U <del>TSDEAD</del>	=======		EW-6 (PT. 6)
11	SCS Runoff	25.32	1	733	107,826	Patrock		<b>22332</b> 9	PW-1A
12	SCS Runoff	2.087	1	725	6,726				PW-1B
13	Reservoir	0.000	1	734	0	12	126.99	2,879	WATER QUALITY SWALE
14	Combine	25.32	1	733	107,826	11, 13	22002		TOTAL TO BASIN 2
15	Reservoir	16.64	1	745	82,763	14	120.76	25,670	BASIN 2
16	Diversion1	0.601	1	745	16,824	15	T-1112	5 <del>737171</del> 2	BASIN 2 INFILTRATION
17	Diversion2	16.04	1	745	65,940	15			BASIN 2 OUTFLOW (PT. 1)
18	SCS Runoff	0.095	1	765	1,177	*****	HARRING ()	HAMANY.	PW-2
19	Reservoir	0.000	1	798	0	18	118.10	368	BASIN 1 (PT.2)
20	SCS Runoff	0.072	1	893	1,948				PW-3
21	SCS Runoff	5.236	1	743	29,497		*****	paratra)	PW-5A
22	Reservoir	1.175	1	781	8,948	21	128.44	10,868	BASIN 3
23	Combine	16.64	1	745	91,712	15, 19, 22	GAPULEY		PROP. TOTAL TO RIVER (PT. 3)
24	SCS Runoff	0.476	1	727	1,715	******	*****	*****	PW-5B (PT. 5)
25	SCS Runoff	1.697	1	737	8,197		REFERENCE.	HAMARITA	PW-6A
26	Reservoir	1.083	1	752	2,070	25	129.94	2,955	BASIN 4
27	SCS Runoff	0.000	1	n/a	0	******	*****	*****	PW-6B
28	Combine	1.083	1	752	2,070	26, 27	******	mann)	TOTAL TO PT. 6
Hydro_SPR_REV.gpw				Return Period: 2 Year			Tuesday, Jun 3, 2008		

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

Tuesday, Jun 3, 2008

= 484

#### Hyd. No. 1

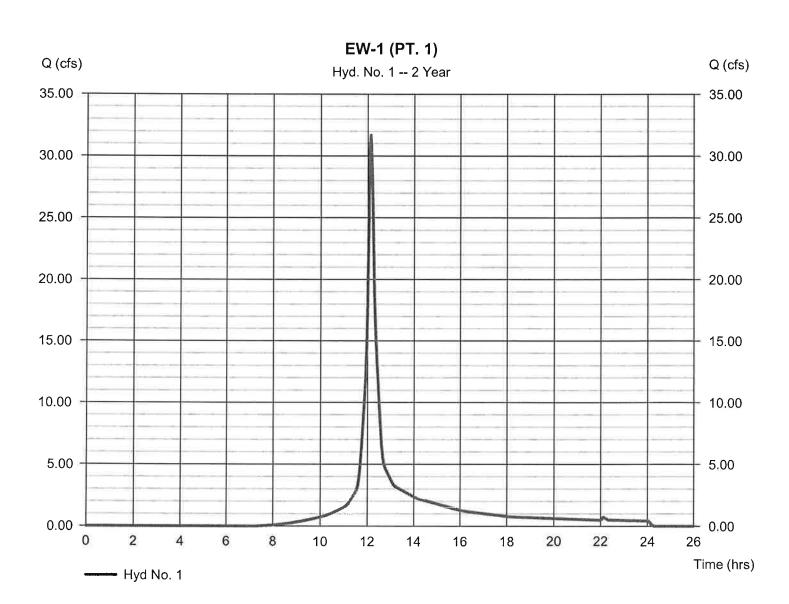
EW-1 (PT. 1)

Storm duration

Hydrograph type = SCS Runoff Peak discharge = 31.68 cfsStorm frequency = 2 yrsTime to peak  $= 12.13 \, hrs$ Time interval Hyd. volume = 1 min = 115,076 cuftDrainage area = 17.050 acCurve number = 87\* Basin Slope = 0.0 % Hydraulic length = 0 ftTc method = TR55 Time of conc. (Tc) = 10.23 minTotal precip. = 3.10 inDistribution = Type III

Shape factor

= 24 hrs



<sup>\*</sup> Composite (Area/CN) = [(3.240 x 39) + (14.180 x 98)] / 17.050

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

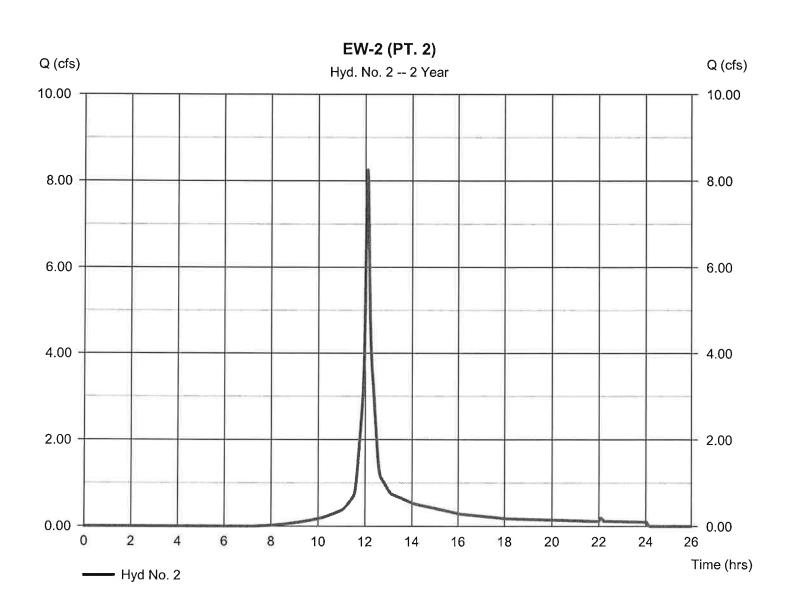
Tuesday, Jun 3, 2008

#### Hyd. No. 2

EW-2 (PT. 2)

Hydrograph type = SCS Runoff Peak discharge = 8.251 cfsStorm frequency Time to peak = 2 yrs $= 12.10 \, hrs$ Time interval = 1 min Hyd. volume = 26,572 cuftDrainage area = 4.110 acCurve number = 87\* Basin Slope = 0.0 % Hydraulic length = 0 ftTc method = TR55 Time of conc. (Tc) = 7.81 minTotal precip. = 3.10 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(3.310 x 98) + (0.800 x 39)] / 4.110



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#### Hyd. No. 3

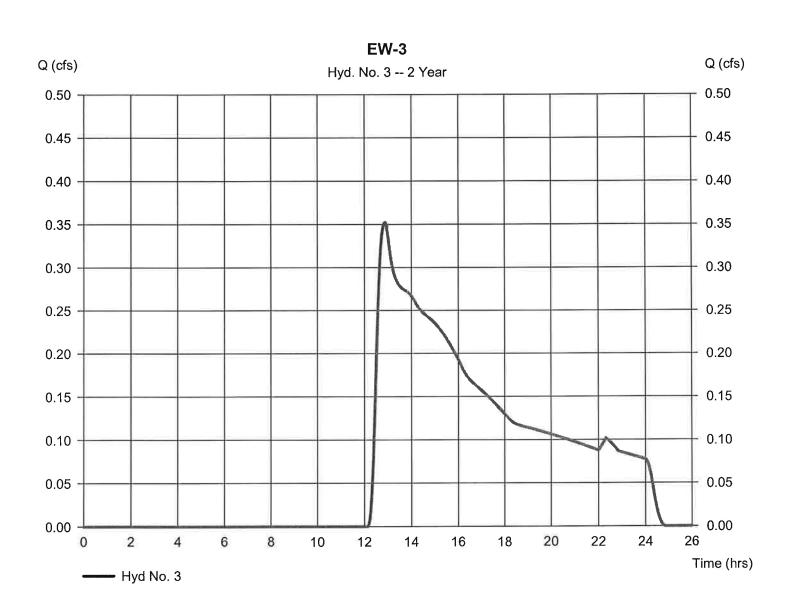
**EW-3** 

= 0.352 cfs= SCS Runoff Peak discharge Hydrograph type Storm frequency Time to peak  $= 12.88 \, hrs$ = 2 yrsHyd. volume = 6,744 cuft Time interval = 1 min Curve number = 52\* Drainage area = 12.310 ac

Basin Slope = 0.0 % Hydraulic length = 0 ft
Tc method = TR55 Time of conc. (Tc) = 31.55 min

Total precip. = 3.10 in Distribution = Type III Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) =  $[(2.280 \times 98) + (0.440 \times 76) + (0.130 \times 83) + (14.090 \times 39)] / 12.310$ 



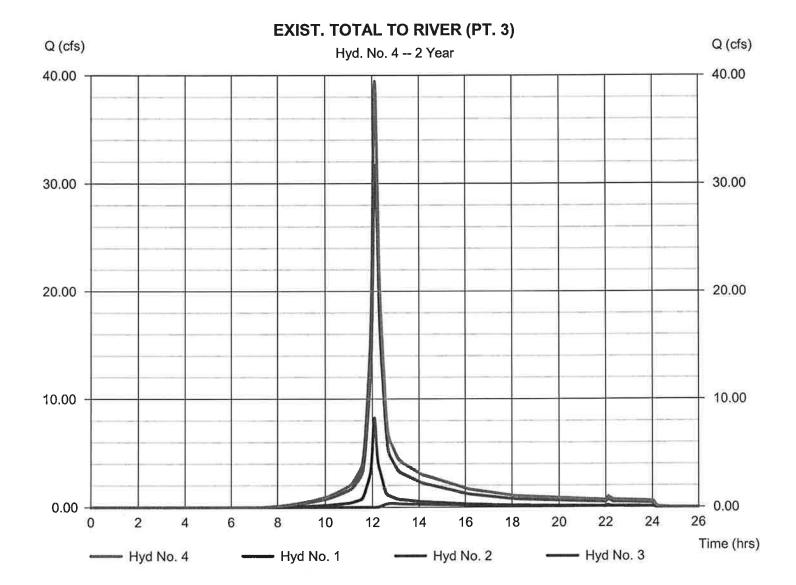
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

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#### Hyd. No. 4

EXIST. TOTAL TO RIVER (PT. 3)

Hydrograph type = Combine Storm frequency = 2 yrs Time interval = 1 min Inflow hyds. = 1, 2, 3 Peak discharge = 39.44 cfs Time to peak = 12.12 hrs Hyd. volume = 148,392 cuft Contrib. drain. area= 33.470 ac



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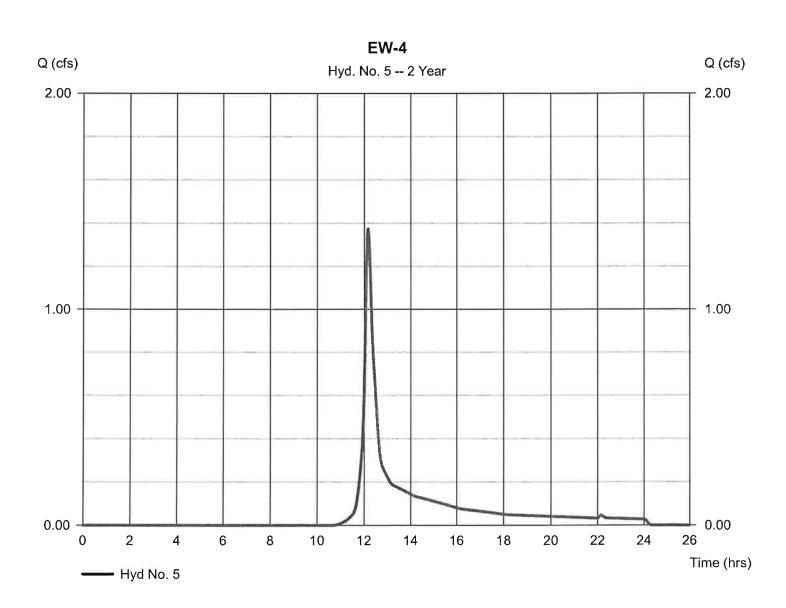
#### Hyd. No. 5

EW-4

Hydrograph type = SCS Runoff Peak discharge = 1.373 cfsStorm frequency = 2 yrsTime to peak  $= 12.17 \, hrs$ Time interval = 1 min Hyd. volume = 5,489 cuftDrainage area = 1.580 acCurve number = 74\* Basin Slope = 0.0 % Hydraulic length = 0 ftTc method = TR55 Time of conc. (Tc) = 12.01 min

Total precip. Distribution = Type III = 3.10 inStorm duration = 484 = 24 hrs Shape factor

<sup>\*</sup> Composite (Area/CN) = [(0.950 x 98) + (0.630 x 39)] / 1.580



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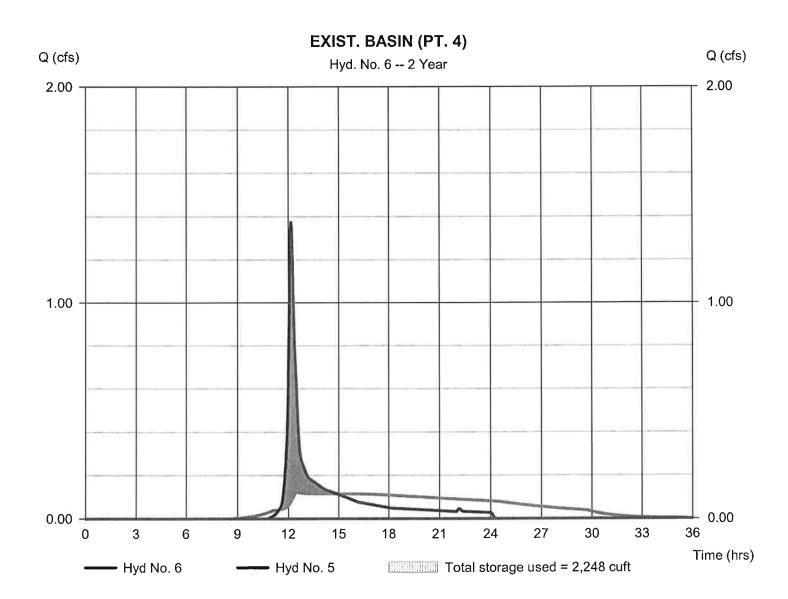
Tuesday, Jun 3, 2008

## Hyd. No. 6

EXIST. BASIN (PT. 4)

= 0.000 cfsHydrograph type Peak discharge = Reservoir Time to peak  $= 13.08 \, hrs$ Storm frequency = 2 yrs Hyd. volume = 0 cuftTime interval = 1 min Max. Elevation = 118.60 ft= 5 - EW-4Inflow hyd. No. Reservoir name = EX. BASIN Max. Storage = 2,248 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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## Hyd. No. 7

EW-5A

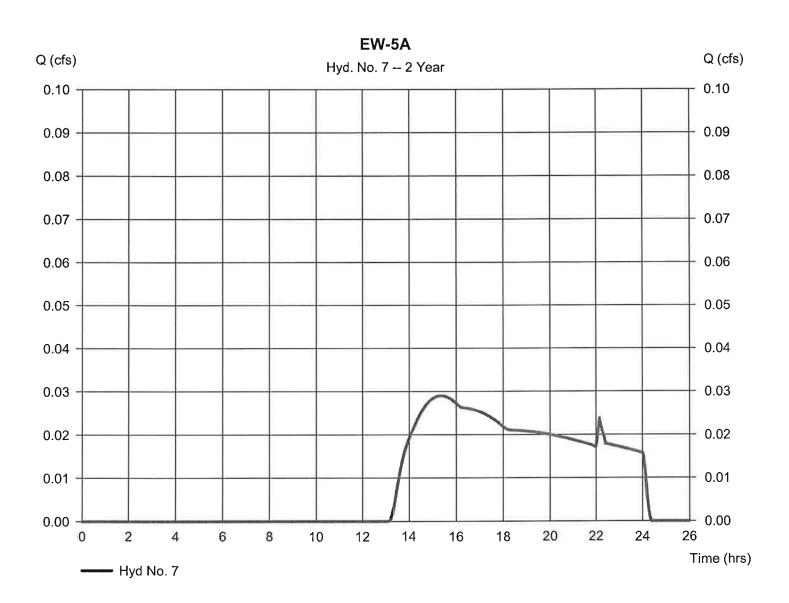
= 0.029 cfsPeak discharge Hydrograph type = SCS Runoff Storm frequency Time to peak = 15.37 hrs= 2 yrsHyd. volume Time interval = 1 min = 820 cuft Curve number = 46\* Drainage area = 4.990 acBasin Slope Hydraulic length = 0 ft= 0.0 % Time of conc. (Tc) = 14.91 minTc method = TR55

Tc method = TR55 Time of conc. (Tc) = 14.91 min

Total precip. = 3.10 in Distribution = Type III

Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.400 \times 98) + (4.750 \times 39)] / 4.990$ 



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## Hyd. No. 8

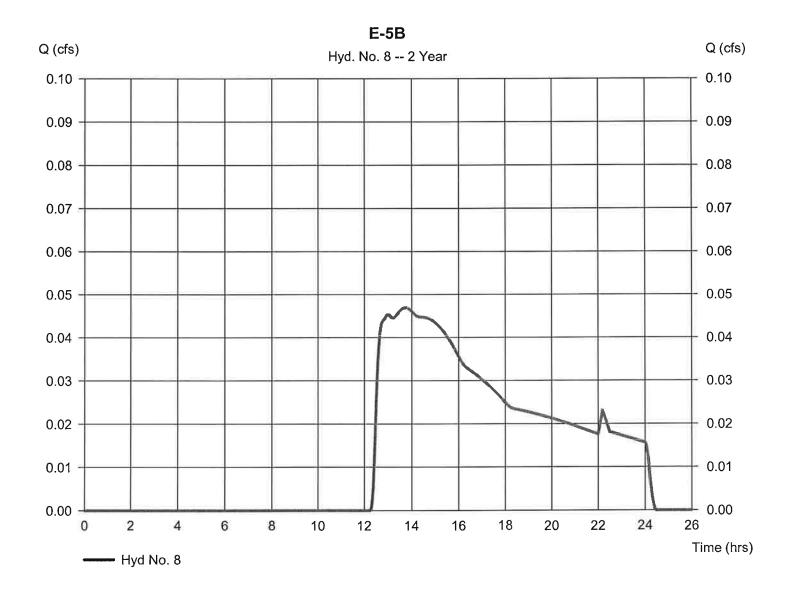
E-5B

Hydrograph type = SCS Runoff Storm frequency = 2 yrsTime interval = 1 min Drainage area = 3.090 acBasin Slope = 0.0 % Tc method = TR55 Total precip. = 3.10 inStorm duration = 24 hrs

Peak discharge = 0.047 cfs
Time to peak = 13.75 hrs
Hyd. volume = 1,209 cuft

Curve number = 50 Hydraulic length = 0 ft

Time of conc. (Tc) = 18.18 min
Distribution = Type III
Shape factor = 484



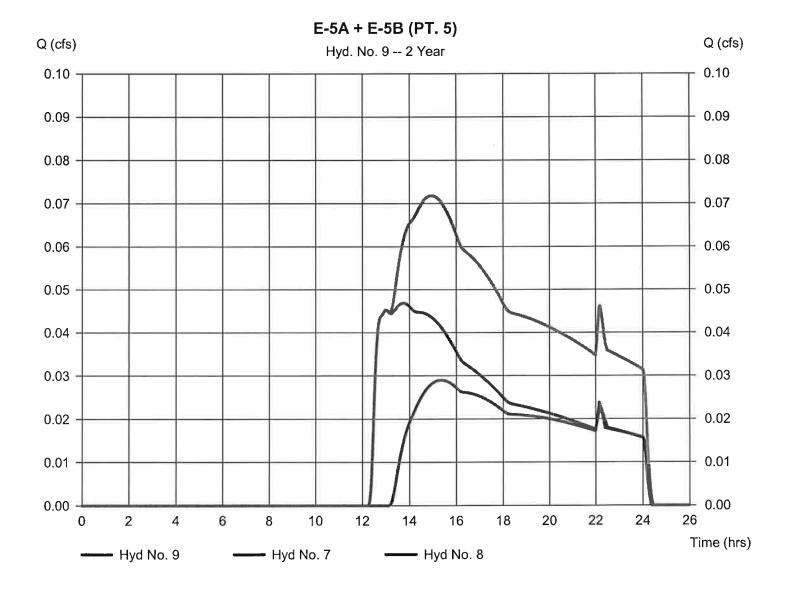
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Tuesday, Jun 3, 2008

## Hyd. No. 9

E-5A + E-5B (PT. 5)

Hydrograph type = Combine Storm frequency = 2 yrs Time interval = 1 min Inflow hyds. = 7, 8 Peak discharge = 0.072 cfs Time to peak = 14.95 hrs Hyd. volume = 2,029 cuft Contrib. drain. area= 8.080 ac



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## Hyd. No. 10

EW-6 (PT. 6)

Hydrograph type Peak discharge = 1.095 cfs= SCS Runoff Storm frequency Time to peak = 12.07 hrs= 2 yrs Time interval Hyd. volume = 4.083 cuft= 1 min Curve number = 61\* Drainage area = 2.830 ac

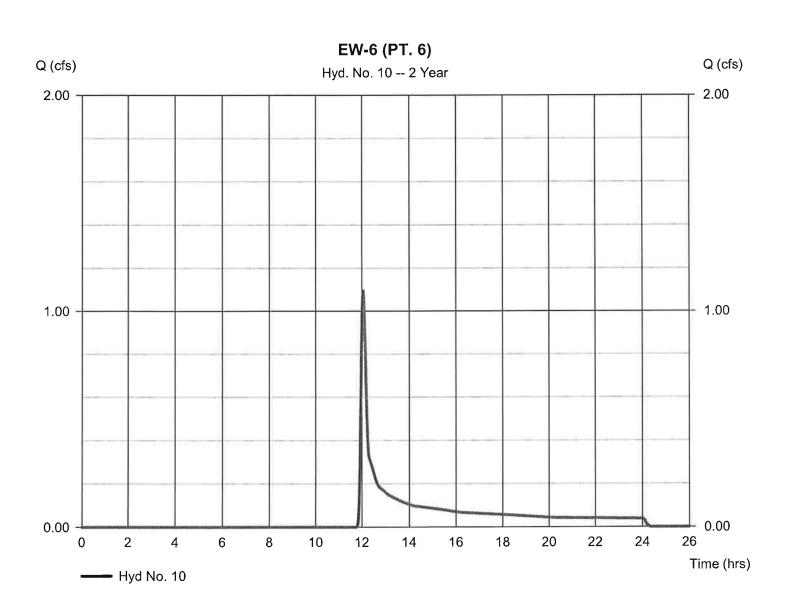
Basin Slope = 0.0 % Hydraulic length = 0 ft
Tc method = TR55 Time of conc. (Tc) = 12.03 min

Tc method = TR55 Time of conc. (Tc) = 12.03 min

Total precip. = 3.10 in Distribution = Type II

Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(0.660 x 98) + (1.790 x 39)] / 2.830



Hydrograph Summary Report
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Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	53.09	1	728	195,223	N <del>eedle 1</del>	*****	*****	EW-1 (PT. 1)
2	SCS Runoff	13.82	1	725	45,078	7-22000			EW-2 (PT. 2)
3	SCS Runoff	3.324	1	753	26,655				EW-3
4	Combine	66.75	1	727	266,955	1, 2, 3	******	HALLES.	EXIST. TOTAL TO RIVER (PT. 3)
5	SCS Runoff	2.927	1	729	11,135	(min	-summer	:=2000125	EW-4
6	Reservoir	0.000	1	732	0	5	119.19	5,096	EXIST. BASIN (PT. 4)
7	SCS Runoff	0.630	1	746	6,040	Cathern			EW-5A
8	SCS Runoff	0.762	1	743	5,544				E-5B
9	Combine	1.385	1	745	11,584	7, 8	(44444)	T-FERRICE	E-5A + E-5B (PT. 5)
10	SCS Runoff	3.951	1	722	10,914	2. <del>000,000</del>			EW-6 (PT. 6)
11	SCS Runoff	45.30	1	732	192,400				PW-1A
12	SCS Runoff	4.338	1	725	13,432			·*****	PW-1B
13	Reservoir	0.842	1	748	3,749	12	127.41	5,189	WATER QUALITY SWALE
14	Combine	45.70	1	732	196,149	11, 13			TOTAL TO BASIN 2
15	Reservoir	34.19	1	742	167,881	14	121.92	40,295	BASIN 2
16	Diversion1	0.820	1	742	19,625	15	s <del>anthas</del> :		BASIN 2 INFILTRATION
17	Diversion2	33.37	1	742	148,255	15	*****	92022	BASIN 2 OUTFLOW (PT. 1)
18	SCS Runoff	0.499	1	755	3,761	- Daniel I			PW-2
19	Reservoir	0.000	1	774	0	18	118.36	1,341	BASIN 1 (PT.2)
20	SCS Runoff	1.274	1	748	10,882		•••••		PW-3
21	SCS Runoff	12.06	1	741	62,928		784444E	(*************************************	PW-5A
22	Reservoir	7.915	1	757	38,755	21	129.25	17,002	BASIN 3
23	Combine	39.25	1	744	206,636	15, 19, 22		722222	PROP. TOTAL TO RIVER (PT. 3)
24	SCS Runoff	0.993	1	727	3,424	222225	\$ <del>89389=</del> 1	STATE	PW-5B (PT. 5)
25	SCS Runoff	2.941	1	737	14,256	*******	S <del>eason</del> s	(Expense)	PW-6A
26	Reservoir	2.731	1	740	6,961	25	130.06	3,214	BASIN 4
27	SCS Runoff	0.009	1	881	248	apounts:			PW-6B
28	Combine	2.731	1	740	7,210	26, 27	\$ <del>805885</del>	U <del>tanag</del>	TOTAL TO PT. 6
Hyc	lro_SPR_RE	V.gpw			Return F	Period: 10 \	⁄ear	Tuesday,	Jun 3, 2008

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

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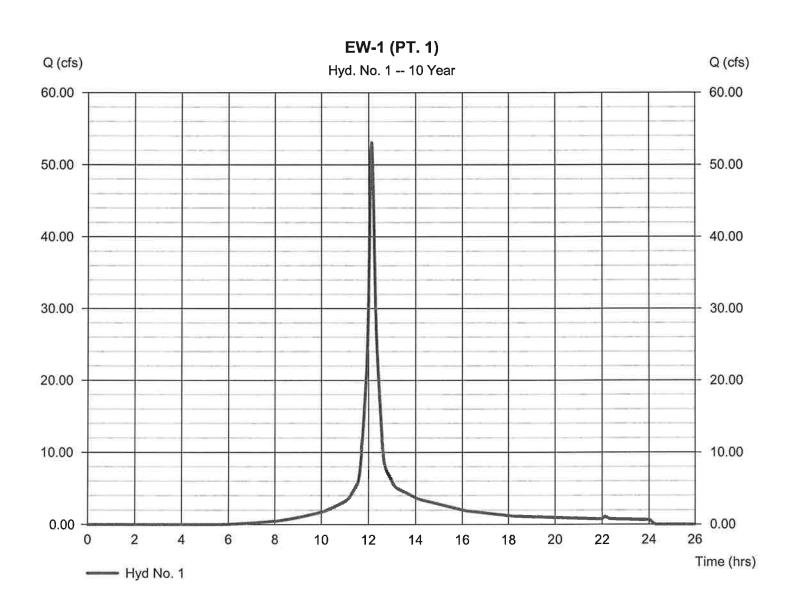
## Hyd. No. 1

EW-1 (PT. 1)

Hydrograph type = SCS Runoff Peak discharge = 53.09 cfsStorm frequency Time to peak  $= 12.13 \, hrs$ = 10 yrsTime interval = 1 min Hyd. volume = 195,223 cuftCurve number Drainage area = 17.050 ac= 87\* Basin Slope = 0.0 %Hydraulic length = 0 ftTime of conc. (Tc) = 10.23 minTc method = TR55

Tc method = TR55 Time of conc. (Tc) = 10.23 mir Total precip. = 4.50 in Distribution = Type III Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) =  $[(3.240 \times 39) + (14.180 \times 98)] / 17.050$ 



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

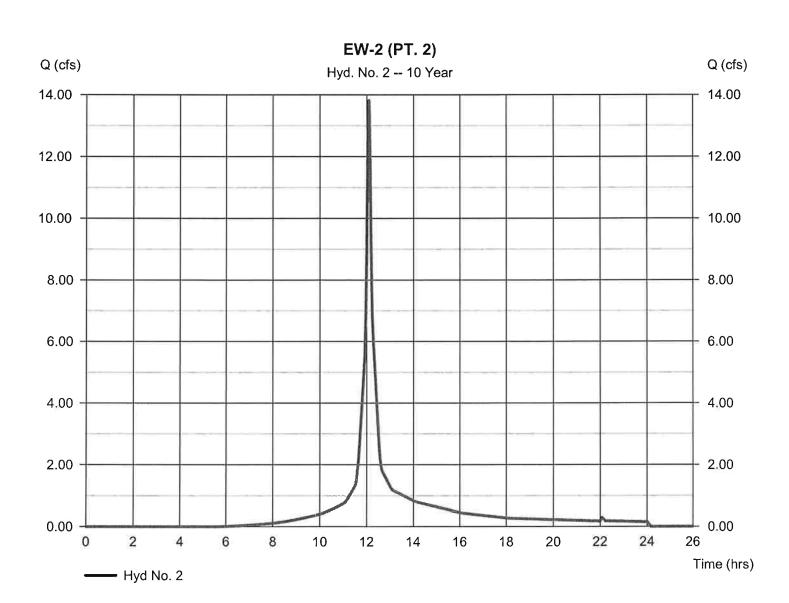
Tuesday, Jun 3, 2008

### Hyd. No. 2

EW-2 (PT. 2)

Hydrograph type = SCS Runoff Peak discharge = 13.82 cfsStorm frequency = 10 yrsTime to peak  $= 12.08 \, hrs$ Time interval = 1 min Hyd. volume = 45,078 cuftDrainage area = 4.110 ac Curve number = 87\* Basin Slope = 0.0 % Hydraulic length = 0 ftTime of conc. (Tc) = 7.81 minTc method = TR55 Total precip. Distribution = Type III = 4.50 inStorm duration = 484 Shape factor = 24 hrs

<sup>\*</sup> Composite (Area/CN) = [(3.310 x 98) + (0.800 x 39)] / 4.110



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

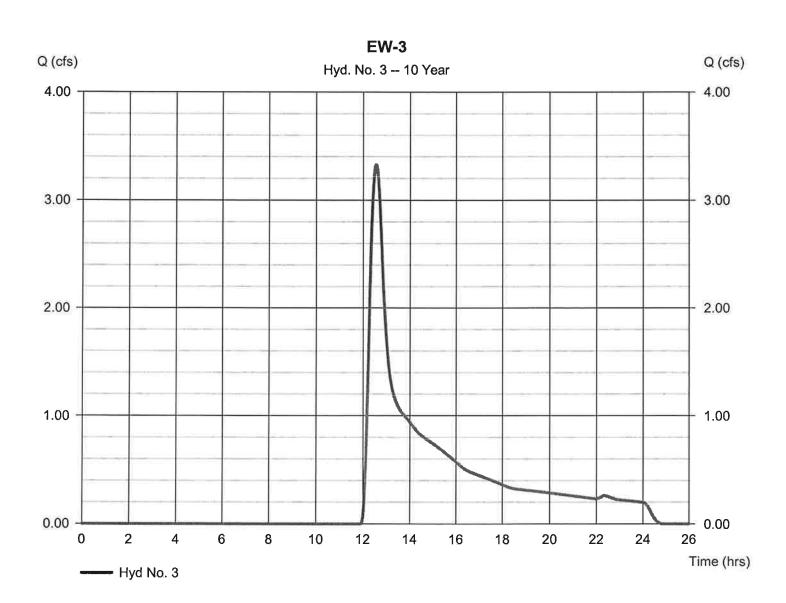
Tuesday, Jun 3, 2008

#### Hyd. No. 3

EW-3

= SCS Runoff Hydrograph type Peak discharge = 3.324 cfsStorm frequency = 10 yrs Time to peak  $= 12.55 \, hrs$ Time interval Hyd. volume = 1 min = 26,655 cuftDrainage area = 12.310 acCurve number = 52\* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 31.55 min = TR55 Total precip. = 4.50 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(2.280 x 98) + (0.440 x 76) + (0.130 x 83) + (14.090 x 39)] / 12.310



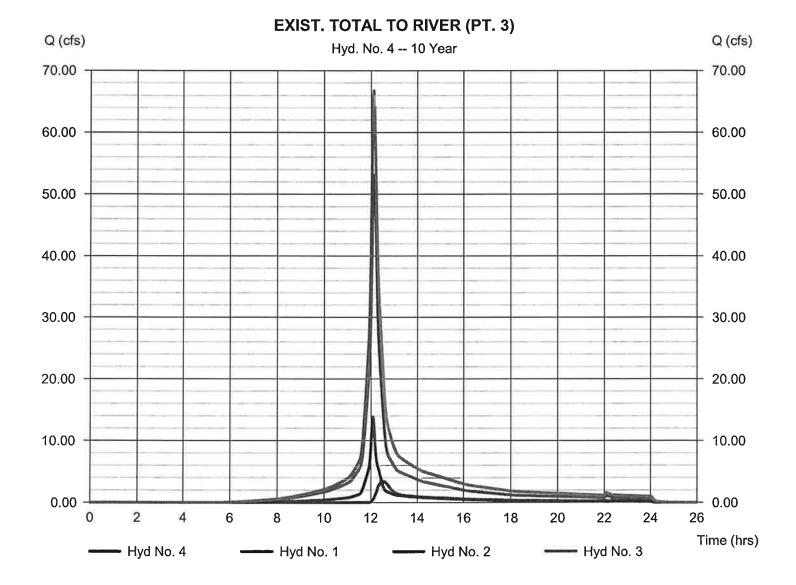
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

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#### Hyd. No. 4

EXIST. TOTAL TO RIVER (PT. 3)

Hydrograph type = Combine Storm frequency = 10 yrs Time interval = 1 min Inflow hyds. = 1, 2, 3 Peak discharge = 66.75 cfs Time to peak = 12.12 hrs Hyd. volume = 266,955 cuft Contrib. drain. area= 33.470 ac



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

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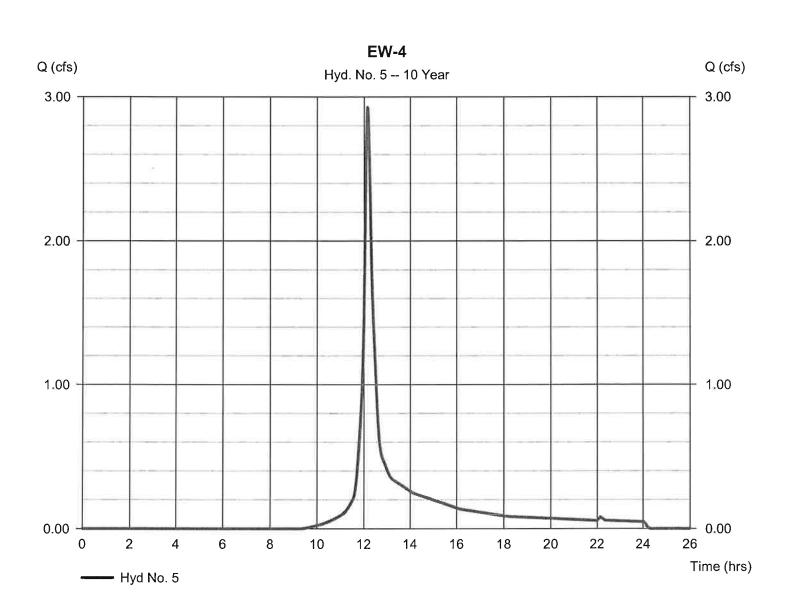
### Hyd. No. 5

EW-4

Hydrograph type = SCS Runoff Peak discharge = 2.927 cfsStorm frequency Time to peak  $= 12.15 \, hrs$ = 10 yrsTime interval = 1 min Hyd. volume = 11,135 cuft = 1.580 acCurve number = 74\* Drainage area Basin Slope Hydraulic length = 0.0 % = 0 ft

Tc method = TR55 Time of conc. (Tc) = 12.01 min
Total precip. = 4.50 in Distribution = Type III
Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.950 \times 98) + (0.630 \times 39)] / 1.580$ 



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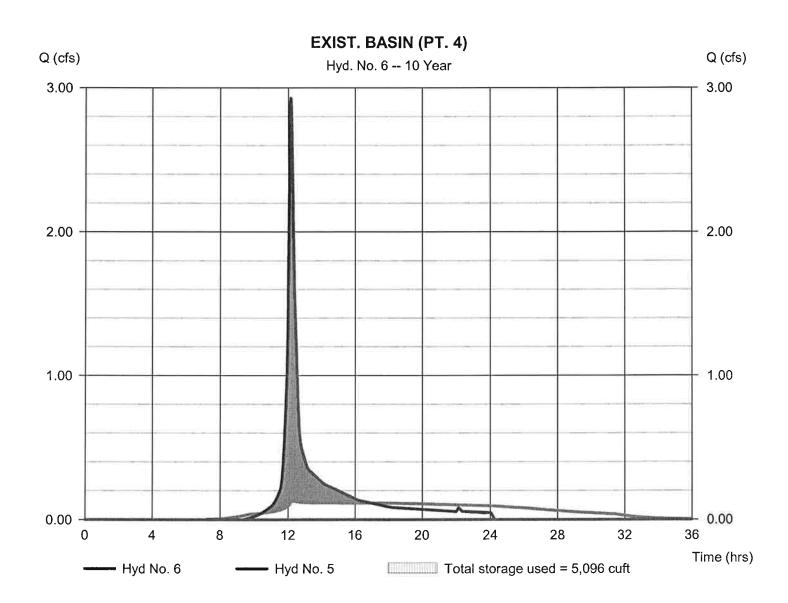
Tuesday, Jun 3, 2008

## Hyd. No. 6

EXIST. BASIN (PT. 4)

Peak discharge = 0.000 cfsHydrograph type = Reservoir Time to peak Storm frequency = 12.20 hrs= 10 yrsTime interval Hyd. volume = 1 min = 0 cuft Max. Elevation Inflow hyd. No. = 119.19 ft= 5 - EW-4Reservoir name Max. Storage = 5,096 cuft = EX. BASIN

Storage Indication method used. Exfiltration extracted from Outflow.



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

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## Hyd. No. 7

EW-5A

Hydrograph type = SCS Runoff
Storm frequency = 10 yrs
Time interval = 1 min
Drainage area = 4.990 ac
Basin Slope = 0.0 %
Tc method = TR55

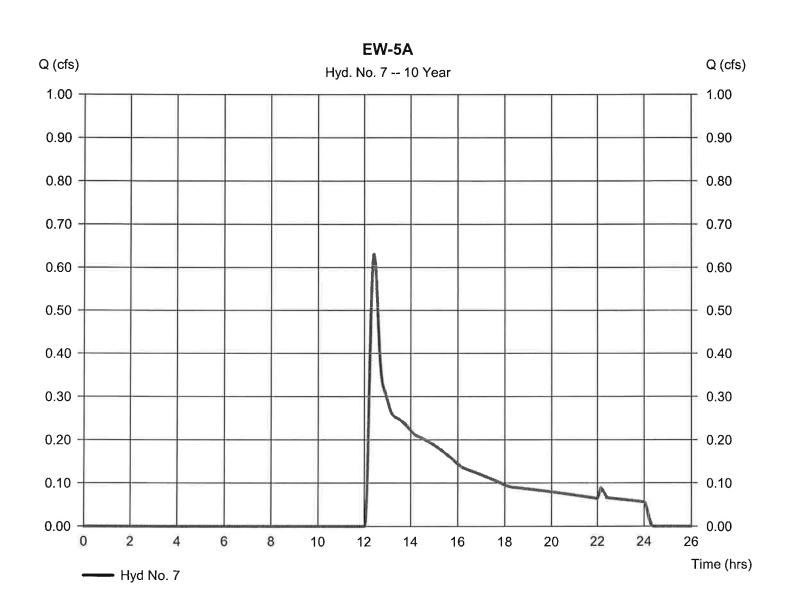
Tc method = TR55
Total precip. = 4.50 in
Storm duration = 24 hrs

Peak discharge = 0.630 cfs Time to peak = 12.43 hrs Hyd. volume = 6,040 cuft

Curve number =  $46^*$ Hydraulic length = 0 ft

Time of conc. (Tc) = 14.91 min
Distribution = Type III
Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(0.400 x 98) + (4.750 x 39)] / 4.990



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

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### Hyd. No. 8

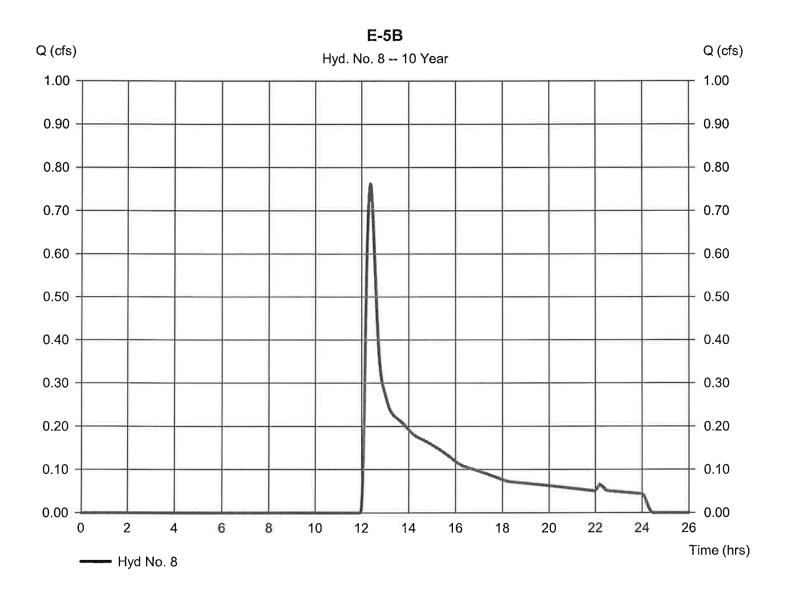
E-5B

= SCS Runoff Hydrograph type Storm frequency = 10 yrsTime interval = 1 min Drainage area = 3.090 acBasin Slope = 0.0 %Tc method = TR55 Total precip. = 4.50 inStorm duration = 24 hrs

Peak discharge = 0.762 cfs
Time to peak = 12.38 hrs
Hyd. volume = 5,544 cuft

Curve number = 50 Hydraulic length = 0 ft

Time of conc. (Tc) = 18.18 min
Distribution = Type III
Shape factor = 484



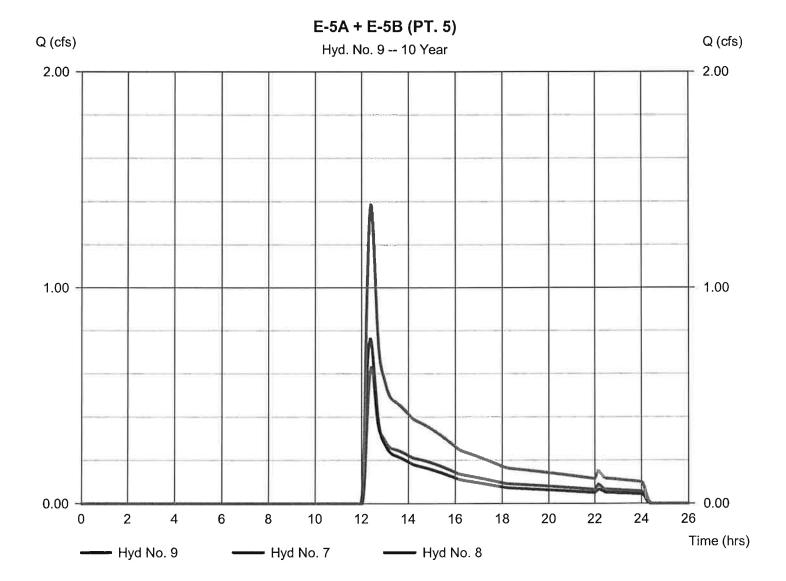
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### Hyd. No. 9

E-5A + E-5B (PT. 5)

Hydrograph type = Combine Storm frequency = 10 yrs Time interval = 1 min Inflow hyds. = 7, 8 Peak discharge = 1.385 cfs
Time to peak = 12.42 hrs
Hyd. volume = 11,584 cuft
Contrib. drain. area= 8.080 ac



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

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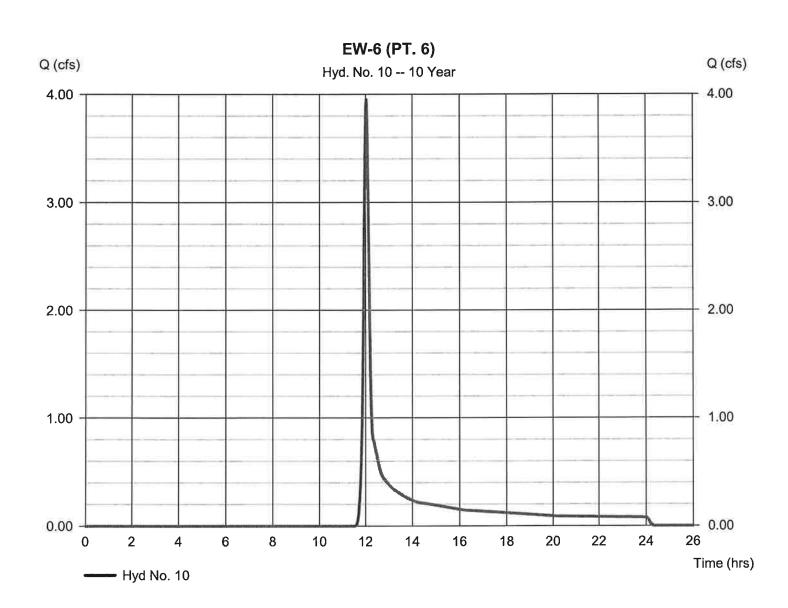
## Hyd. No. 10

EW-6 (PT. 6)

Hydrograph type = SCS Runoff
Storm frequency = 10 yrs
Time interval = 1 min
Peak discharge = 3.951 cfs
Time to peak = 12.03 hrs
Hyd. volume = 10,914 cuft

Tc method = TR55 Time of conc. (Tc) = 12.03 min
Total precip. = 4.50 in Distribution = Type II
Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(0.660 x 98) + (1.790 x 39)] / 2.830



Hydrograph Summary Report
Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	91.48	1	728	345,180				EW-1 (PT. 1)
2	SCS Runoff	23.83	1	725	79,704		20222	200002	EW-2 (PT. 2)
3	SCS Runoff	13.92	1	746	83,057		******		EW-3
4	Combine	120.33	1	727	507,942	1, 2, 3			EXIST. TOTAL TO RIVER (PT. 3)
5	SCS Runoff	6.070	1	729	22,821			-2.222	EW-4
6	Reservoir	0.000	1	768	0	5	120.10	12,018	EXIST. BASIN (PT. 4)
7	SCS Runoff	4.778	1	733	23,917	222222			EW-5A
8	SCS Runoff	3.796	1	735	18,482	(*2511-00			E-5B
9	Combine	8.554	1	734	42,399	7, 8	****	:====:	E-5A + E-5B (PT. 5)
10	SCS Runoff	10.68	1	721	27,323	2000000	FRANCE.	1803002	EW-6 (PT. 6)
11	SCS Runoff	82.29	1	732	354,916	2000	2		PW-1A
12	SCS Runoff	8.803	1	725	27,183	32			PW-1B
13	Reservoir	4.011	1	733	14,267	12	127.96	8,308	WATER QUALITY SWALE
14	Combine	86.29	1	732	369,183	11, 13		120000	TOTAL TO BASIN 2
15	Reservoir	65.82	1	741	336,563	14	123.29	63,332	BASIN 2
16	Diversion1	1.025	1	741	23,696	15	SHIZAR	******	BASIN 2 INFILTRATION
17	Diversion2	64.79	1	741	312,865	15		7 <u>282862</u>	BASIN 2 OUTFLOW (PT. 1)
18	SCS Runoff	1.683	1	749	10,491		*****		PW-2
19	Reservoir	0.035	1	815	215	18	119.08	4,292	BASIN 1 (PT.2)
20	SCS Runoff	7.448	1	737	39,243		•••••	×2.0002	PW-3
21	SCS Runoff	26.40	1	740	134,167			: <del>******</del>	PW-5A
22	Reservoir	17.27	1	757	106,346	21	130.69	31,280	BASIN 3
23	Combine	80.60	1	743	443,123	15, 19, 22		7201142	PROP. TOTAL TO RIVER (PT. 3)
24	SCS Runoff	2.021	1	727	6,929	******	*****	*****	PW-5B (PT. 5)
25	SCS Runoff	5.210	1	736	25,740	·	EARTH-	(STATUS)	PW-6A
26	Reservoir	5.006	1	739	16,969	25	130.19	3,527	BASIN 4
27	SCS Runoff	0.275	1	728	1,726		******	(ANNEXE)	PW-6B
28	Combine	5.237	1	739	18,695	26, 27		3 <del>555105</del> 1	TOTAL TO PT. 6
Hyd	ro_SPR_RE	V.gpw			Return F	Period: 100	Year	Tuesday, J	lun 3, 2008

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

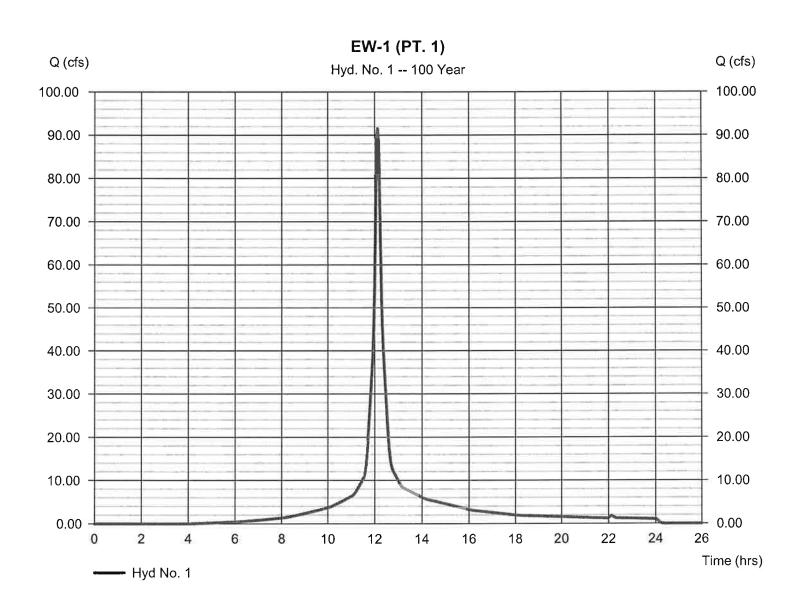
Tuesday, Jun 3, 2008

### Hyd. No. 1

EW-1 (PT. 1)

= SCS Runoff Peak discharge = 91.48 cfsHydrograph type Time to peak = 12.13 hrs Storm frequency = 100 yrs= 345,180 cuftTime interval = 1 min Hyd. volume Curve number = 87\* Drainage area = 17.050 acHydraulic length Basin Slope = 0 ft= 0.0 % Time of conc. (Tc) = 10.23 minTc method = TR55 = Type III Total precip. Distribution = 7.00 in= 484 Storm duration = 24 hrs Shape factor

<sup>\*</sup> Composite (Area/CN) = [(3.240 x 39) + (14.180 x 98)] / 17.050



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

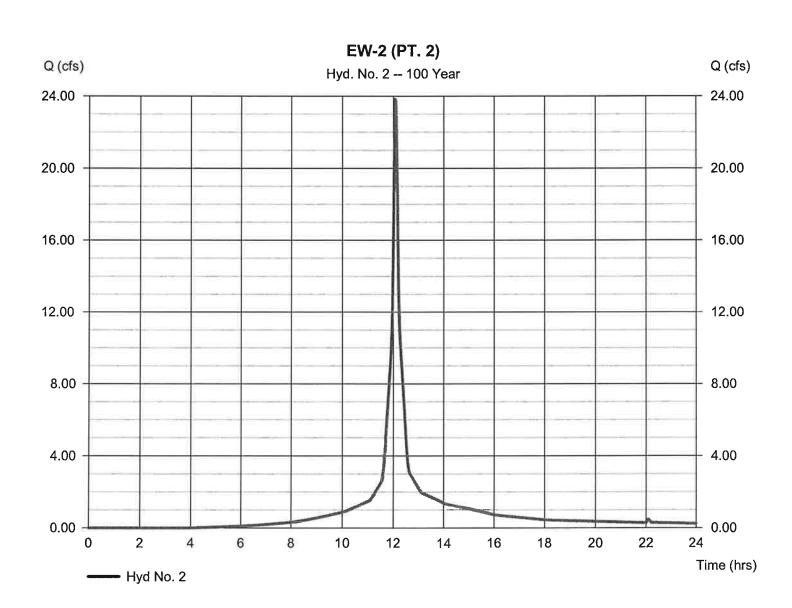
Tuesday, Jun 3, 2008

### Hyd. No. 2

EW-2 (PT. 2)

= SCS Runoff Hydrograph type Peak discharge = 23.83 cfsStorm frequency = 100 yrs Time to peak  $= 12.08 \, hrs$ Time interval Hyd. volume = 79,704 cuft= 1 min Drainage area = 4.110 acCurve number = 87\* Basin Slope Hydraulic length = 0 ft= 0.0 % Tc method Time of conc. (Tc) = 7.81 min= TR55 Total precip. = 7.00 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(3.310 x 98) + (0.800 x 39)] / 4.110



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

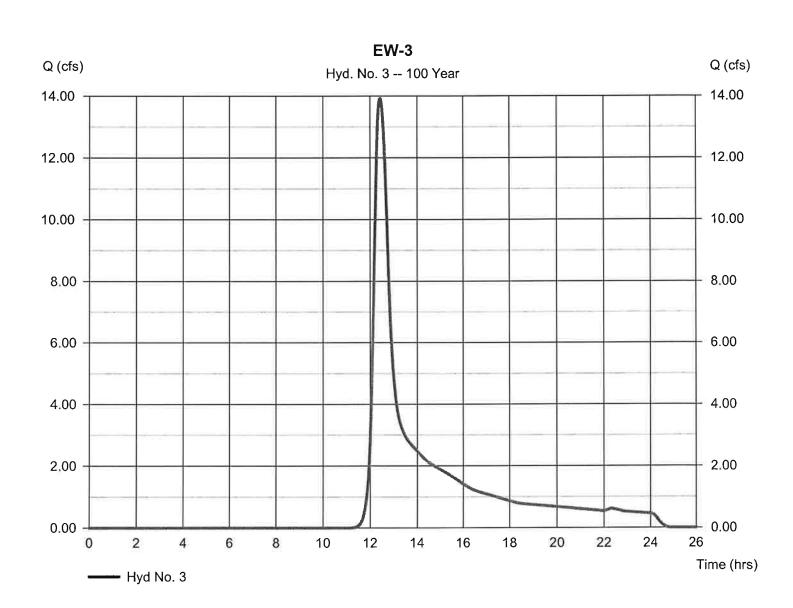
Tuesday, Jun 3, 2008

### Hyd. No. 3

EW-3

= SCS Runoff = 13.92 cfsHydrograph type Peak discharge Storm frequency Time to peak  $= 12.43 \, hrs$ = 100 yrsHyd. volume Time interval = 83,057 cuft= 1 minCurve number = 52\* Drainage area = 12.310 acHydraulic length = 0 ftBasin Slope = 0.0 % Time of conc. (Tc) = 31.55 minTc method = TR55 = Type III Distribution Total precip. = 7.00 inStorm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(2.280 x 98) + (0.440 x 76) + (0.130 x 83) + (14.090 x 39)] / 12.310



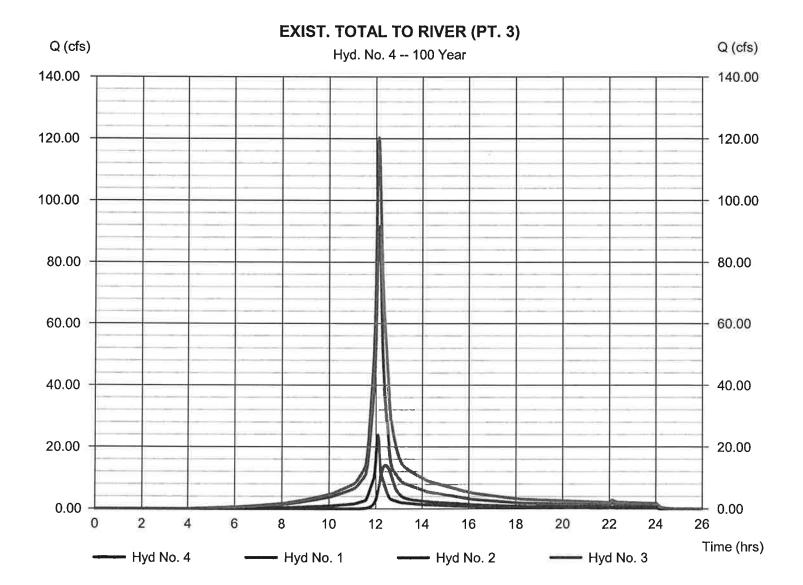
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

Tuesday, Jun 3, 2008

### Hyd. No. 4

EXIST. TOTAL TO RIVER (PT. 3)

Hydrograph type = Combine Storm frequency = 100 yrs Time interval = 1 min Inflow hyds. = 1, 2, 3 Peak discharge = 120.33 cfs Time to peak = 12.12 hrs Hyd. volume = 507,942 cuft Contrib. drain. area= 33.470 ac



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

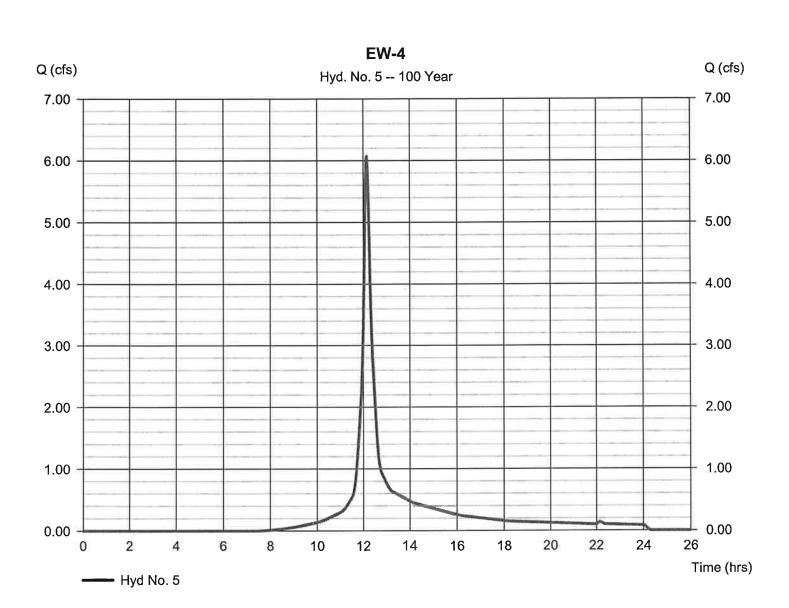
Tuesday, Jun 3, 2008

#### Hyd. No. 5

EW-4

= SCS Runoff = 6.070 cfsPeak discharge Hydrograph type Time to peak  $= 12.15 \, hrs$ Storm frequency = 100 yrsHyd. volume = 22,821 cuft Time interval = 1 minCurve number = 74\* Drainage area = 1.580 acHydraulic length Basin Slope = 0 ft= 0.0 %Time of conc. (Tc) = 12.01 minTc method = TR55 = Type III Distribution Total precip. = 7.00 in= 484 Storm duration = 24 hrs Shape factor

<sup>\*</sup> Composite (Area/CN) = [(0.950 x 98) + (0.630 x 39)] / 1.580



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

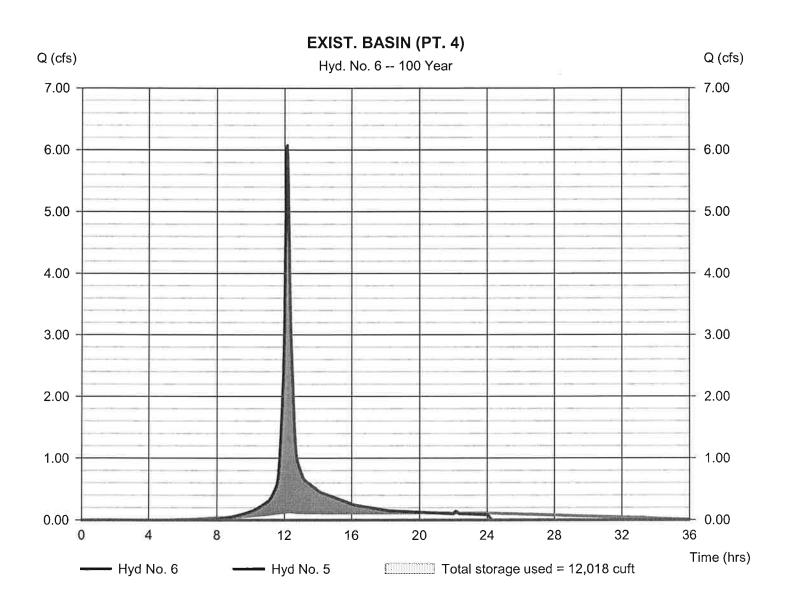
Tuesday, Jun 3, 2008

#### Hyd. No. 6

EXIST. BASIN (PT. 4)

Hydrograph type Peak discharge = 0.000 cfs= Reservoir Storm frequency Time to peak  $= 12.80 \, hrs$ = 100 yrsHyd. volume Time interval = 1 min = 0 cuftInflow hyd. No. Max. Elevation = 120.10 ft= 5 - EW-4Max. Storage Reservoir name = EX. BASIN = 12,018 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

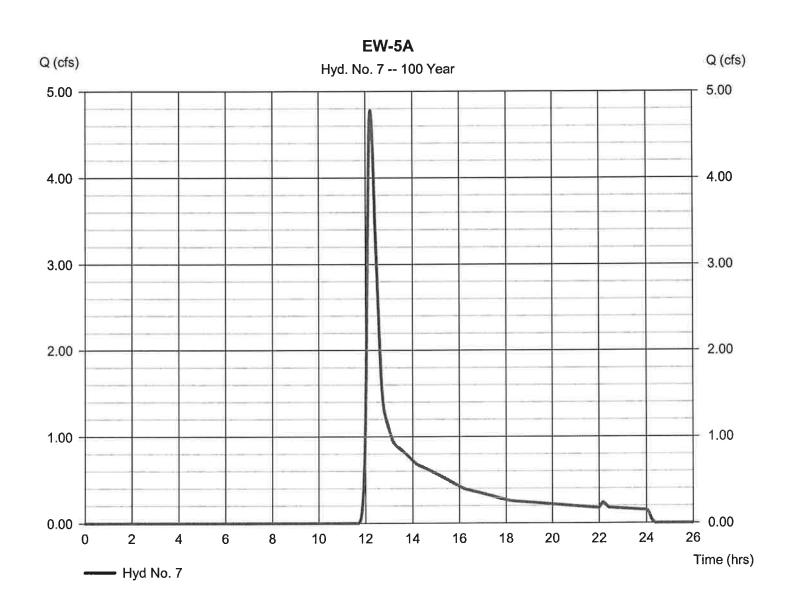
Tuesday, Jun 3, 2008

### Hyd. No. 7

EW-5A

= 4.778 cfsPeak discharge = SCS Runoff Hydrograph type Storm frequency Time to peak = 12.22 hrs= 100 yrs= 23,917 cuftTime interval Hyd. volume = 1 min Drainage area Curve number = 46\* = 4.990 acBasin Slope Hydraulic length = 0 ft= 0.0 %Time of conc. (Tc) = 14.91 minTc method = TR55 = Type III Distribution Total precip. = 7.00 in= 484 Shape factor Storm duration = 24 hrs

<sup>\*</sup> Composite (Area/CN) =  $[(0.400 \times 98) + (4.750 \times 39)] / 4.990$ 



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

Tuesday, Jun 3, 2008

#### Hyd. No. 8

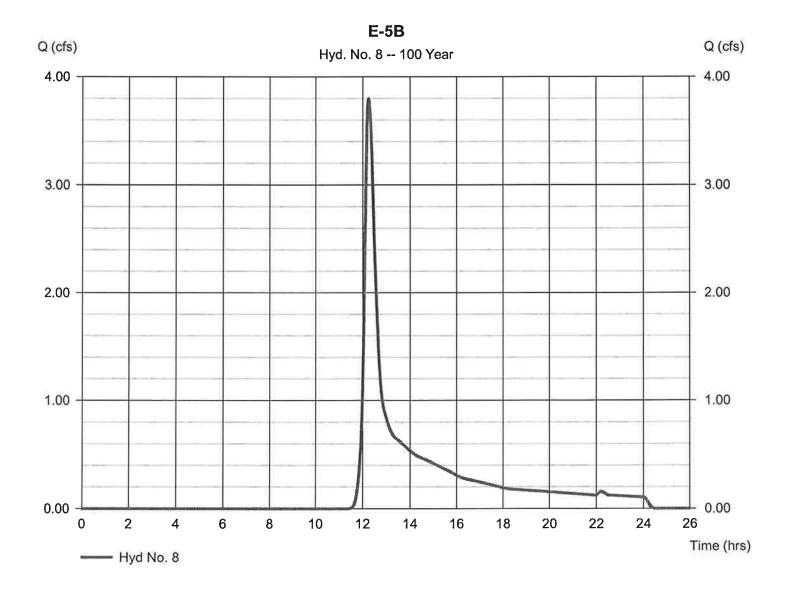
E-5B

Hydrograph type = SCS Runoff Storm frequency = 100 yrsTime interval = 1 min Drainage area = 3.090 acBasin Slope = 0.0 %Tc method = TR55 Total precip. = 7.00 inStorm duration = 24 hrs

Peak discharge = 3.796 cfs
Time to peak = 12.25 hrs
Hyd. volume = 18,482 cuft

Curve number = 50Hydraulic length = 0 ft

Time of conc. (Tc) = 18.18 min
Distribution = Type III
Shape factor = 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

Tuesday, Jun 3, 2008

### Hyd. No. 9

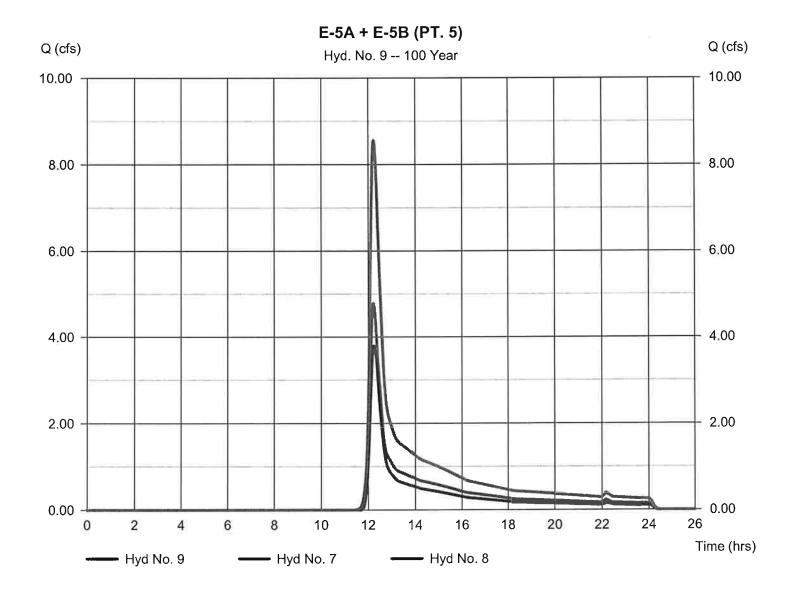
E-5A + E-5B (PT. 5)

Hydrograph type = Combine Storm frequency = 100 yrs Time interval = 1 min

Inflow hyds.

= 7,8

Peak discharge = 8.554 cfs Time to peak = 12.23 hrs Hyd. volume = 42,399 cuft Contrib. drain. area= 8.080 ac



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

Tuesday, Jun 3, 2008

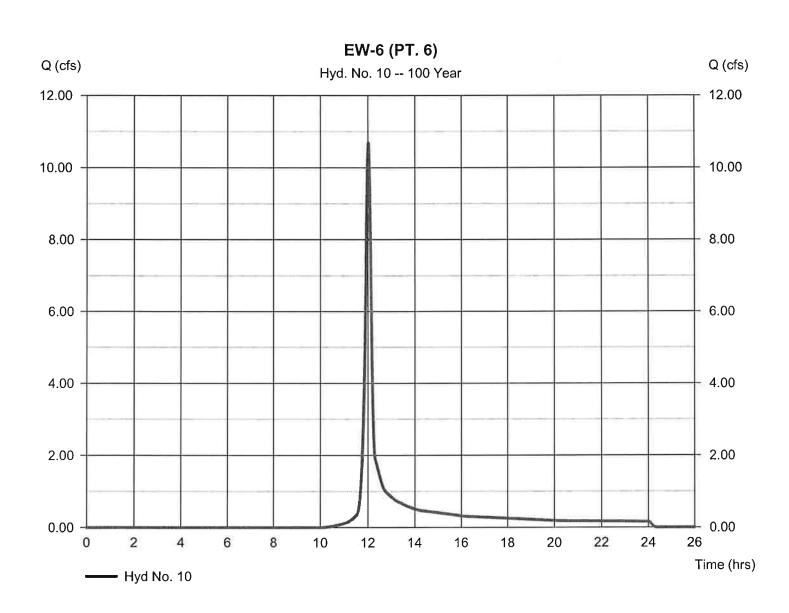
#### Hyd. No. 10

EW-6 (PT. 6)

Hydrograph type = SCS Runoff Peak discharge = 10.68 cfsTime to peak = 12.02 hrsStorm frequency = 100 yrsTime interval = 1 min Hyd. volume = 27,323 cuft Drainage area = 2.830 acCurve number = 61\*

Tc method = TR55 Time of conc. (Tc) = 12.03 min
Total precip. = 7.00 in Distribution = Type II
Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.660 \times 98) + (1.790 \times 39)] / 2.830$ 



### **APPENDIX C: PROPOSED CONDITIONS HYDROLOGY CALCULATIONS**

Runoff Curve Numbers and Runoff Time of Concentration Pond Reports Hydrograph Plots (2, 10, 25, 100 year storm events)

Project: Wayland Town Center By: CAD Date 06/02/08

Location: Wayland, MA Checked: Date

Check One: Present Developed PROPOSED WATERSHED 1A (PW-1A)

#### 1. Runoff curve number (CN)

Soil Name and	Cover Description		CN		Area	Product of
Hydrologic Group (appendix A)	(cover type, treatment, and hydrologic conditions percent impervious unconnected/connected impervious area ratio)	Table 2-2	Figure 2-3	Figure 2-4	X acres	CN x Area
А	Grass - good	39			5.23	203.97
A	Impervious (pavement, roof)	98			14.44	1415.12
						0.00
						0.00
						0.00
						0.00
						0.00
						0.00
						0.00
Use only one	CN source per line.	Total	ls =		19.67	1619.09

 $CN ext{ (weighted)} = \frac{\text{total product}}{\text{total area}}$  82.3127 Use CN = 82

#### 2. Runoff

	-	Storm #1	Storm #2	Storm #3	
Frequency	yr.	2	10	100	
Rainfall, P (24 hour)	in.	3.30	4.70	6.90	
Runoff, Q	in.	1.62	2.81	4.82	

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

Project:

**Wayland Town Center** 

By:

CAD Date 06/02/08

Location:

Wayland, MA

Checked:

Date

Check One:

Present

Developed

PROPOSED WATERSHED 1B (PW-1B)

#### 1. Runoff curve number (CN)

Soil Name and	Cover Description		CN		Area	Product of	
Hydrologic Group (appendix A)	(cover type, treatment, and hydrologic conditions percent impervious unconnected/connected impervious area ratio)	Table 2-2	Figure 2-3	Figure 2-4	X acres mi² %	CN x Area	
А	Grass - good	39			0.68	26.52	
А	Impervious (pavement, roof)	98			1.07	104.86	
						0.00	
						0.00	
	0					0.00	
						0.00	
						0.00	
						0.00	
ļ						0.00	
Use only one	CN source per line.	Total	s =	8	1.75	131.38	
CN (weig	ghted) = total product 75.0743	U	se CN	1=	75		

#### 2. Runoff

	r	Storm #1	Storm #2	Storm #3	
Frequency	yr.	2	10	100	
Rainfall, P (24 hour)	in.	3.30	4.70	6.90	
Runoff, Q	in.	1.16	2.21	4.06	

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

**Wayland Town Center** Project: CAD Date 06/02/08

Location: Wayland, MA Checked: Date

Check One: PROPOSED WATERSHED 2 (PW-2) Present Developed

#### 1. Runoff curve number (CN)

Soil Name and	Cover Description		CN		Area	Product of
Hydrologic Group (appendix A)	(cover type, treatment, and hydrologic conditions percent impervious unconnected/connected impervious area ratio)	Table 2-2	Figure 2-3	Figure 2-4	X acres mi² %	CN x Area
Α	Grass - good	39			0.94	36.66
Α	Impervious (pavement, roof)	98			0.37	36.26
						0.00
						0.00
						0.00
						0.00
						0.00
						0.00
						0.00
Use only one	CN source per line.	Total	s =		1.31	72.92
CN (weig	ghted) = total product total area 55.6641	Jυ	se CN	1=	56	

#### 2. Runoff

	-	Storm #1	Storm #2	Storm #3	
Frequency	yr.	2	10	100	
Rainfall, P (24 hour)	in.	3.30	4.70	6.90	
Runoff, Q	in.	0.31	0.89	2.15	

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

Project:

**Wayland Town Center** 

By:

CAD Date 06/02/08

Location:

Wayland, MA

Checked:

Date

Check One:

**Present** 

PROPOSED WATERSHED 3 (PW-3)

### 1. Runoff curve number (CN)

Soil Name and	Cover Description		CN		Area	Product of
Hydrologic Group (appendix A)	(cover type, treatment, and hydrologic conditions percent impervious unconnected/connected impervious area ratio)	Table 2-2	Figure 2-3	Figure 2-4	X acres	CN x Area
Α	Grass - good	39			5.95	232.05
Α	Wetland	83			0.63	52.29
Α	Impervious (pavement, roof)	98			0.67	65.66
						0.00
						0.00
						0.00
						0.00
						0.00
L						0.00
Use only one	CN source per line.	Total	s =		7.25	350
CN (weia	hted) = total product 48 27	50 11	se CN	t=	48	

2. Runoff

CN (weighted) =

	//	Storm #1	Storm #2	Storm #3	
Frequency	yr.	2	10	100	
Rainfall, P (24 hour)	in.	3.30	4.70	6.90	
Runoff, Q	in.	0.11	0.48	1.44	

48.2759

total area

Use CN=

48

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

Project: Wayland Town Center By: CAD Date 06/02/08

Location: Wayland, MA Checked: Date

Check One: Present Developed PROPOSED WATERSHED 5A (PW-5A)

### 1. Runoff curve number (CN)

Soil Name and	Cover Description		CN		Area	Product of	
Hydrologic Group (appendix A)	(cover type, treatment, and hydrologic conditions percent impervious unconnected/connected impervious area ratio)	Table 2-2	Figure 2-3	Figure 2-4	X acres	CN x Area	
A	Grass - good	39			4.65	181.35	
Α	Impervious (pavement, roof)	98			5.35	524.30	
						0.00	
						0.00	
						0.00	
						0.00	
						0.00	
						0.00	
						0.00	
Use only one (	CN source per line.	Total	s =		10	705.65	

CN (weighted) = total product total area 70.5650 Use CN= 71

#### 2. Runoff

	-	Storm #1	Storm #2	Storm #3
Frequency	yr.	2	10	100
Rainfall, P (24 hour)	in.	3.30	4.70	6.90
Runoff, Q	in.	0.94	1.89	3.64

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

Project: **Wayland Town Center** Ву: **CAD** Date 06/02/08

Location: Wayland, MA Checked: Date

Check One: **Present** Developed PROPOSED WATERSHED 5B (PW-5B)

#### 1. Runoff curve number (CN)

Soil Name and	Cover Description		CN		Area	Product of
Hydrologic Group (appendix A)	(cover type, treatment, and hydrologic conditions percent impervious unconnected/connected impervious area ratio)	Table 2-2	Figure 2-3	Figure 2-4	X acres mi² %	CN x Area
Α	Grass - good	39			0.18	7.02
Α	Impervious (pavement, roof)	98			0.28	27.44
						0.00
						0.00
						0.00
						0.00
						0.00
						0.00
						0.00
Use only one CN source per line.		Total	s =		0.46	34.46
CN (weig	ghted) = total product total area 74.9130	U	se CN	<b>/=</b>	75	

#### 2. Runoff

	-	Storm #1	Storm #2	Storm #3	
Frequency	yr.	2	10	100	
Rainfall, P (24 hour)	in.	3.30	4.70	6.90	
Runoff, Q	in.	1.16	2.21	4.06	

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

total area

Project:

**Wayland Town Center** 

By:

CAD Date 06/02/08

Location:

Wayland, MA

Checked:

Date

Check One:

Present

Developed

PROPOSED WATERSHED 6A (PW-6A)

#### 1. Runoff curve number (CN)

Soil Name and	Cover Description		CN		Area	Product of	
Hydrologic	(cover type, treatment, and					CN x Area	
Group	hydrologic conditions percent impervious	2-5	2-3	Figure 2-4	X acres		
	unconnected/connected impervious	Table 2-2	Figure 7	nre	mi <sup>2</sup>		
(appendix A)	area ratio)	Ta I	Fig	Fig	%		
A	Grass - good	39			0.30	11.70	
A	Impervious (pavement, roof)	98			1.06	103.88	
						0.00	
						- 5.55	
						0.00	
						0.00	
						0.00	
						0.00	
						0.00	
						0.00	
Use only one CN source per line.		Totals =		1.36	115.58		

#### 2. Runoff

CN (weighted) =

	-	Storm #1	Storm #2	Storm #3	
Frequency	yr.	2	10	100	
Rainfall, P (24 hour)	in.	3.30	4.70	6.90	
Runoff, Q	in.	1.84	3.09	5.16	

84.9853

Use CN=

85

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

total product

total area

### Worksheet 2: Runoff curve number and runoff

Project: Wayland Town Center By: CAD Date 06/02/08

Location: Wayland, MA Checked: Date

Check One: Present Developed PROPOSED WATERSHED 6B (PW-6B)

#### 1. Runoff curve number (CN)

Soil Name and	Cover Description		CN		Area	Product of	
Hydrologic Group (appendix A)	(cover type, treatment, and hydrologic conditions percent impervious unconnected/connected impervious area ratio)	Table 2-2	Figure 2-3	Figure 2-4	X acres	CN x Area	
А	Grass - good	39			0.60	23.40	
Α	Impervious (pavement, roof)	98			0.00	0.00	
						0.00	
						0.00	
						0.00	
						0.00	
						0.00	
						0.00	
						0.00	
Use only one	CN source per line.	Total	s =		0.6	23.4	

CN (weighted) = total product total area 39.0000 Use CN= 39

#### 2. Runoff

	-	Storm #1	Storm #2	Storm #3	
Frequency	yr.	2	10	100	
Rainfall, P (24 hour)	in.	3.30	4.70	6.90	
Runoff, Q	in.	0.00	0.14	0.73	

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

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### Hyd. No. 11

PW-1A

<u>Description</u>	A		<u>B</u>		<u>C</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.200 = 100.0 = 3.10 = 1.00		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	= 16.53	+	0.00	+	0.00	=	16.53
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 70.00 = 1.00 = Unpave = 1.61	ed	0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00		
Travel Time (min)	= 0.72	+	0.00	+	0.00	=	0.72
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	= 1.77 = 2.36 = 0.50 = 0.012 = 7.24 = 540.0		0.00 0.00 0.00 0.015 0.00 0.0		0.00 0.00 0.00 0.015 0.00 0.0		
Travel Time (min)	= 1.24	+	0.00	+	0.00	=	1.24
Total Travel Time, Tc							18.50 min

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# Hyd. No. 18

PW-2

<u>Description</u>	<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.20 = 100 = 3.10 = 0.25	0	0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	= 28.7	'9 +	0.00	+	0.00	=	28.79
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)  Travel Time (min)	= 400 = 0.25 = Unp = 0.81	aved	0.00 0.00 Unpav 0.00	⁄ed +	0.00 0.00 Paved 0.00	=	8.26
, ,	- 0.20	in the second	0.00	-	0.00	_	0.20
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	= 1.76 = 2.35 = 0.50 = 0.01 = 7.23 = 205	2	0.00 0.00 0.00 0.015 0.00 0.0		0.00 0.00 0.00 0.015 0.00 0.0		
Travel Time (min)	= 0.47	+	0.00	+	0.00	=	0.47
Total Travel Time, Tc							37.52 min

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### Hyd. No. 20

PW-3

<u>Description</u>		<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	=	0.200 100.0 3.10 2.00		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	=	12.53	+	0.00	+	0.00	=	12.53
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= =	430.00 0.50 Unpaved 1.14	d	0.00 0.00 Unpave 0.00	ed	0.00 0.00 Unpave 0.00	ed	
Travel Time (min)	=	6.28	+	0.00	+	0.00	=	6.28
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	= =	0.00 0.00 0.00 0.015 0.00 0.0		0.00 0.00 0.00 0.015 0.00 0.0		0.00 0.00 0.00 0.015 0.00 0.0		
Travel Time (min)	=	0.00	+	0.00	+	0.00	=	0.00
Total Travel Time, Tc								18.81 min

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### Hyd. No. 21

PW-5A

<u>Description</u>	A		<u>B</u>		<u>C</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.200 = 100.0 = 3.10 = 0.50		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	= 21.82	+	0.00	+	0.00	=	21.82
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 360.00 = 0.50 = Unpave = 1.14	ed	0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00		
Travel Time (min)	= 5.26	+	0.00	+	0.00	=	5.26
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	= 1.76 = 2.36 = 0.50 = 0.012 = 7.21 = 80.0		0.00 0.00 0.00 0.015 0.00 0.0		0.00 0.00 0.00 0.015 0.00 0.0		
Travel Time (min)	= 0.18	+	0.00	+	0.00	=	0.18
Total Travel Time, Tc							

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### Hyd. No. 24

PW-5B (PT. 5)

<u>Description</u>	<u>A</u>		<u>B</u>		<u>c</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.200 = 70.0 = 3.10 = 7.00		0.011 30.0 3.10 5.00		0.011 0.0 0.00 0.00		
Travel Time (min)	= 5.71	+	0.33	+	0.00	=	6.03
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 170.00 = 3.50 = Paved = 3.80		280.00 0.80 Unpave 1.44	ed	0.00 0.00 Paved 0.00		
Travel Time (min)	= 0.75	+	3.23	+	0.00	=	3.98
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	= 0.00 = 0.00 = 0.00 = 0.015 = 0.00 = 0.0		0.00 0.00 0.00 0.015 0.00 0.0		0.00 0.00 0.00 0.015 0.00 0.0		
Travel Time (min)	= 0.00	+	0.00	+	0.00	=	0.00
Total Travel Time, Tc							

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# Hyd. No. 25

PW-6A

<u>Description</u>	4	<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= ( = (	0.200 100.0 3.10 0.50		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	= 2	21.82	+	0.00	+	0.00	=	21.82
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= ( = (	200.00 0.50 Unpaved 1.14	I	0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00		
Travel Time (min)	= :	2.92	+	0.00	+	0.00	=	2.92
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s) Flow length (ft)	= ( = ( = (	0.00 0.00 0.00 0.015 0.00		0.00 0.00 0.00 0.015 0.00 0.0		0.00 0.00 0.00 0.015 0.00 0.0		
Travel Time (min)	= (	0.00	+	0.00	+	0.00	=	0.00
Total Travel Time, Tc								24.74 min

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#### Pond No. 1 - BASIN 2

#### **Pond Data**

Contours - User-defined contour areas. Average end area method used for volume calculation. Begining Elevation = 116.00 ft

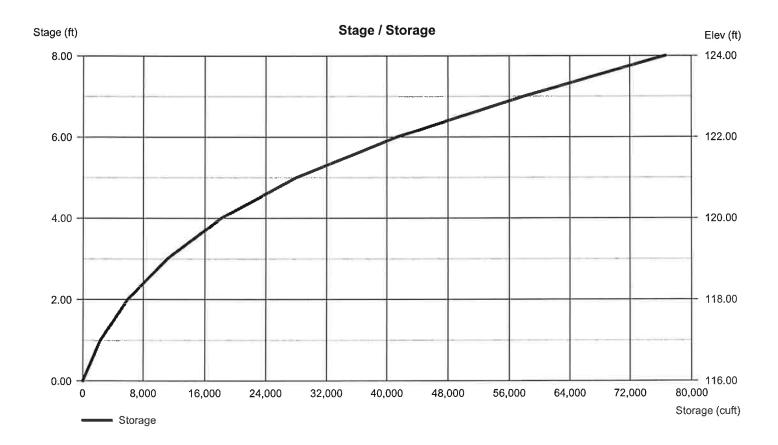
#### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)		
0.00	116.00	1,690	0	0		
1.00	117.00	2,915	2,303	2,303		
2.00	118.00	4,360	3,638	5,940		
3.00	119.00	6,043	5,202	11,142		
4.00	120.00	7,985	7,014	18,156		
5.00	121.00	11,696	9,841	27,996		
6.00	122.00	15,017	13,357	41,353		
7.00	123.00	17,997	16,507	57,860		
8.00	124.00	19,572	18,785	76,644		

#### **Culvert / Orifice Structures**

#### **Weir Structures**

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 36.00	0.00	0.00	0.00	Crest Len (ft)	= 6.00	0.00	0.00	0.00
Span (in)	= 36.00	0.00	0.00	0.00	Crest El. (ft)	= 122.80	0.00	0.00	0.00
No. Barrels	= 1	0	0	0	Weir Coeff.	= 2.60	3.33	3.33	3.33
Invert El. (ft)	= 118.50	0.00	0.00	0.00	Weir Type	= Broad			
Length (ft)	= 45.00	0.00	0.00	0.00	Multi-Stage	= No	No	No	No
Slope (%)	= 0.50	0.00	0.00	n/a					
N-Value	= .012	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 2.400 (by	Contour)		
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			



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#### Pond No. 2 - BASIN 3

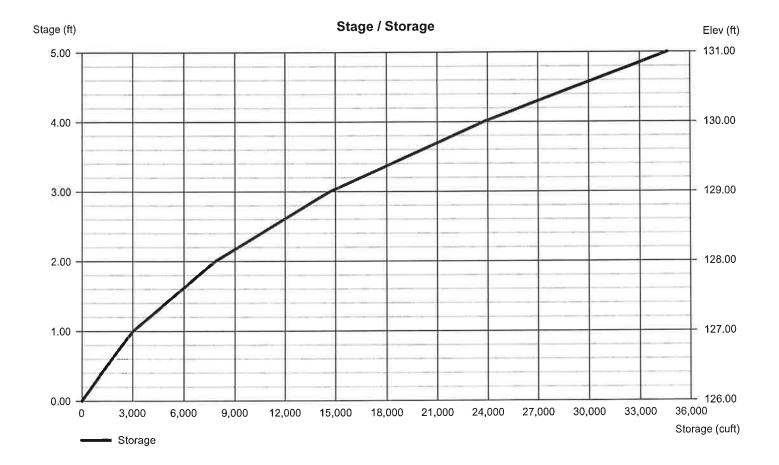
#### **Pond Data**

Contours - User-defined contour areas. Average end area method used for volume calculation. Begining Elevation = 126.00 ft

#### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	126.00	2,172	0	0
1.00	127.00	3,880	3,026	3,026
2.00	128.00	5,778	4,829	7,855
3.00	129.00	7.901	6,840	14,695
4.00	130.00	10,251	9,076	23,771
5.00	131.00	11,511	10,881	34,652

#### **Weir Structures Culvert / Orifice Structures** [C] [D] [B] [A] [A] [B] [C] [PrfRsr] 0.00 0.00 0.00 0.00 0.00 0.00 = 0.00Rise (in) = 24.00Crest Len (ft) 0.00 0.00 0.00 0.00 Crest El. (ft) = 0.000.00 Span (in) = 24.000.00 Weir Coeff. = 3.333.33 3.33 3.33 = 1 0 0 No. Barrels 0 = ---0.00 0.00 Weir Type Invert El. (ft) = 128.000.00 No No = No No Length (ft) = 200.000.00 0.00 0.00 Multi-Stage = 0.500.00 0.00 n/a Slope (%) N-Value = .012 .013 .013 n/a = 2.400 (by Contour) 0.60 Orifice Coeff. = 0.600.60 0.60 Exfil.(in/hr) = 0.00Multi-Stage = n/a No No No TW Elev. (ft)



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#### Pond No. 4 - BASIN 4

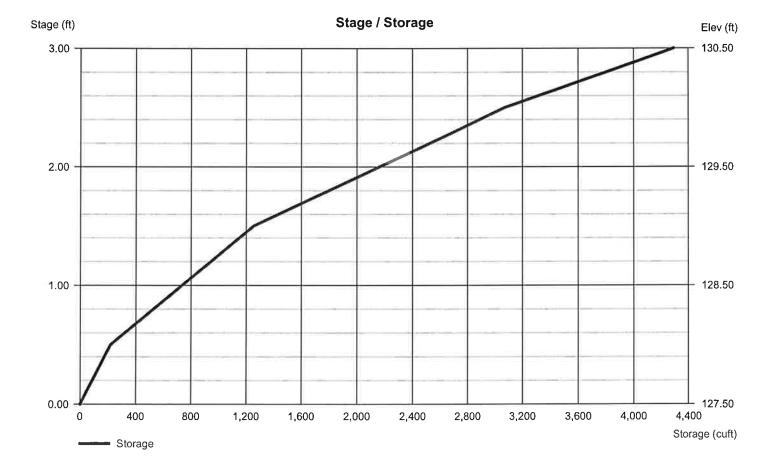
#### **Pond Data**

Contours - User-defined contour areas. Average end area method used for volume calculation. Begining Elevation = 127.50 ft

#### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	127.50	200	0	0
0.50	128.00	670	218	218
1.50	129.00	1,407	1,039	1,256
2.50	130.00	2,225	1,816	3,072
3.00	130.50	2,657	1,221	4,293

Culvert / Ori	fice Structi	Weir Structures								
	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]	
Rise (in)	= 0.00	0.00	0.00	0.00	Crest Len (ft)	= 8.00	0.00	0.00	0.00	
Span (in)	= 0.00	0.00	0.00	0.00	Crest El. (ft)	= 129.80	0.00	0.00	0.00	
No. Barrels	= 0	0	0	0	Weir Coeff.	= 2.60	3.33	3.33	3.33	
Invert El. (ft)	= 0.00	0.00	0.00	0.00	Weir Type	= Broad				
Length (ft)	= 0.00	0.00	0.00	0.00	Multi-Stage	= No	No	No	No	
Slope (%)	= 0.00	0.00	0.00	n/a						
N-Value	= .013	.013	.013	n/a						
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 2.400 (by	Contour)			
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00				



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#### Pond No. 5 - WATER QUALITY SWALE

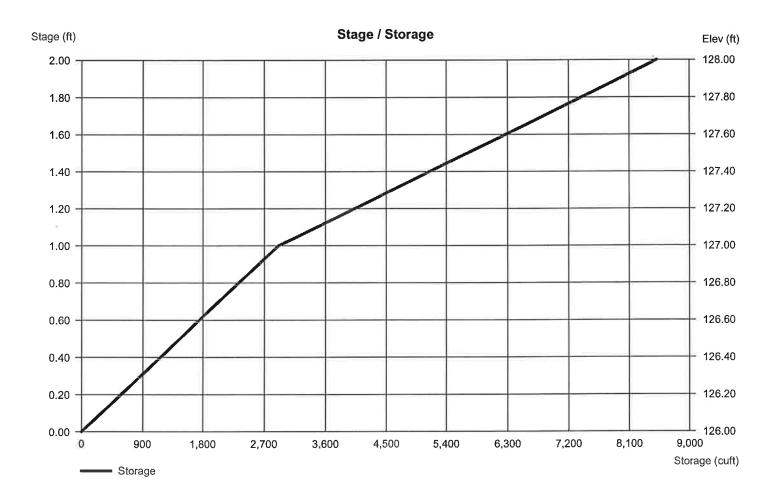
#### **Pond Data**

Contours - User-defined contour areas. Average end area method used for volume calculation. Begining Elevation = 126.00 ft

#### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	126.00	1,916	0	Ō
1.00	127.00	3,905	2,911	2,911
2.00	128.00	7,305	5,605	8,516

Culvert / Ori	fice Structu	Weir Structures								
	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]	
Rise (in)	= 18.00	0.00	0.00	0.00	Crest Len (ft)	= 0.00	0.00	0.00	0.00	
Span (in)	= 18.00	0.00	0.00	0.00	Crest El. (ft)	= 0.00	0.00	0.00	0.00	
No. Barrels	= 1	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33	
Invert El. (ft)	= 127.00	0.00	0.00	0.00	Weir Type	=	1444			
Length (ft)	= 140.00	0.00	0.00	0.00	Multi-Stage	= No	No	No	No	
Slope (%)	= 0.50	0.00	0.00	n/a						
N-Value	= .013	.013	.013	n/a						
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 2.400 (b)	y Contour)			
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00				



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#### Pond No. 8 - UPGRADED BASIN

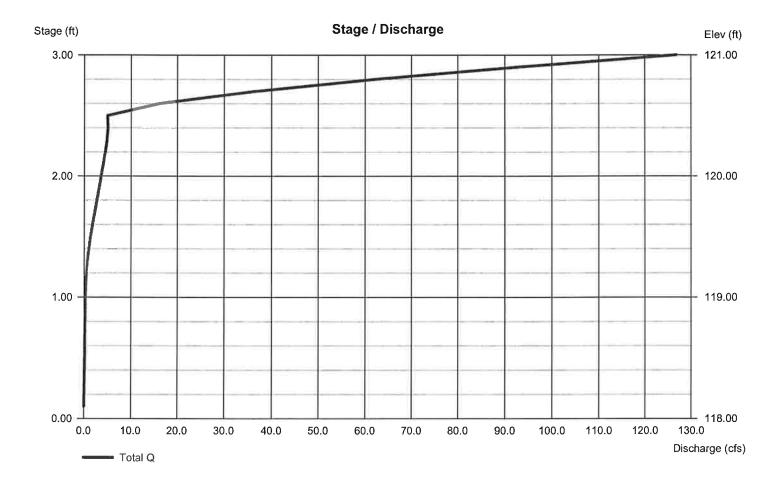
#### **Pond Data**

Contours - User-defined contour areas. Average end area method used for volume calculation. Begining Elevation = 118.00 ft

#### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	118.00	1,828	0	0
1.00	119.00	5,668	3,748	3,748
2.00	120.00	8,193	6,931	10,679
3.00	121.00	20,000	14,097	24,775

Culvert / Ori	fice Structu	Weir Structures								
	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]	
Rise (in)	= 18.00	0.00	0.00	0.00	Crest Len (ft)	= 130.00	0.00	0.00	0.00	
Span (in)	= 18.00	0.00	0.00	0.00	Crest El. (ft)	= 120.50	0.00	0.00	0.00	
No. Barrels	= 1	0	0	0	Weir Coeff.	= 2.60	3.33	3.33	3.33	
Invert El. (ft)	= 119.00	0.00	0.00	0.00	Weir Type	= Broad				
Length (ft)	= 200.00	0.00	0.00	0.00	Multi-Stage	= No	No	No	No	
Slope (%)	= 0.20	0.00	0.00	n/a						
N-Value	= .012	.013	.013	n/a						
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 2.400 (by	Contour)			
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00				



Hydrograph Summary Report
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Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	3.300	1	730	14,107	( <del></del>			EW-1 (PT. 1)
2	SCS Runoff	0.864	1	727	3,257			*******	EW-2 (PT. 2)
3	SCS Runoff	0.000	1	n/a	0			: <del>******</del>	EW-3
4	Combine	4.099	1	729	17,364	1, 2, 3			EXIST. TOTAL TO RIVER (PT. 3)
5	SCS Runoff	0.005	1	890	131	residence	12711112		EW-4
6	Reservoir	0.000	1	960	0	5	118.01	37.2	EXIST. BASIN (PT. 4)
7	SCS Runoff	0.000	1	n/a	0	( <del>Carrina</del>			EW-5A
8	SCS Runoff	0.000	1	n/a	0			SPERSON	E-5B
9	Combine	0.000	1	n/a	0	7, 8	:eorete:	OMMANUE.	E-5A + E-5B (PT. 5)
10	SCS Runoff	0.000	1	n/a	0	() <del>TARGERA</del>		******	EW-6 (PT. 6)
11	SCS Runoff	1.436	1	741	9,324			Salana.	PW-1A
12	SCS Runoff	0.007	1	825	199	:::::::::::::::::::::::::::::::::::::::			PW-1B
13	Reservoir	0.000	1	893	0	12	126.02	61.1	WATER QUALITY SWALE
14	Combine	1.436	1	741	9,324	11, 13	*****	1224145	TOTAL TO BASIN 2
15	Reservoir	0.000	1	1477	0	14	117.41	3,803	BASIN 2
16	Diversion1	0.289	1	1477	1,526	15	******		BASIN 2 INFILTRATION
17	Diversion2	0.000	1	n/a	-1,526	15			BASIN 2 OUTFLOW (PT. 1)
18	SCS Runoff	0.000	1	n/a	0			144004	PW-2
19	Reservoir	0.000	1	n/a	0	18	118.00	0.000	BASIN 1 (PT.2)
20	SCS Runoff	0.000	1	n/a	0		<u>-</u>	CHARLES T	PW-3
21	SCS Runoff	0.009	1	1337	283		*****		PW-5A
22	Reservoir	0.000	1	1254	0	21	126.03	104	BASIN 3
23	Combine	0.000	1	1484	0	15, 19, 22		(* <u>155656</u>	PROP. TOTAL TO RIVER (PT. 3)
24	SCS Runoff	0.002	1	827	51	******	*****	:	PW-5B (PT. 5)
25	SCS Runoff	0.136	1	745	851	HOCOURS	: SIMIRS	(	PW-6A
26	Reservoir	0.000	1	930	0	25	128.02	235	BASIN 4
27	SCS Runoff	0.000	1	n/a	0	******	*****	: <del>CONSTR</del>	PW-6B
28	Combine	0.000	1	930	0	26, 27	5 <del>8778775</del> 3		TOTAL TO PT. 6
			55						
Hydro_SPR_REV.gpw				Return F	Period: 1 Ye	ear	Tuesday,	Jun 3, 2008	

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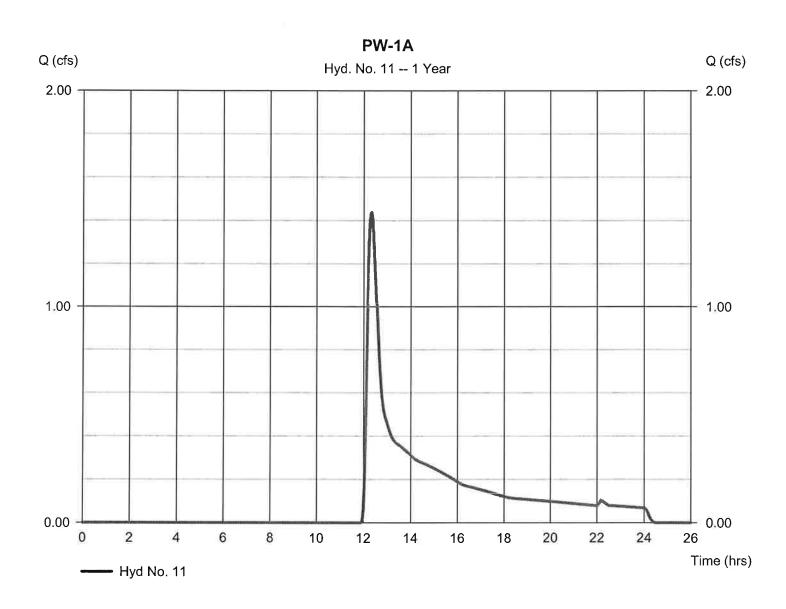
### Hyd. No. 11

PW-1A

Hydrograph type = SCS Runoff Peak discharge = 1.436 cfsStorm frequency = 1 yrs Time to peak  $= 12.35 \, hrs$ Time interval Hyd. volume = 1 min = 9.324 cuft Drainage area Curve number = 19.670 ac = 83\* Hydraulic length Basin Slope = 0.0 % = 0 ft

Tc method = TR55 Time of conc. (Tc) = 18.50 min
Total precip. = 1.00 in Distribution = Type III
Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(13.300 x 98) + (5.150 x 39)] / 19.670



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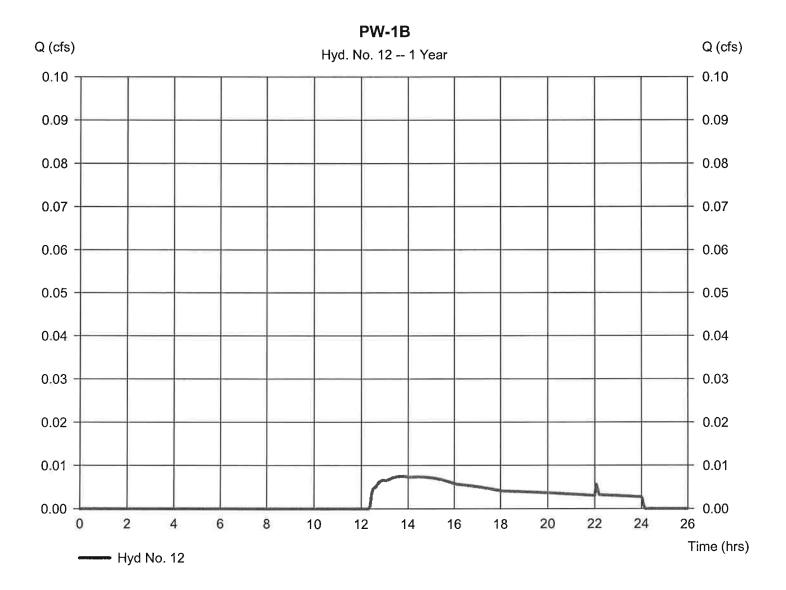
### Hyd. No. 12

PW-1B

Hydrograph type = SCS Runoff Storm frequency = 1 yrsTime interval = 1 min= 1.750 acDrainage area Basin Slope = 0.0 %Tc method = USER Total precip. = 1.00 inStorm duration = 24 hrs

Peak discharge = 0.007 cfs
Time to peak = 13.75 hrs
Hyd. volume = 199 cuft
Curve number = 75
Hydraulic length = 0 ft
Time of conc. (Tc) = 6.00 min
Distribution = Type III

Distribution = Type Shape factor = 484



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### Hyd. No. 13

### WATER QUALITY SWALE

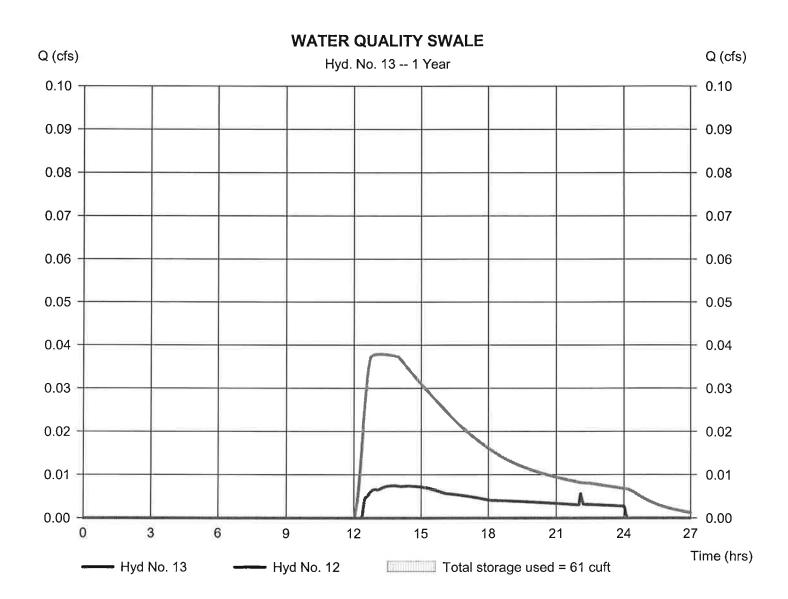
Hydrograph type = Reservoir Storm frequency = 1 yrs Time interval = 1 min Inflow hyd. No. = 12 - PW-1B

Reservoir name = WATER QUALITY SWALE

Peak discharge = 0.000 cfs Time to peak = 14.88 hrs Hyd. volume = 0 cuft

Max. Elevation = 126.02 ft Max. Storage = 61 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



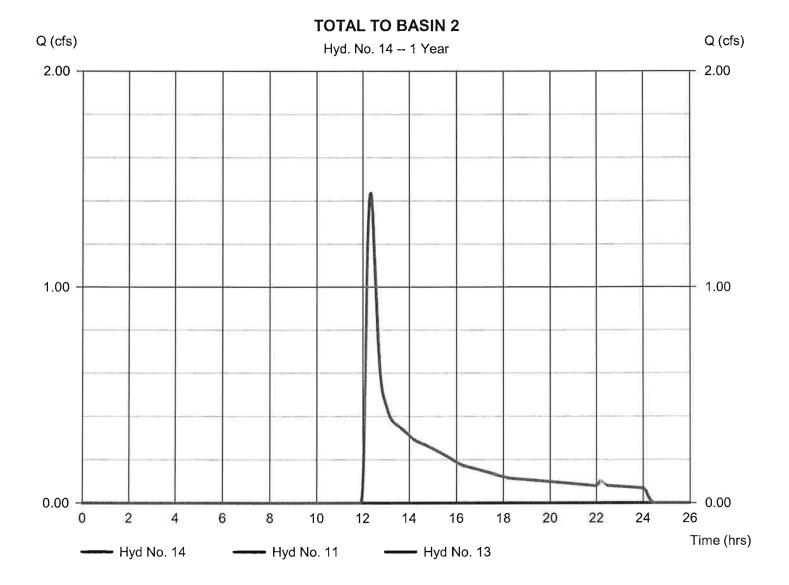
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### Hyd. No. 14

#### **TOTAL TO BASIN 2**

Hydrograph type = Combine Storm frequency = 1 yrs Time interval = 1 min Inflow hyds. = 11, 13 Peak discharge = 1.436 cfs Time to peak = 12.35 hrs Hyd. volume = 9,324 cuft Contrib. drain. area= 19.670 ac



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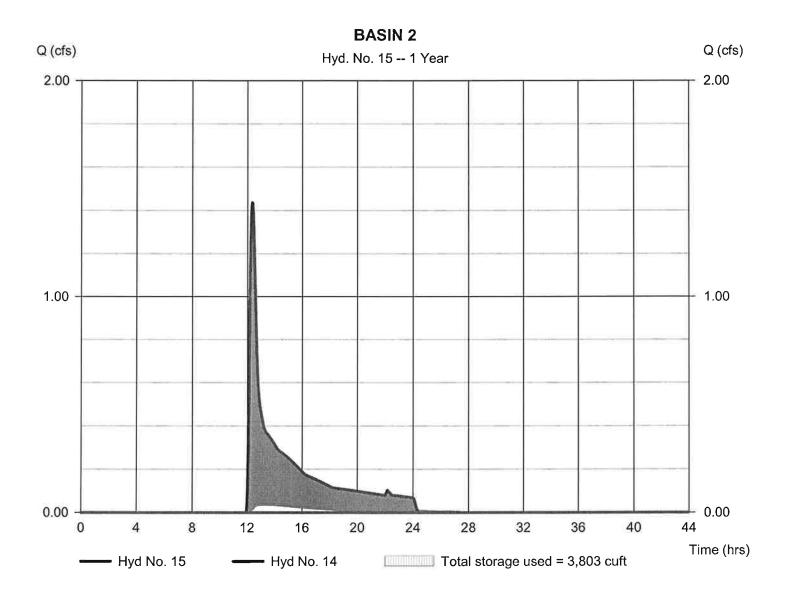
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### Hyd. No. 15

#### BASIN 2

Hydrograph type Peak discharge = Reservoir = 0.000 cfsStorm frequency = 1 yrsTime to peak  $= 24.62 \, hrs$ Time interval Hyd. volume = 0 cuft= 1 min Inflow hyd. No. Max. Elevation = 117.41 ft= 14 - TOTAL TO BASIN 2 Reservoir name = BASIN 2 Max. Storage = 3,803 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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### Hyd. No. 16

#### **BASIN 2 INFILTRATION**

Hydrograph type = Diversion1

Storm frequency = 1 yrsTime interval = 1 min

Inflow hydrograph = 15 - BASIN 2 Diversion method = Pond - BASIN 2

9 cfs disc to n arg 2 hrs ak 6 cuft /olui le

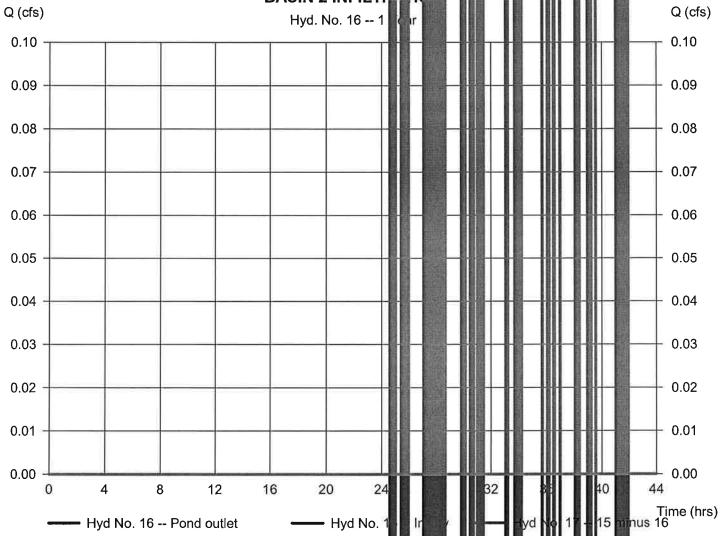
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### **BASIN 2 INFILTE**



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### Hyd. No. 17

**BASIN 2 OUTFLOW (PT. 1)** 

Hydrograph type = Diversion2

Storm frequency = 1 yrs

Time interval = 1 min

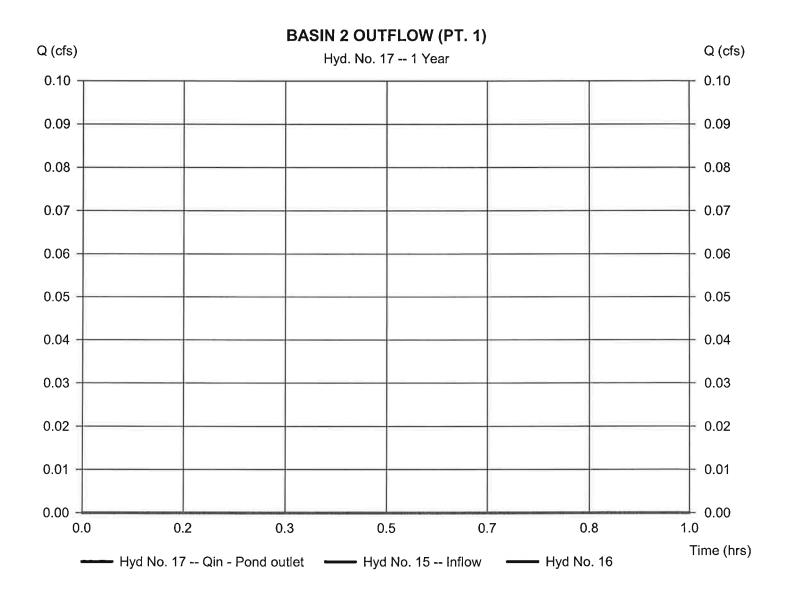
Inflow hydrograph = 15 - BASIN 2 Diversion method = Pond - BASIN 2 Peak discharge = 0.000 cfs

Time to peak = n/a

Hyd. volume = -1,526 cuft

2nd diverted hyd. = 16

Pond structure = Exfiltration



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### Hyd. No. 18

PW-2

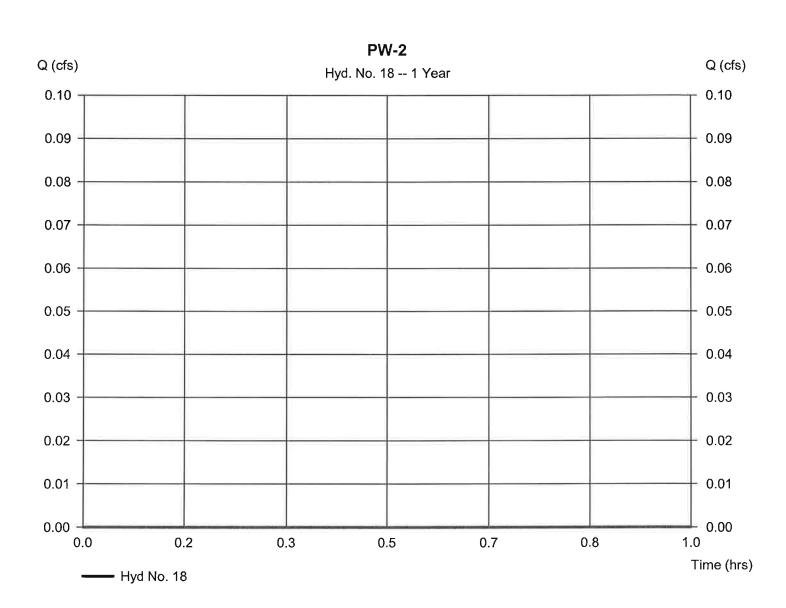
Hydrograph type= SCS RunoffPeaStorm frequency= 1 yrsTimeTime interval= 1 minHydDrainage area= 1.310 acCunBasin Slope= 0.0 %Hyd

Tc method = TR55
Total precip. = 1.00 in
Storm duration = 24 hrs

Peak discharge = 0.000 cfs
Time to peak = n/a
Hyd. volume = 0 cuft
Curve number = 56\*
Hydraulic length = 0 ft
Time of conc. (Tc) = 37.52 min

Distribution = Type III
Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(7.230 x 98) + (0.300 x 39)] / 1.310



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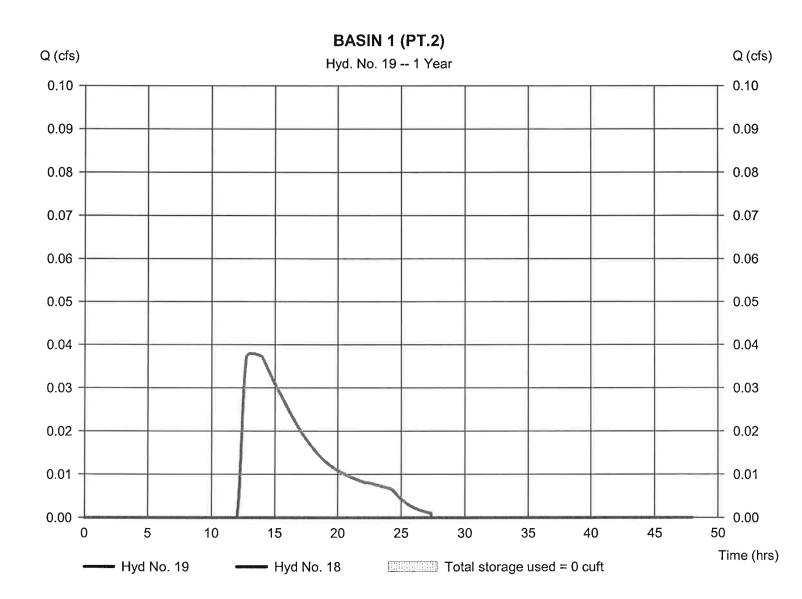
### Hyd. No. 19

BASIN 1 (PT.2)

Hydrograph type = Reservoir Peak discharge = 0.000 cfs

Storm frequency Time to peak = n/a= 1 yrsTime interval Hyd. volume = 1 min= 0 cuftMax. Elevation Inflow hyd. No.  $= 118.00 \, \text{ft}$ = 18 - PW-2 Reservoir name Max. Storage = UPGRADED BASIN = 0 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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### Hyd. No. 20

PW-3

Hydrograph type = SCS Runoff Storm frequency = 1 yrsTime interval = 1 min= 7.250 acDrainage area Basin Slope = 0.0 %Tc method = TR55

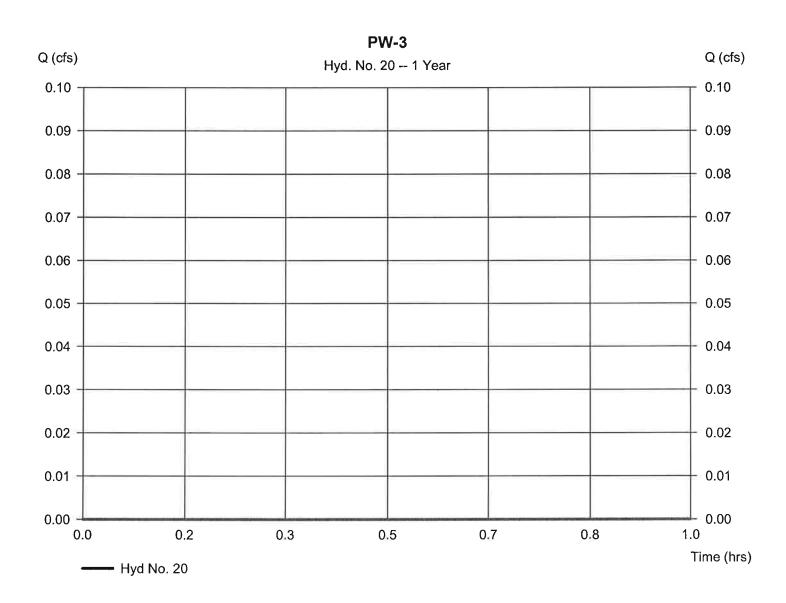
Total precip. = 1.00 inStorm duration = 24 hrs

Peak discharge = 0.000 cfs

Time to peak = n/aHyd. volume = 0 cuft Curve number = 48\*Hydraulic length = 0 ft

Time of conc. (Tc) = 18.81 minDistribution = Type III = 484 Shape factor

<sup>\*</sup> Composite (Area/CN) = [(7.240 x 39)] / 7.250



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### Hyd. No. 21

PW-5A

Hydrograph type = SCS Runoff

Storm frequency = 1 yrs
Time interval = 1 min
Drainage area = 10.000 ac
Basin Slope = 0.0 %

Basin Slope = 0.0 % Tc method = TR55 Total precip. = 1.00 in

Storm duration = 24 hrs

Peak discharge = 0.009 cfs Time to peak = 22.28 hrs

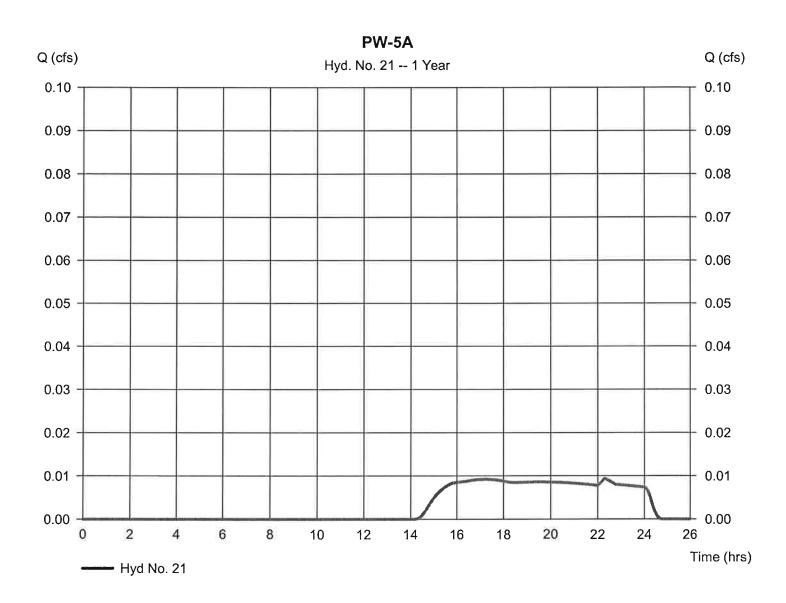
Hyd. volume = 283 cuft
Curve number = 71\*

Hydraulic length = 0 ft

Time of conc. (Tc) = 27.26 min Distribution = Type III

Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(0.880 x 98) + (3.950 x 39)] / 10.000



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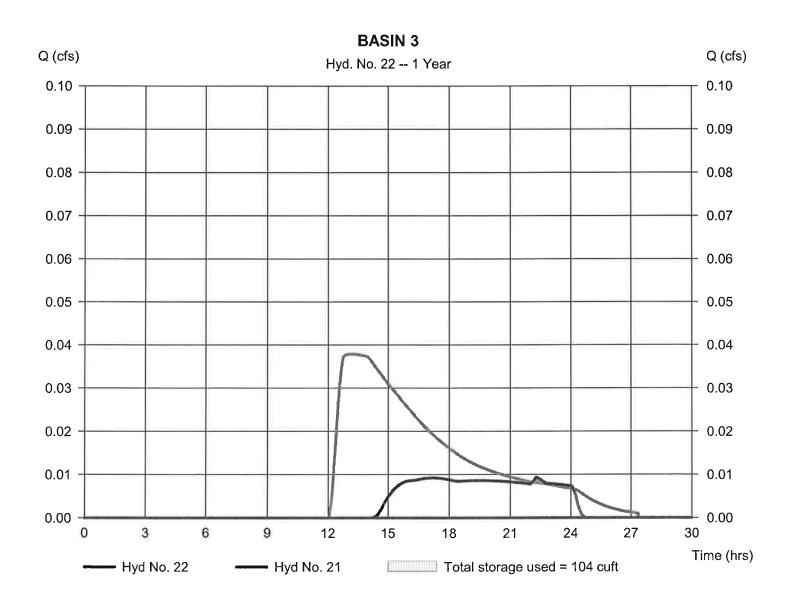
### Hyd. No. 22

BASIN 3

Hydrograph type = Reservoir
Storm frequency = 1 yrs
Time interval = 1 min
Inflow hyd. No. = 21 - PW-5A
Reservoir name = BASIN 3

Peak discharge = 0.000 cfs
Time to peak = 20.90 hrs
Hyd. volume = 0 cuft
Max. Elevation = 126.03 ft
Max. Storage = 104 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



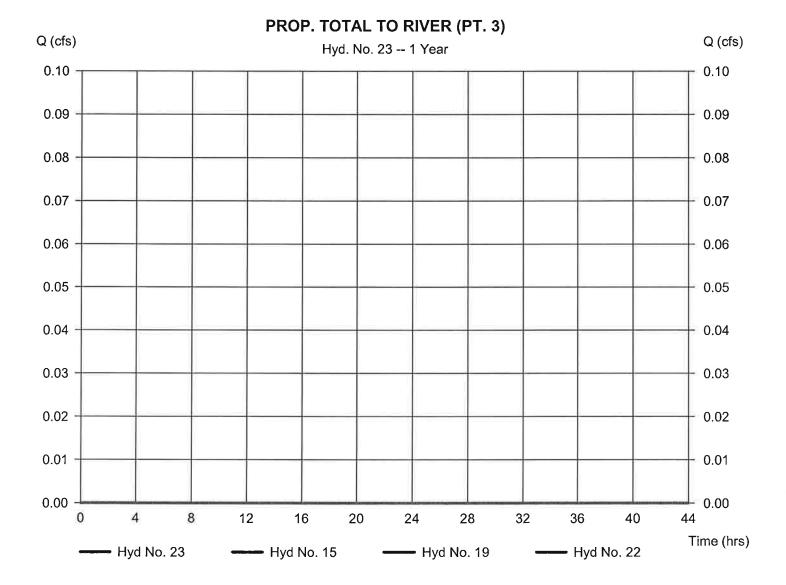
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### Hyd. No. 23

PROP. TOTAL TO RIVER (PT. 3)

Hydrograph type = Combine Storm frequency = 1 yrs Time interval = 1 min Inflow hyds. = 15, 19, 22 Peak discharge = 0.000 cfs
Time to peak = 24.73 hrs
Hyd. volume = 0 cuft
Contrib. drain. area= 0.000 ac



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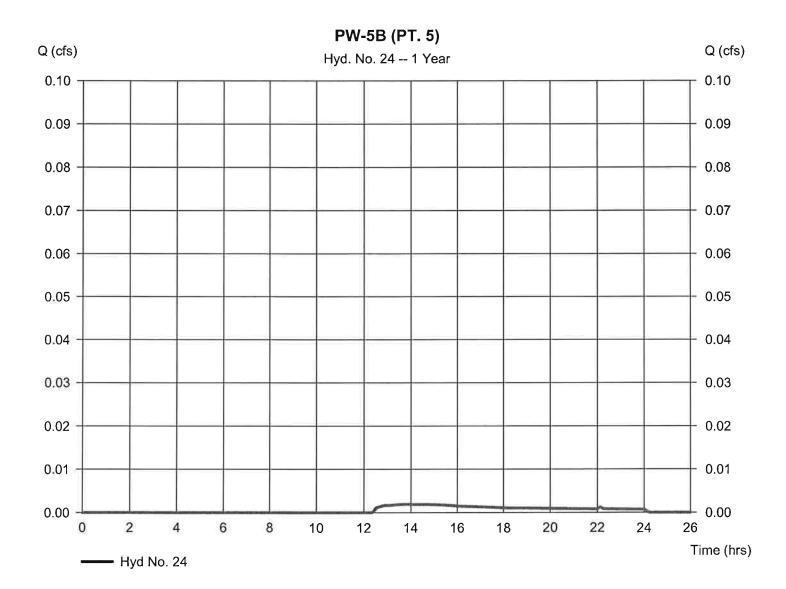
Tuesday, Jun 3, 2008

### Hyd. No. 24

PW-5B (PT. 5)

Hydrograph type = SCS Runoff Peak discharge = 0.002 cfsStorm frequency Time to peak  $= 13.78 \, hrs$ = 1 yrsTime interval Hyd. volume = 51 cuft = 1 min Curve number = 75 Drainage area = 0.460 acBasin Slope Hydraulic length = 0 ft= 0.0 %

Tc method = TR55 Time of conc. (Tc) = 10.01 min
Total precip. = 1.00 in Distribution = Type III
Storm duration = 24 hrs Shape factor = 484



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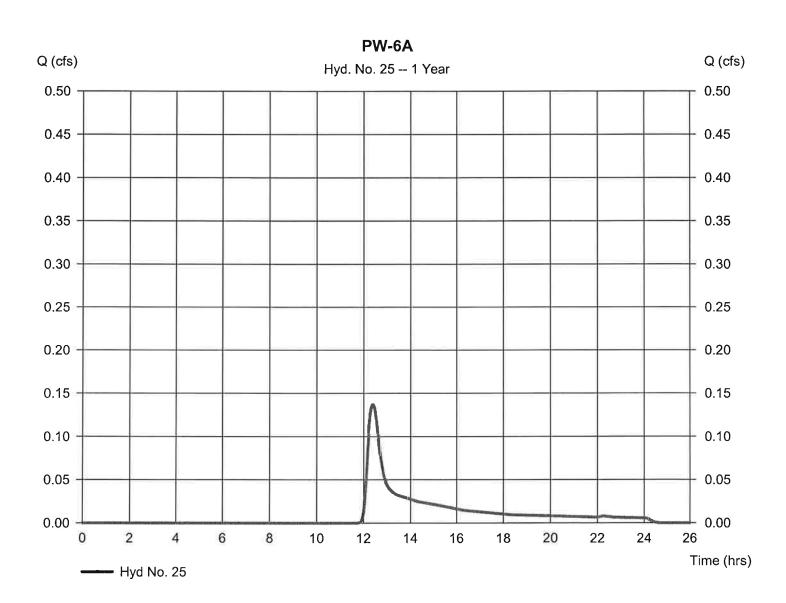
### Hyd. No. 25

PW-6A

Hydrograph type = SCS Runoff Peak discharge = 0.136 cfsStorm frequency = 1 yrsTime to peak  $= 12.42 \, hrs$ Time interval Hyd. volume = 1 min = 851 cuft Drainage area = 1.350 acCurve number = 85\* Hydraulic length = 0 ftBasin Slope = 0.0 %

Tc method = TR55 Time of conc. (Tc) = 24.74 min
Total precip. = 1.00 in Distribution = Type III
Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(0.380 x 39) + (0.650 x 98)] / 1.350



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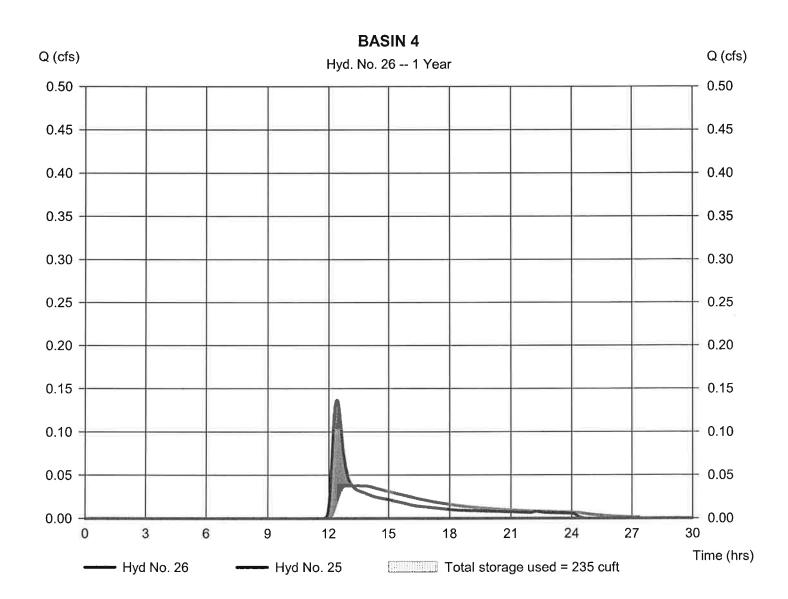
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### Hyd. No. 26

**BASIN 4** 

Hydrograph type Peak discharge = 0.000 cfs= Reservoir Storm frequency Time to peak  $= 15.50 \, hrs$ = 1 yrs Time interval Hyd. volume = 0 cuft = 1 min Inflow hyd. No. Max. Elevation = 128.02 ft= 25 - PW-6A Reservoir name = BASIN 4 Max. Storage = 235 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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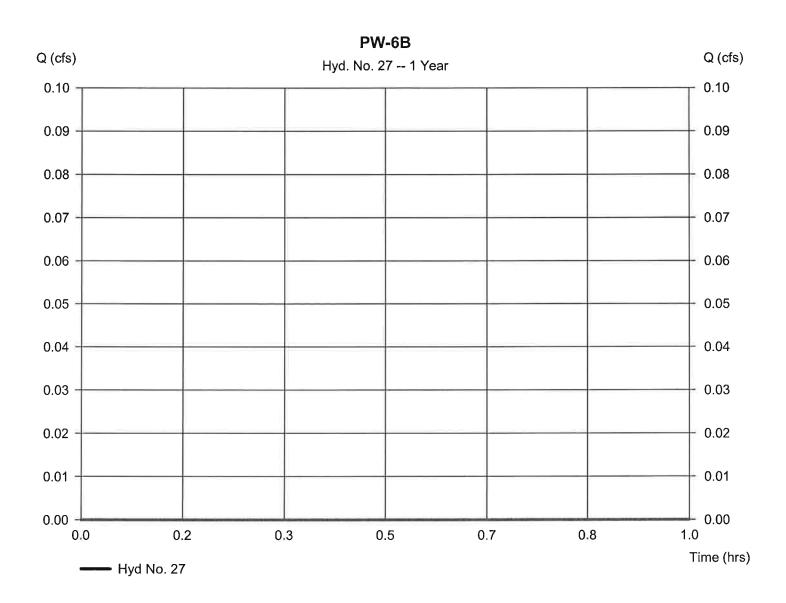
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### Hyd. No. 27

PW-6B

= SCS Runoff Peak discharge = 0.000 cfsHydrograph type Storm frequency Time to peak = n/a= 1 yrsTime interval Hyd. volume = 1 min= 0 cuftCurve number = 39\* Drainage area = 0.600 acHydraulic length Basin Slope = 0.0 %= 0 ftTime of conc. (Tc) = 6.00 minTc method = USER Total precip. = 1.00 inDistribution = Type III Storm duration = 484 = 24 hrs Shape factor

<sup>\*</sup> Composite (Area/CN) = [(1.610 x 39)] / 0.600



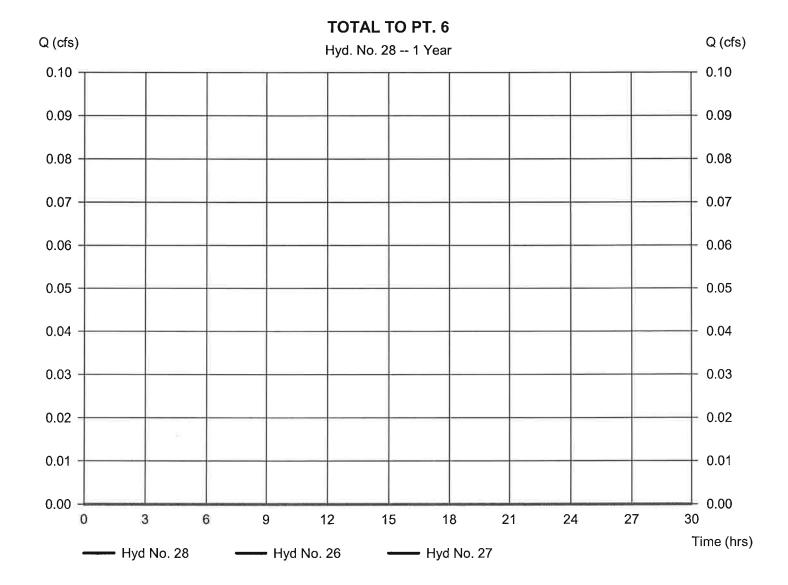
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### Hyd. No. 28

TOTAL TO PT. 6

Hydrograph type = Combine Storm frequency = 1 yrs Time interval = 1 min Inflow hyds. = 26, 27 Peak discharge = 0.000 cfs Time to peak = 15.50 hrs Hyd. volume = 0 cuft Contrib. drain. area= 0.600 ac



Hydrograph Summary Report
Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	31.68	1	728	115,076	Stritten	*****	******	EW-1 (PT. 1)
2	SCS Runoff	8.251	1	726	26,572				EW-2 (PT. 2)
3	SCS Runoff	0.352	1	773	6,744	200000	WEEKEN T	<del>uniter</del> :	EW-3
4	Combine	39.44	1	727	148,392	1, 2, 3			EXIST. TOTAL TO RIVER (PT. 3)
5	SCS Runoff	1.373	1	730	5,489	\		<del>57/10</del> /	EW-4
6	Reservoir	0.000	1	785	0	5	118.60	2,248	EXIST. BASIN (PT. 4)
7	SCS Runoff	0.029	1	922	820		*****	*****	EW-5A
8	SCS Runoff	0.047	1	825	1,209	ATTREST.	#######//		E-5B
9	Combine	0.072	1	897	2,029	7, 8	<u> </u>	<u> 1865-185</u>	E-5A + E-5B (PT. 5)
10	SCS Runoff	1.095	1	724	4,083		******		EW-6 (PT. 6)
11	SCS Runoff	25.32	1	733	107,826	19 <del>110110</del> 0	######################################		PW-1A
12	SCS Runoff	2.087	1	725	6,726	Fallman C	MINISTERN)		PW-1B
13	Reservoir	0.000	1	734	0	12	126.99	2,879	WATER QUALITY SWALE
14	Combine	25.32	1	733	107,826	11, 13	<b>504669</b> .0		TOTAL TO BASIN 2
15	Reservoir	16.64	1	745	82,763	14	120.76	25,670	BASIN 2
16	Diversion1	0.601	1	745	16,824	15	*****		BASIN 2 INFILTRATION
17	Diversion2	16.04	1	745	65,940	15	******	20205	BASIN 2 OUTFLOW (PT. 1)
18	SCS Runoff	0.095	1	765	1,177	-	0200001		PW-2
19	Reservoir	0.000	1	798	0	18	118.10	368	BASIN 1 (PT.2)
20	SCS Runoff	0.072	1	893	1,948		######################################	STORES.	PW-3
21	SCS Runoff	5.236	1	743	29,497		22202		PW-5A
22	Reservoir	1.175	1	781	8,948	21	128.44	10,868	BASIN 3
23	Combine	16.64	1	745	91,712	15, 19, 22	<del></del>		PROP. TOTAL TO RIVER (PT. 3)
24	SCS Runoff	0.476	1	727	1,715		vene		PW-5B (PT. 5)
25	SCS Runoff	1.697	1	737	8,197		***************************************	*****	PW-6A
26	Reservoir	1.083	1	752	2,070	25	129.94	2,955	BASIN 4
27	SCS Runoff	0.000	1	n/a	0		Marie V	- Finale	PW-6B
28	Combine	1.083	1	752	2,070	26, 27	*****	*****	TOTAL TO PT. 6
Hyd	Hydro_SPR_REV.gpw				Return F	Period: 2 Ye	ear	Tuesday, c	Jun 3, 2008

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### Hyd. No. 11

PW-1A

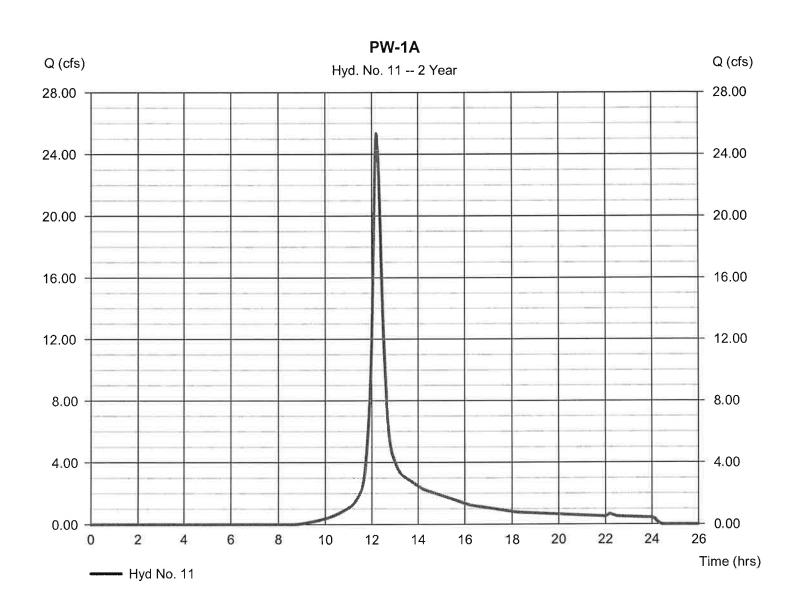
Peak discharge = 25.32 cfsHydrograph type = SCS Runoff Time to peak Storm frequency = 12.22 hrs= 2 yrsHyd. volume Time interval = 1 min = 107,826 cuft Curve number = 83\* Drainage area = 19.670 acBasin Slope Hydraulic length = 0 ft= 0.0 %Time of conc. (Tc) = 18.50 minTc method

Tc method = TR55 Time of conc. (Tc) = 18.50 min

Total precip. = 3.10 in Distribution = Type III

Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(13.300 x 98) + (5.150 x 39)] / 19.670



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### Hyd. No. 12

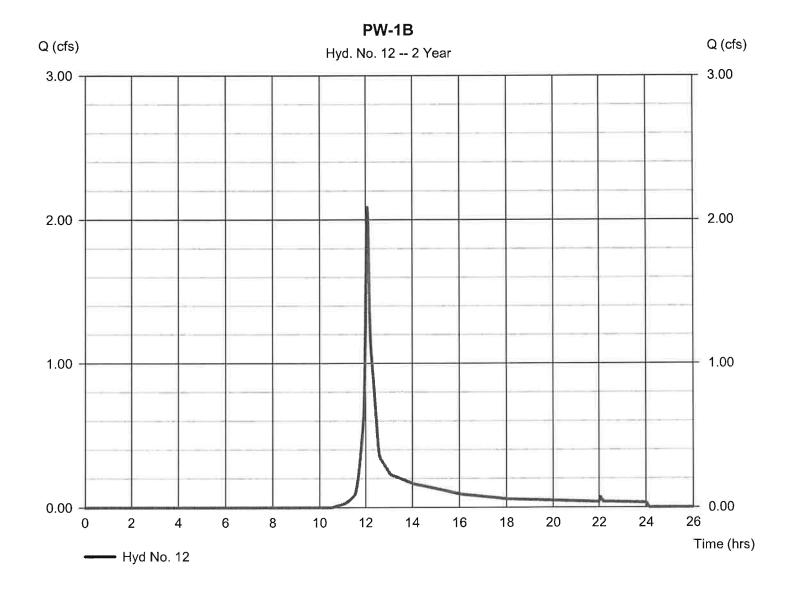
PW-1B

Hydrograph type = SCS Runoff Storm frequency = 2 yrsTime interval = 1 min Drainage area = 1.750 acBasin Slope = 0.0 % Tc method = USER Total precip. = 3.10 inStorm duration = 24 hrs

Peak discharge = 2.087 cfs
Time to peak = 12.08 hrs
Hyd. volume = 6,726 cuft
Curve number = 75
Hydraulic length = 0 ft
Time of conc. (Tc) = 6.00 min
Distribution = Type III

= 484

Shape factor



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### Hyd. No. 13

#### WATER QUALITY SWALE

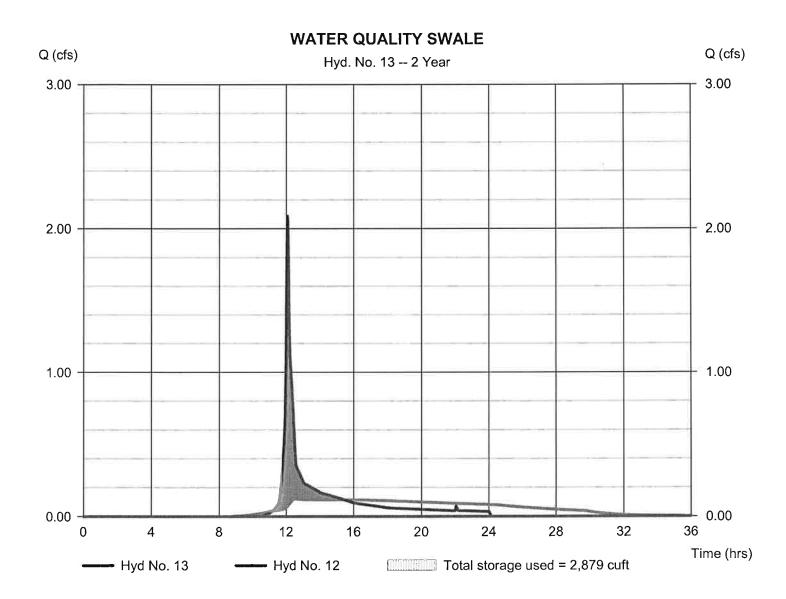
Hydrograph type = Reservoir Storm frequency = 2 yrs Time interval = 1 min Inflow hyd. No. = 12 - PW-1B

Reservoir name = WATER QUALITY SWALE

Peak discharge = 0.000 cfs Time to peak = 12.23 hrs Hyd. volume = 0 cuft

Max. Elevation = 126.99 ft Max. Storage = 2,879 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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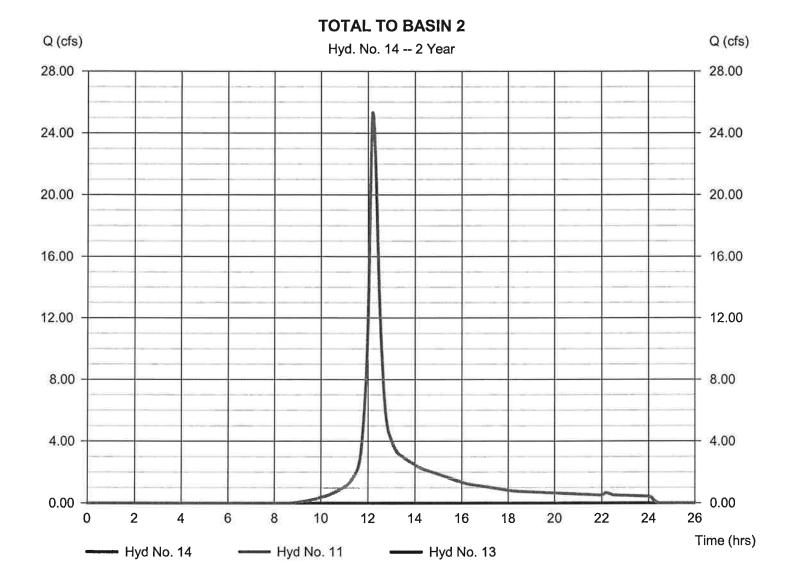
Tuesday, Jun 3, 2008

### Hyd. No. 14

#### **TOTAL TO BASIN 2**

Hydrograph type = Combine Storm frequency = 2 yrs Time interval = 1 min Inflow hyds. = 11, 13

Peak discharge = 25.32 cfs Time to peak = 12.22 hrs Hyd. volume = 107,826 cuft Contrib. drain. area= 19.670 ac



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#### Hyd. No. 15

**BASIN 2** 

Hydrograph type = Reservoir Storm frequency = 2 yrs Time interval = 1 min

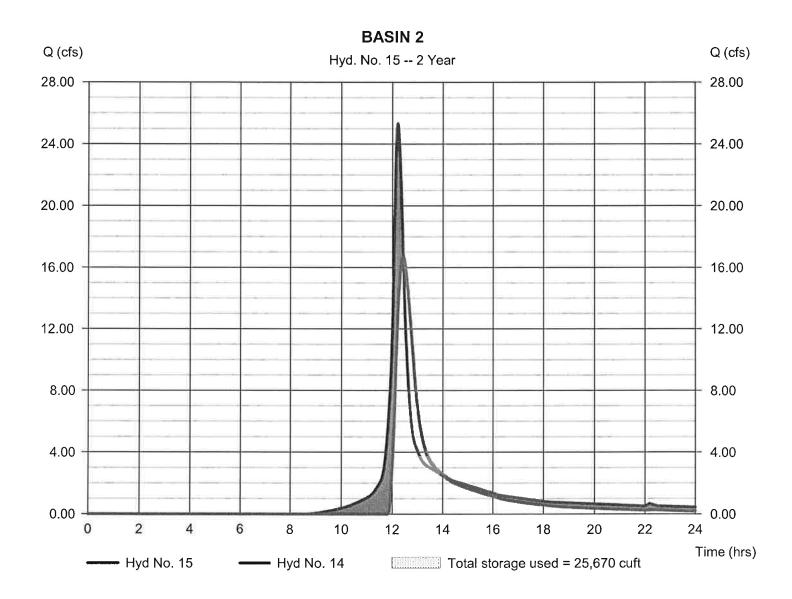
Time interval = 1 min Inflow hyd. No. = 14 - TOTAL TO BASIN 2

Reservoir name = BASIN 2

Peak discharge = 16.64 cfs

Time to peak = 12.42 hrs Hyd. volume = 82,763 cuft Max. Elevation = 120.76 ft

Max. Storage = 25,670 cuft



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### Hyd. No. 16

#### **BASIN 2 INFILTRATION**

Hydrograph type = Diversion1 Storm frequency = 2 yrs

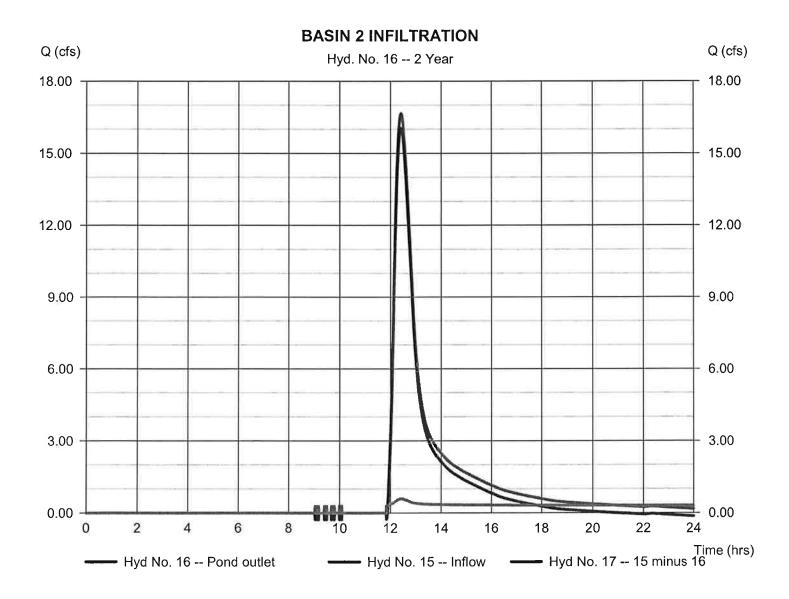
Time interval = 1 min

Inflow hydrograph = 15 - BASIN 2 Diversion method = Pond - BASIN 2

Peak discharge = 0.601 cfsTime to peak = 12.42 hrsHyd. volume = 16,824 cuft

2nd diverted hyd. = 17

Pond structure = Exfiltration



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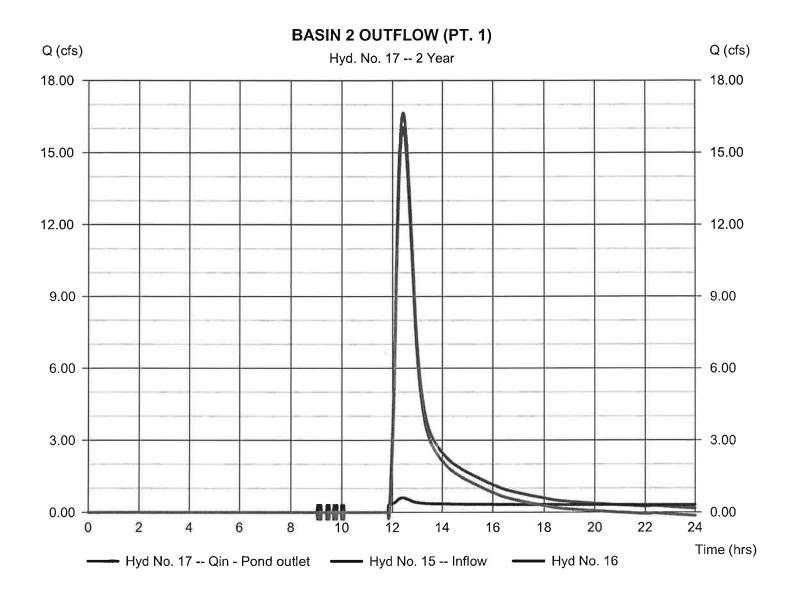
### Hyd. No. 17

BASIN 2 OUTFLOW (PT. 1)

Hydrograph type = Diversion2 Peak discharge = 16.04 cfs
Storm frequency = 2 yrs Time to peak = 12.42 hrs
Time interval = 1 min Hyd. volume = 65,940 cuft

Inflow hydrograph = 15 - BASIN 2 2nd diverted hyd. = 16

Diversion method = Pond - BASIN 2 Pond structure = Exfiltration



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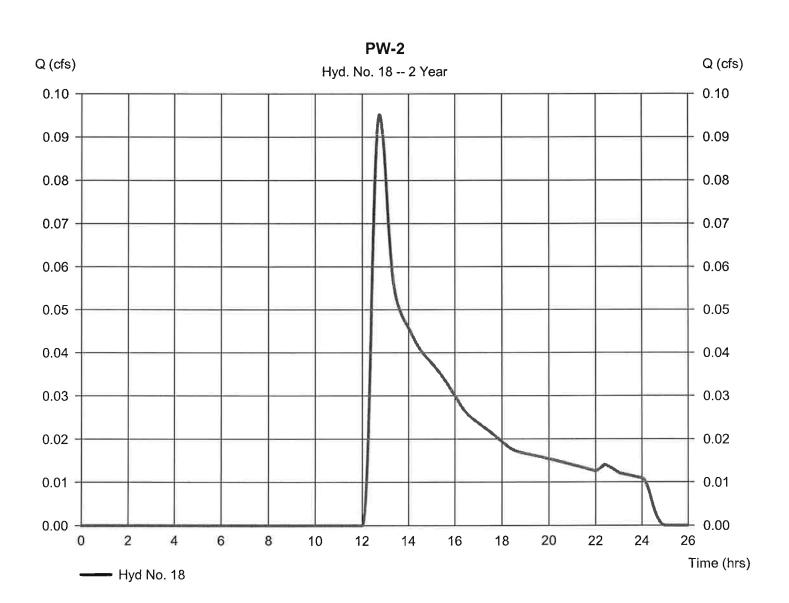
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#### Hyd. No. 18

PW-2

Hydrograph type = SCS Runoff Peak discharge = 0.095 cfsStorm frequency Time to peak  $= 12.75 \, hrs$ = 2 yrs Time interval = 1 min Hyd. volume = 1,177 cuftDrainage area = 1.310 acCurve number = 56\* Basin Slope Hydraulic length = 0.0 %= 0 ftTime of conc. (Tc) = 37.52 minTc method = TR55 Total precip. Distribution = Type III = 3.10 inStorm duration Shape factor = 484 = 24 hrs

<sup>\*</sup> Composite (Area/CN) = [(7.230 x 98) + (0.300 x 39)] / 1.310



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### Hyd. No. 19

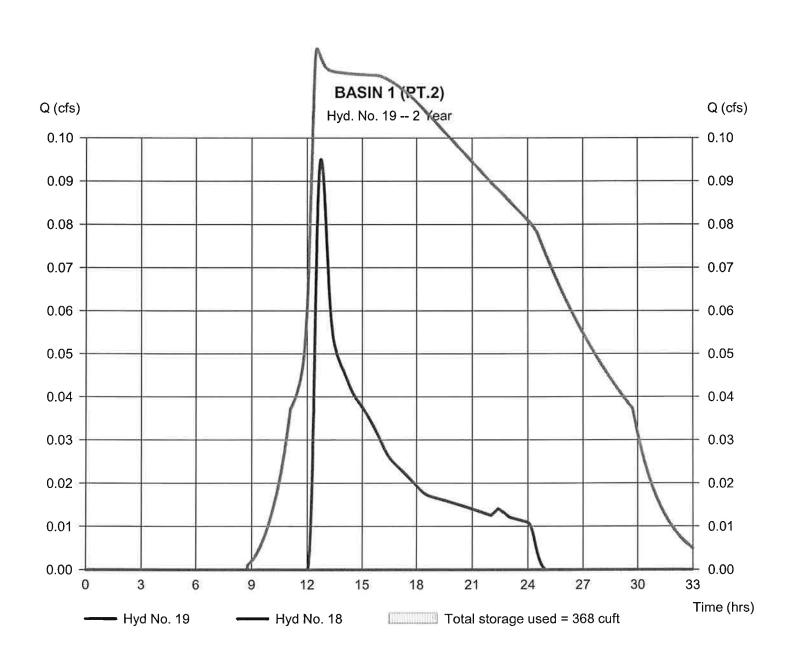
BASIN 1 (PT.2)

Hydrograph type = Reservoir Storm frequency = 2 yrs Time interval = 1 min Inflow hyd. No. = 18 - PW-2

Reservoir name = UPGRADED BASIN

Peak discharge = 0.000 cfs
Time to peak = 13.30 hrs
Hyd. volume = 0 cuft
Max. Elevation = 118.10 ft

Max. Storage = 368 cuft



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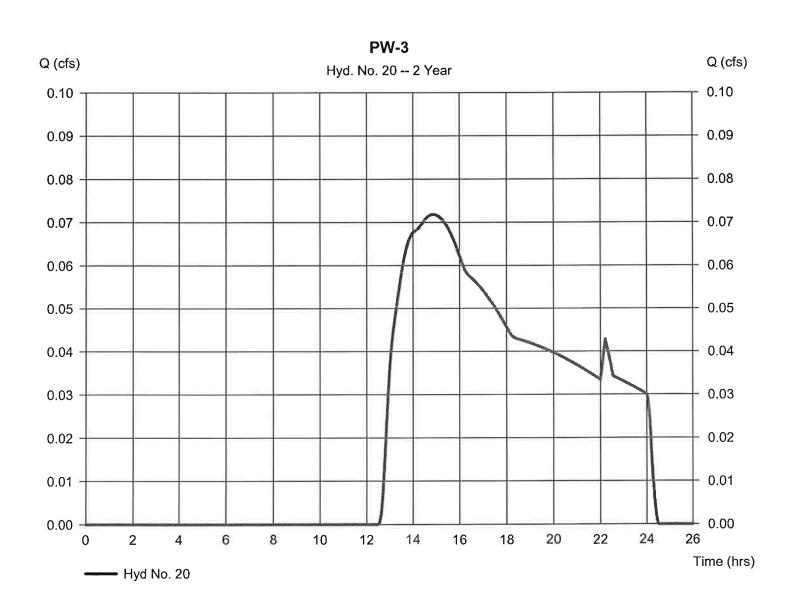
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#### Hyd. No. 20

PW-3

= 0.072 cfsHydrograph type = SCS Runoff Peak discharge Time to peak = 14.88 hrs Storm frequency = 2 yrs Time interval = 1 min Hyd. volume = 1,948 cuft = 48\* Drainage area = 7.250 acCurve number Basin Slope Hydraulic length = 0 ft= 0.0 %Time of conc. (Tc) = 18.81 minTc method = TR55 Total precip. Distribution = Type III = 3.10 in= 484 Storm duration Shape factor = 24 hrs

<sup>\*</sup> Composite (Area/CN) = [(7.240 x 39)] / 7.250



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#### Hyd. No. 21

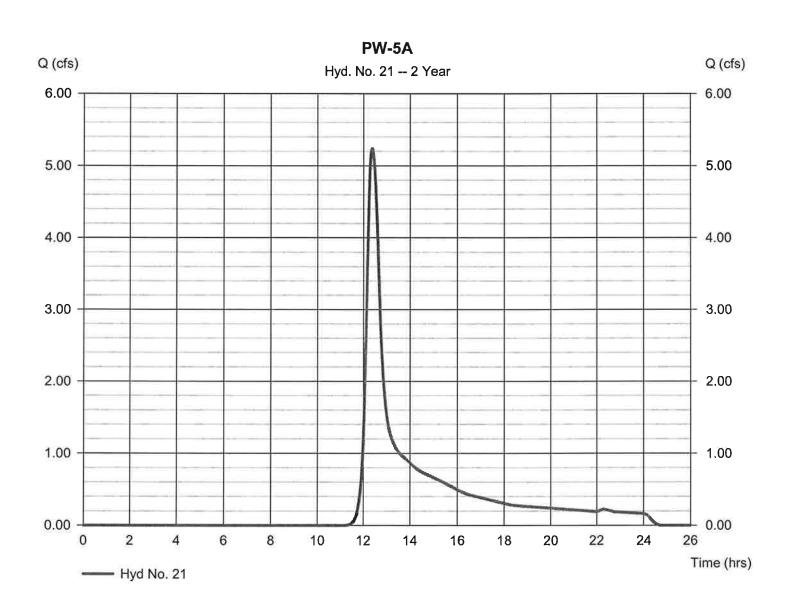
PW-5A

Hydrograph type = SCS Runoff Peak discharge = 5.236 cfs
Storm frequency = 2 yrs Time to peak = 12.38 hrs
Time interval = 1 min Hyd. volume = 29,497 cuft

Drainage area = 10.000 ac Curve number =  $71^*$  Basin Slope = 0.0% Hydraulic length = 0 ft

Tc method = TR55 Time of conc. (Tc) = 27.26 min
Total precip. = 3.10 in Distribution = Type III
Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(0,880 x 98) + (3.950 x 39)] / 10.000



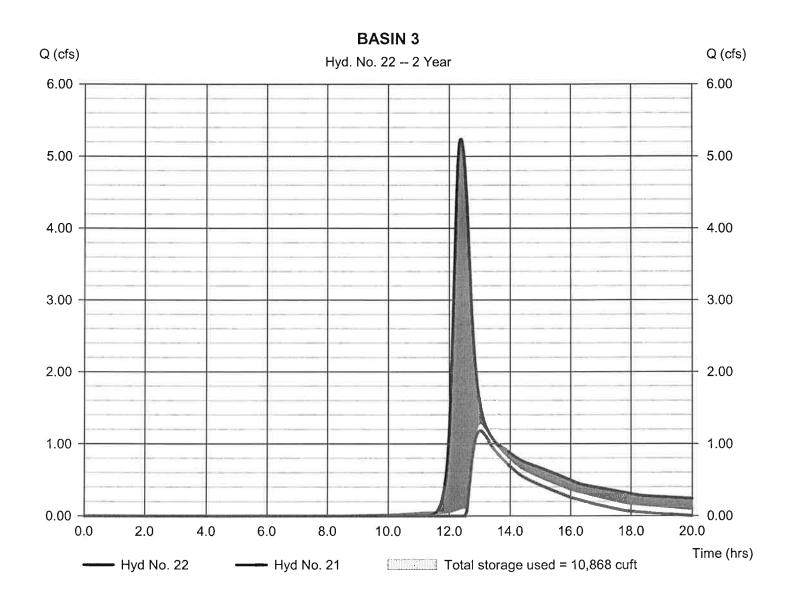
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### Hyd. No. 22

BASIN 3

Hydrograph type = Reservoir Peak discharge = 1.175 cfsStorm frequency Time to peak  $= 13.02 \, hrs$ = 2 yrsTime interval = 1 min Hyd. volume = 8,948 cuftMax. Elevation Inflow hyd. No. = 21 - PW-5A = 128.44 ftReservoir name = BASIN 3 Max. Storage = 10,868 cuft



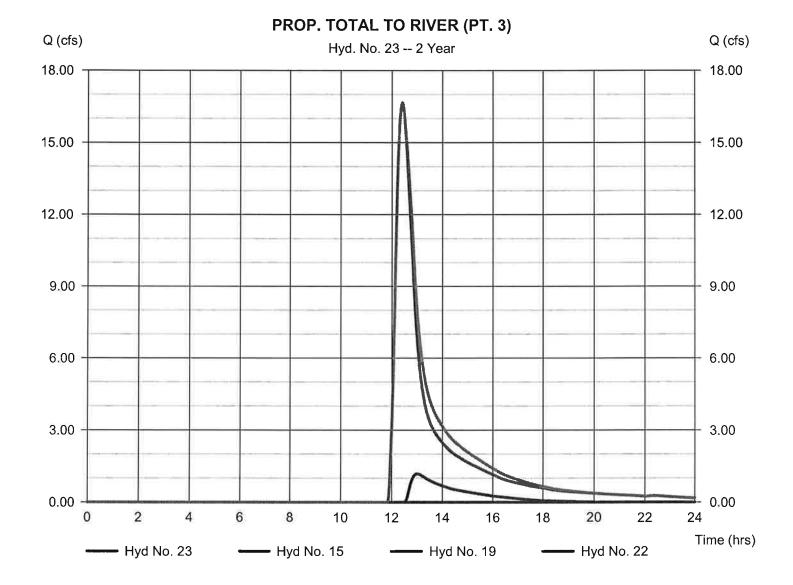
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### Hyd. No. 23

PROP. TOTAL TO RIVER (PT. 3)

Hydrograph type = Combine Storm frequency = 2 yrs Time interval = 1 min Inflow hyds. = 15, 19, 22 Peak discharge = 16.64 cfs Time to peak = 12.42 hrs Hyd. volume = 91,712 cuft Contrib. drain. area= 0.000 ac



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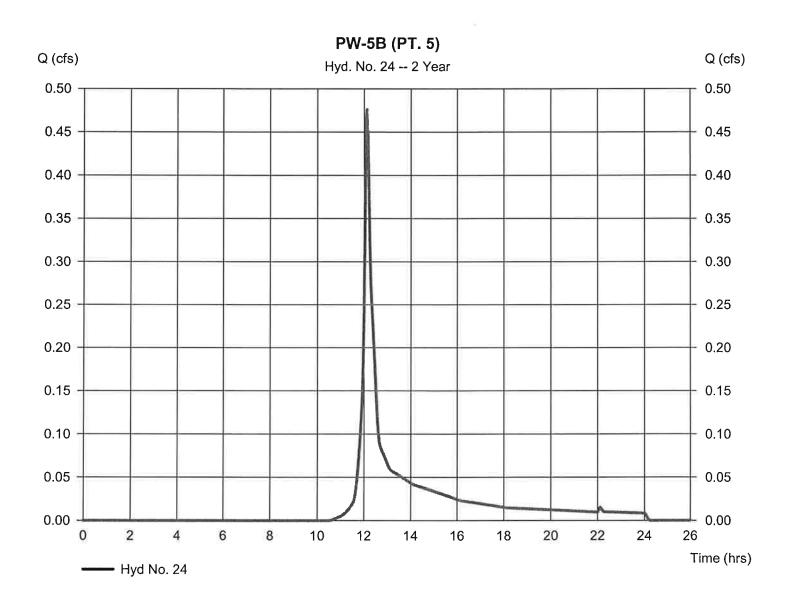
#### Hyd. No. 24

PW-5B (PT. 5)

Hydrograph type= SCS RunoffPeak discharge= 0.476 cfsStorm frequency= 2 yrsTime to peak= 12.12 hrsTime interval= 1 minHyd. volume= 1,715 cuft

Drainage area = 0.460 ac Curve number = 75 Basin Slope = 0.0 % Hydraulic length = 0 ft

Tc method = TR55 Time of conc. (Tc) = 10.01 min
Total precip. = 3.10 in Distribution = Type III
Storm duration = 24 hrs Shape factor = 484



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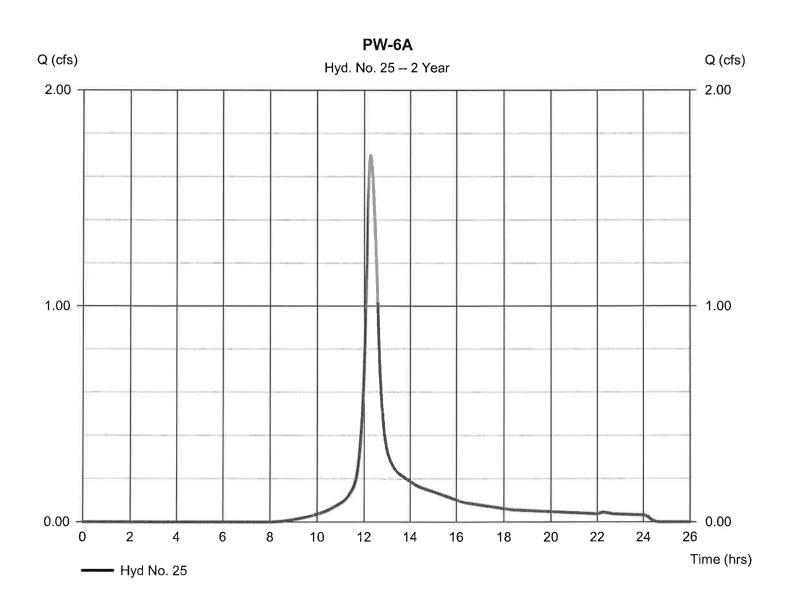
#### Hyd. No. 25

PW-6A

= SCS Runoff Hydrograph type Peak discharge = 1.697 cfsStorm frequency Time to peak = 2 yrs = 12.28 hrsTime interval = 1 min Hyd. volume = 8,197 cuft Drainage area = 1.350 acCurve number = 85\* Basin Slope = 0.0 % Hydraulic length = 0 ft

Tc method = TR55 Time of conc. (Tc) = 24.74 min
Total precip. = 3.10 in Distribution = Type III
Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.380 \times 39) + (0.650 \times 98)] / 1.350$ 



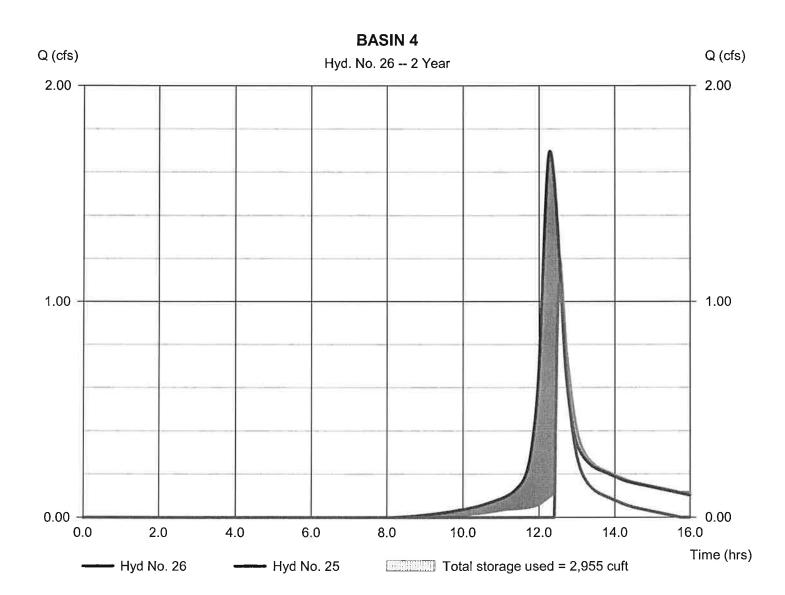
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#### Hyd. No. 26

**BASIN 4** 

Peak discharge Hydrograph type = Reservoir = 1.083 cfsStorm frequency = 2 yrs Time to peak  $= 12.53 \, hrs$ Time interval = 1 min Hyd. volume = 2,070 cuftInflow hyd. No. = 25 - PW-6A Max. Elevation = 129.94 ftReservoir name = BASIN 4 Max. Storage = 2,955 cuft



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### Hyd. No. 27

PW-6B

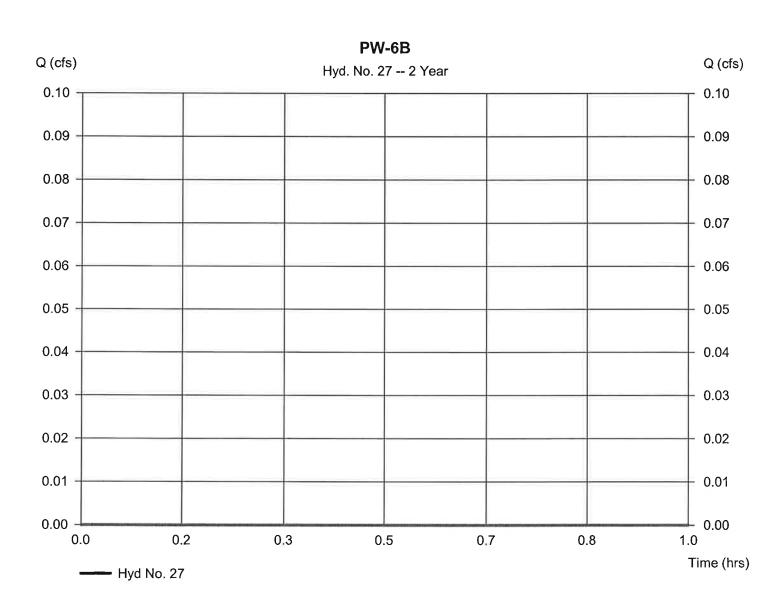
Hydrograph type = SCS Runoff Storm frequency = 2 yrsTime interval = 1 min Drainage area = 0.600 acBasin Slope = 0.0 % Tc method = USER Total precip. = 3.10 inStorm duration = 24 hrs

Peak discharge = 0.000 cfs
Time to peak = n/a
Hyd. volume = 0 cuft
Curve number = 39\*

Hydraulic length = 0 ft

Time of conc. (Tc) = 6.00 min
Distribution = Type III
Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(1.610 x 39)] / 0.600



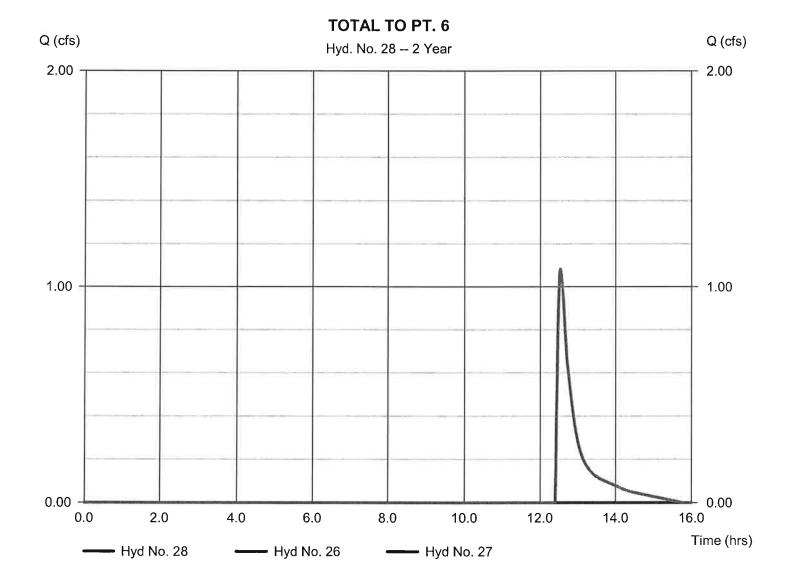
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### Hyd. No. 28

TOTAL TO PT. 6

Hydrograph type = Combine Storm frequency = 2 yrs Time interval = 1 min Inflow hyds. = 26, 27 Peak discharge = 1.083 cfs Time to peak = 12.53 hrs Hyd. volume = 2,070 cuft Contrib. drain. area= 0.600 ac



# Hydrograph Summary Report Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	53.09	1	728	195,223	-	******		EW-1 (PT. 1)
2	SCS Runoff	13.82	1	725	45,078	:: <del>2.2522=</del>		244224	EW-2 (PT. 2)
3	SCS Runoff	3.324	1	753	26,655		*****		EW-3
4	Combine	66.75	1	727	266,955	1, 2, 3			EXIST. TOTAL TO RIVER (PT. 3)
5	SCS Runoff	2.927	1	729	11,135	SAMMIN	520000		EW-4
6	Reservoir	0.000	1	732	0	5	119.19	5,096	EXIST. BASIN (PT. 4)
7	SCS Runoff	0.630	1	746	6,040		A		EW-5A
8	SCS Runoff	0.762	1	743	5,544	-			E-5B
9	Combine	1.385	1	745	11,584	7, 8	*****	: <del>====</del> :	E-5A + E-5B (PT. 5)
10	SCS Runoff	3.951	1	722	10,914	\ <del></del>		3 <b>0000</b> 00	EW-6 (PT. 6)
11	SCS Runoff	45.30	1	732	192,400		2		PW-1A
12	SCS Runoff	4.338	1	725	13,432		*****		PW-1B
13	Reservoir	0.842	1	748	3,749	12	127.41	5,189	WATER QUALITY SWALE
14	Combine	45.70	1	732	196,149	11, 13	42.202		TOTAL TO BASIN 2
15	Reservoir	34.19	1	742	167,881	14	121.92	40,295	BASIN 2
16	Diversion1	0.820	1	742	19,625	15	GE1115E		BASIN 2 INFILTRATION
17	Diversion2	33.37	1	742	148,255	15			BASIN 2 OUTFLOW (PT. 1)
18	SCS Runoff	0.499	1	755	3,761	*****			PW-2
19	Reservoir	0.000	1	774	0	18	118.36	1,341	BASIN 1 (PT.2)
20	SCS Runoff	1.274	1	748	10,882				PW-3
21	SCS Runoff	12.06	1	741	62,928		(MARTER)		PW-5A
22	Reservoir	7.915	1	757	38,755	21	129.25	17,002	BASIN 3
23	Combine	39.25	1	744	206,636	15, 19, 22			PROP. TOTAL TO RIVER (PT. 3)
24	SCS Runoff	0.993	1	727	3,424		*****	*****	PW-5B (PT. 5)
25	SCS Runoff	2.941	1	737	14,256	1.555575		*****	PW-6A
26	Reservoir	2.731	1	740	6,961	25	130.06	3,214	BASIN 4
27	SCS Runoff	0.009	1	881	248		*****	*****	PW-6B
28	Combine	2.731	1	740	7,210	26, 27	******	30000	TOTAL TO PT. 6
Hydro_SPR_REV.gpw					Return Period: 10 Year			Tuesday, Jun 3, 2008	

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#### Hyd. No. 11

PW-1A

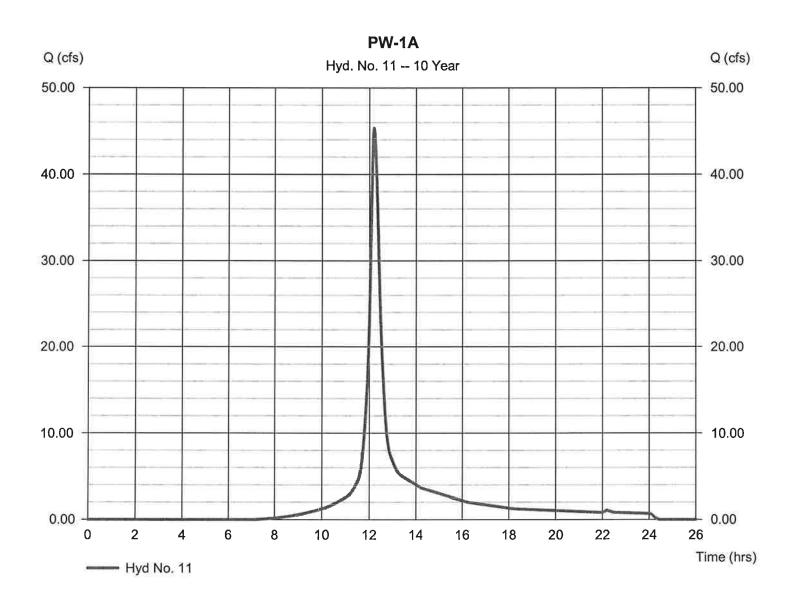
Hydrograph type = SCS Runoff Peak discharge = 45.30 cfsStorm frequency = 10 yrs Time to peak  $= 12.20 \, hrs$ Time interval Hyd. volume = 1 min = 192,400 cuftDrainage area = 19.670 acCurve number = 83\* Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) = 18.50 min

Tc method = TR55 Time of conc. (Tc) = 18.50 min

Total precip. = 4.50 in Distribution = Type III

Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(13.300 x 98) + (5.150 x 39)] / 19.670



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#### Hyd. No. 12

Storm duration

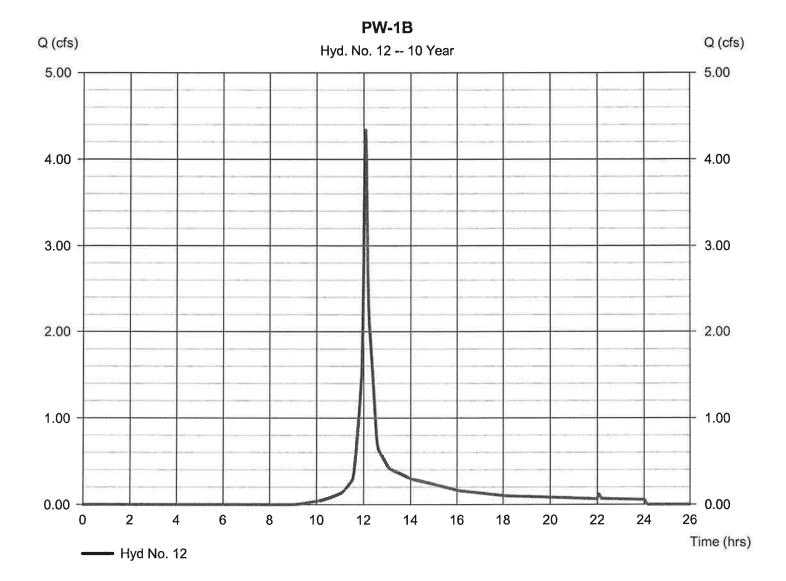
PW-1B

Hydrograph type = SCS Runoff
Storm frequency = 10 yrs
Time interval = 1 min
Drainage area = 1.750 ac
Basin Slope = 0.0 %
Tc method = USER
Total precip. = 4.50 in

= 24 hrs

Peak discharge = 4.338 cfs
Time to peak = 12.08 hrs
Hyd. volume = 13,432 cuft
Curve number = 75

Hydraulic length = 0 ft
Time of conc. (Tc) = 6.00 min
Distribution = Type III
Shape factor = 484



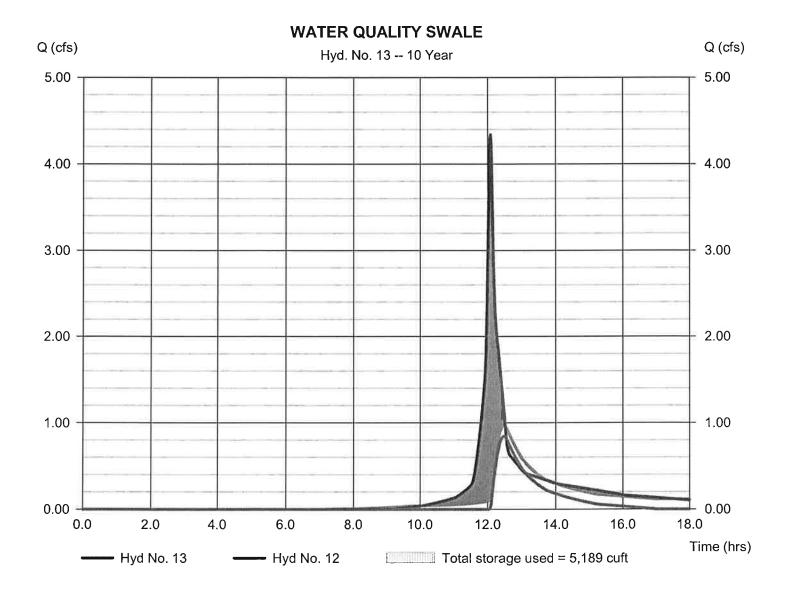
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#### Hyd. No. 13

#### WATER QUALITY SWALE

Hydrograph type Peak discharge = 0.842 cfs= Reservoir Storm frequency Time to peak  $= 12.47 \, hrs$ = 10 yrs Time interval Hyd. volume = 3,749 cuft= 1 min = 127.41 ftInflow hyd. No. Max. Elevation = 12 - PW-1B Reservoir name = WATER QUALITY SWALE Max. Storage = 5,189 cuft



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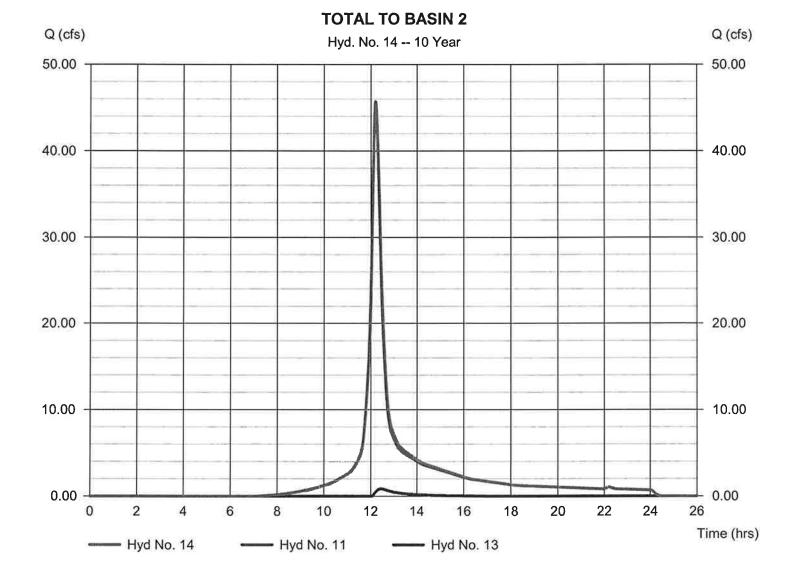
Tuesday, Jun 3, 2008

### Hyd. No. 14

#### **TOTAL TO BASIN 2**

Hydrograph type = Combine Storm frequency = 10 yrs Time interval = 1 min Inflow hyds. = 11, 13

Peak discharge = 45.70 cfs Time to peak = 12.20 hrs Hyd. volume = 196,149 cuft Contrib. drain. area = 19.670 ac



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= 34.19 cfs

 $= 12.37 \, hrs$ 

= 121.92 ft

= 167,881 cuft

= 40,295 cuft

#### Hyd. No. 15

#### BASIN 2

Hydrograph type = Reservoir Storm frequency = 10 yrs Time interval = 1 min

Inflow hyd. No. Reservoir name

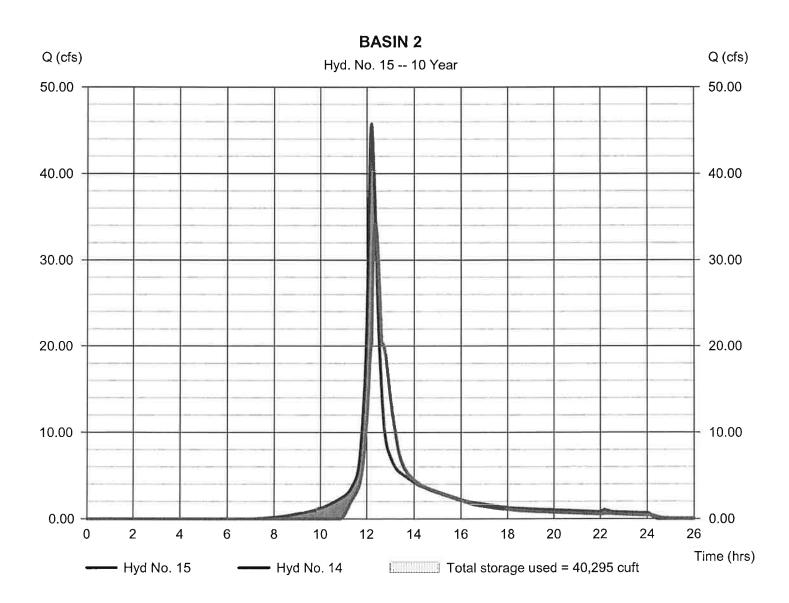
= 14 - TOTAL TO BASIN 2

Max. Elevation Max. Storage = BASIN 2

Peak discharge

Time to peak

Hyd. volume



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#### Hyd. No. 16

#### **BASIN 2 INFILTRATION**

Hydrograph type = Diversion1 Storm frequency = 10 yrsTime interval = 1 min

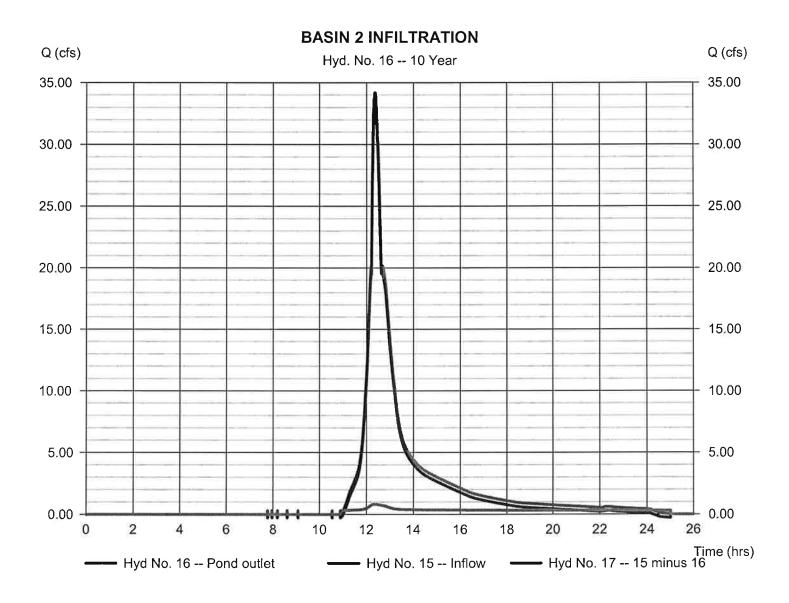
Inflow hydrograph = 15 - BASIN 2

Diversion method = Pond - BASIN 2

Peak discharge = 0.820 cfsTime to peak  $= 12.37 \, hrs$ Hyd. volume = 19,625 cuft

2nd diverted hyd. = 17

Pond structure = Exfiltration



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### Hyd. No. 17

BASIN 2 OUTFLOW (PT. 1)

Hydrograph type = Diversion2 Storm frequency = 10 yrs Time interval = 1 min

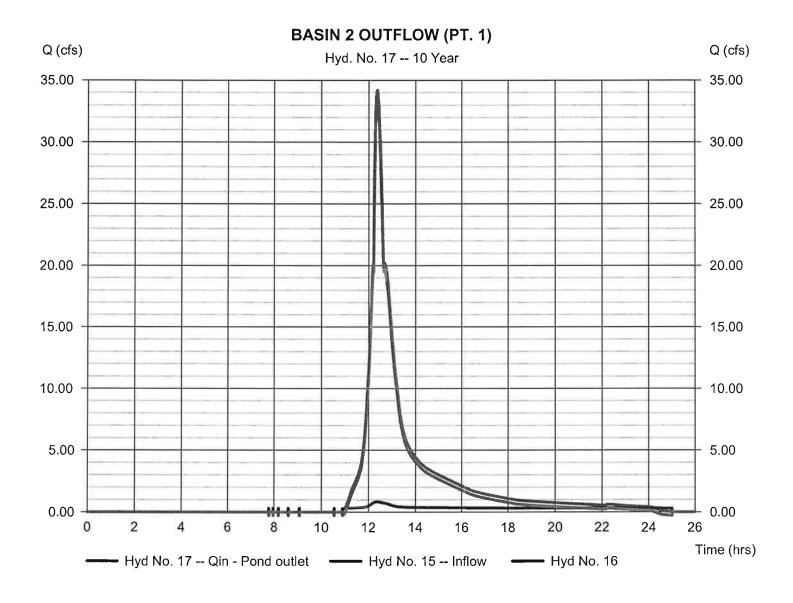
Inflow hydrograph = 15 - BASIN 2

Diversion method = Pond - BASIN 2

Peak discharge = 33.37 cfsTime to peak  $= 12.37 \, hrs$ Hyd. volume = 148,255 cuft

2nd diverted hyd. = 16

Pond structure = Exfiltration



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#### Hyd. No. 18

PW-2

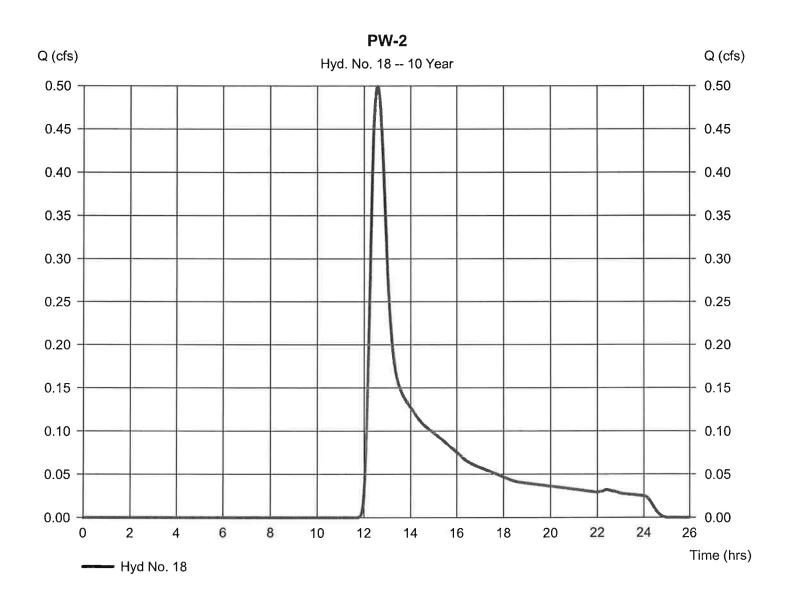
Hydrograph type= SCS RunoffPoStorm frequency= 10 yrsTiTime interval= 1 minHDrainage area= 1.310 acCBasin Slope= 0.0 %HTc method= TR55Ti

Total precip. = 4.50 in Storm duration = 24 hrs Peak discharge = 0.499 cfs Time to peak = 12.58 hrs Hyd. volume = 3,761 cuft

Curve number  $= 56^*$ Hydraulic length = 0 ft

Time of conc. (Tc) = 37.52 min
Distribution = Type III
Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(7.230 x 98) + (0.300 x 39)] / 1.310



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### Hyd. No. 19

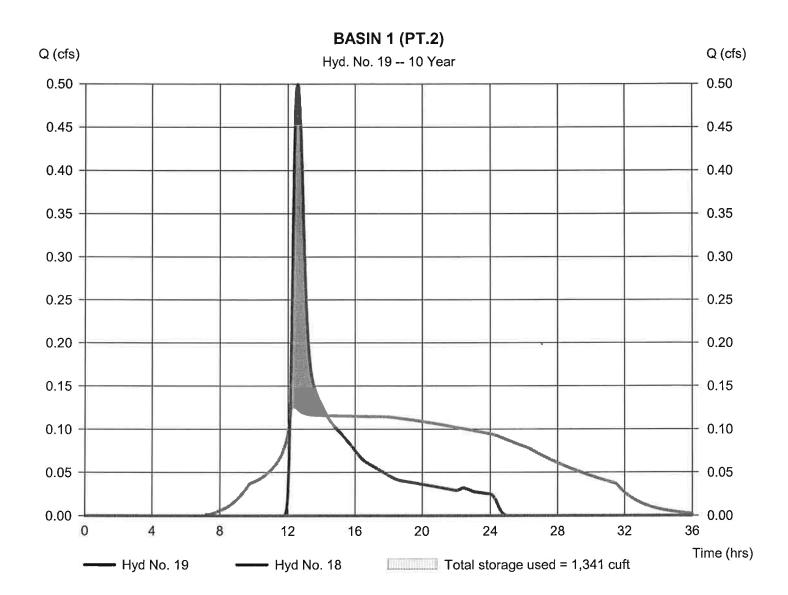
BASIN 1 (PT.2)

Hydrograph type = Reservoir Storm frequency = 10 yrs Time interval = 1 min Inflow hyd. No. = 18 - PW-2

Reservoir name = UPGRADED BASIN

Peak discharge = 0.000 cfs Time to peak = 12.90 hrs Hyd. volume = 0 cuft

Max. Elevation = 118.36 ft Max. Storage = 1,341 cuft



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#### Hyd. No. 20

PW-3

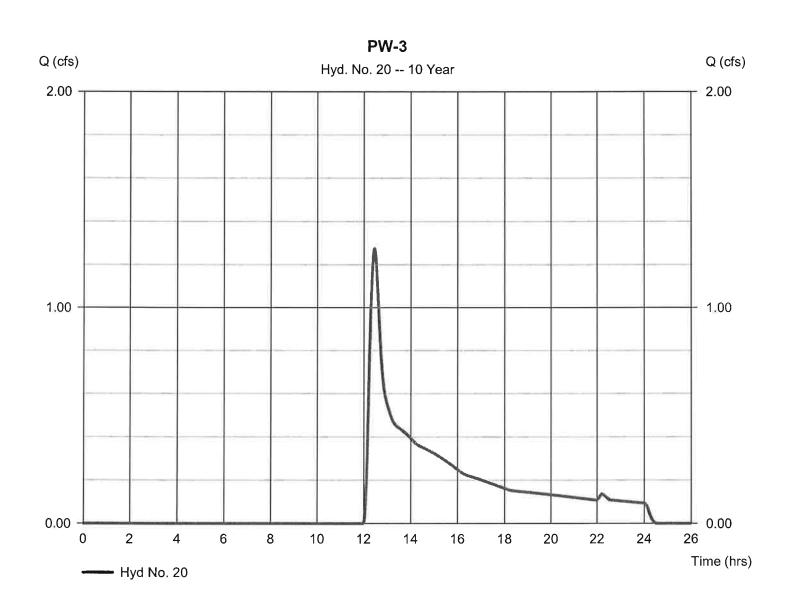
= SCS Runoff Hydrograph type Storm frequency = 10 yrsTime interval = 1 minDrainage area = 7.250 acBasin Slope = 0.0 %Tc method = TR55 Total precip. = 4.50 inStorm duration = 24 hrs

Peak discharge = 1.274 cfs Time to peak = 12.47 hrs Hyd. volume = 10,882 cuft

Curve number = 48\*Hydraulic length = 0 ft

Time of conc. (Tc) = 18.81 min
Distribution = Type III
Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(7.240 x 39)] / 7.250



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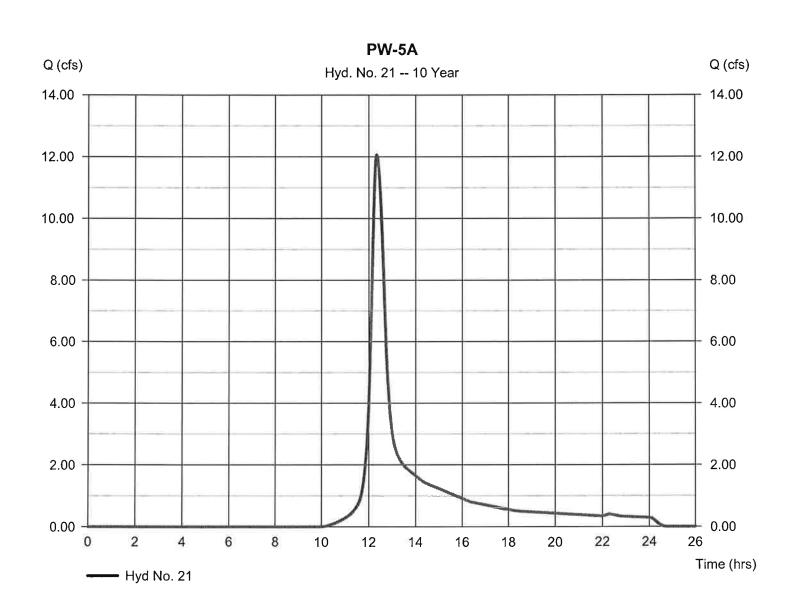
#### Hyd. No. 21

PW-5A

Hydrograph type = SCS Runoff Peak discharge = 12.06 cfsStorm frequency Time to peak  $= 12.35 \, hrs$ = 10 yrsTime interval = 1 min Hyd. volume = 62,928 cuft = 71\* Drainage area = 10.000 acCurve number Hydraulic length = 0 ftBasin Slope = 0.0 %

Tc method = TR55 Time of conc. (Tc) = 27.26 min
Total precip. = 4.50 in Distribution = Type III
Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(0.880 x 98) + (3.950 x 39)] / 10.000



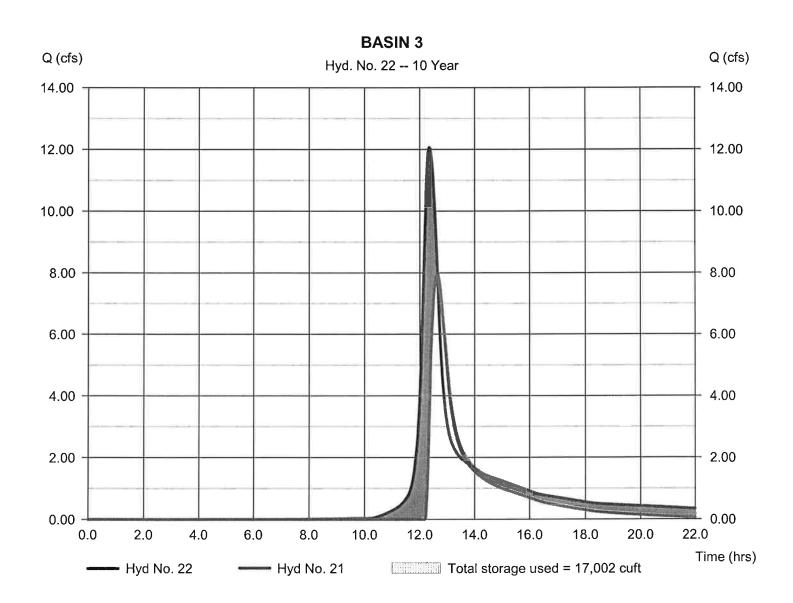
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#### Hyd. No. 22

BASIN 3

Hydrograph type Peak discharge = 7.915 cfs= Reservoir Time to peak Storm frequency  $= 12.62 \, hrs$ = 10 yrsHyd. volume Time interval = 38,755 cuft = 1 minMax. Elevation  $= 129.25 \, ft$ Inflow hyd. No. = 21 - PW-5A Reservoir name Max. Storage = 17,002 cuft= BASIN 3



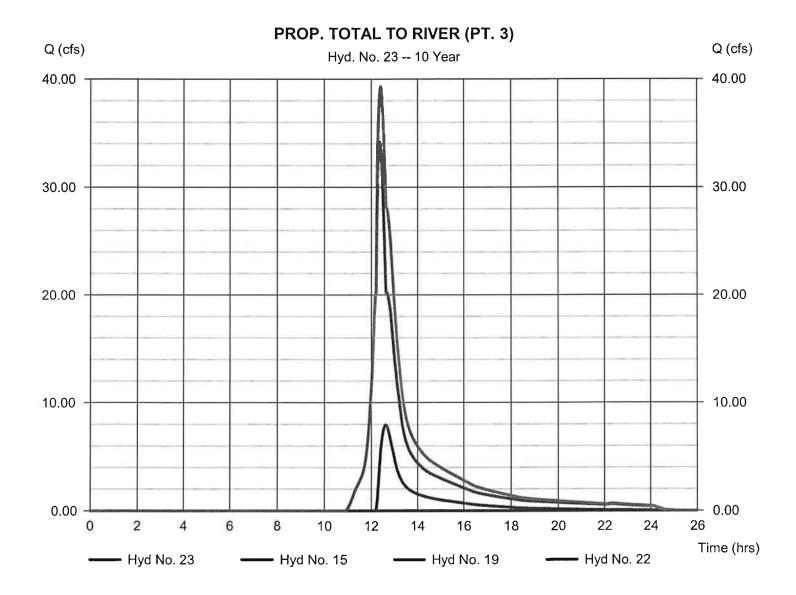
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#### Hyd. No. 23

PROP. TOTAL TO RIVER (PT. 3)

Hydrograph type = Combine Storm frequency = 10 yrs Time interval = 1 min Inflow hyds. = 15, 19, 22 Peak discharge = 39.25 cfs
Time to peak = 12.40 hrs
Hyd. volume = 206,636 cuft
Contrib. drain. area= 0.000 ac



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= Type III

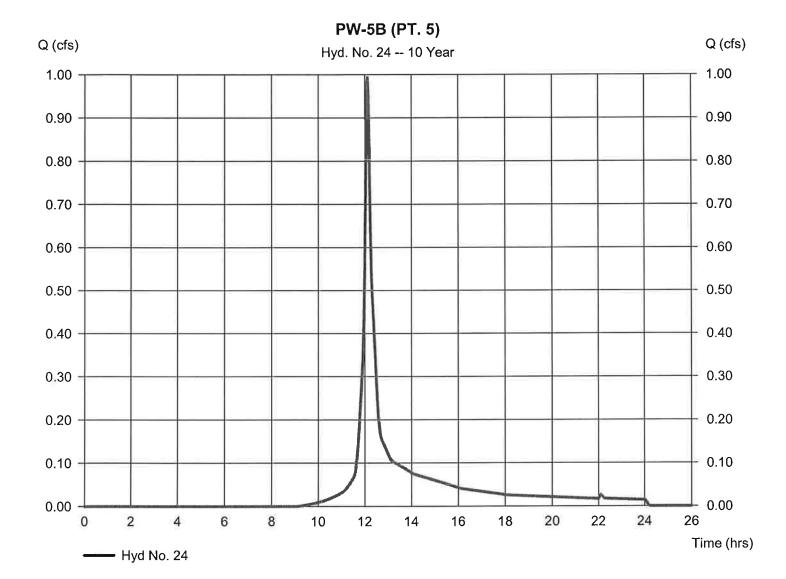
= 484

### Hyd. No. 24

PW-5B (PT. 5)

= SCS Runoff Peak discharge = 0.993 cfsHydrograph type Time to peak = 12.12 hrs Storm frequency = 10 yrsTime interval = 1 min Hyd. volume = 3,424 cuftDrainage area = 0.460 acCurve number = 75 = 0 ft

Hydraulic length Basin Slope = 0.0 % Tc method Time of conc. (Tc) = 10.01 min= TR55 Distribution Total precip. = 4.50 inStorm duration Shape factor = 24 hrs



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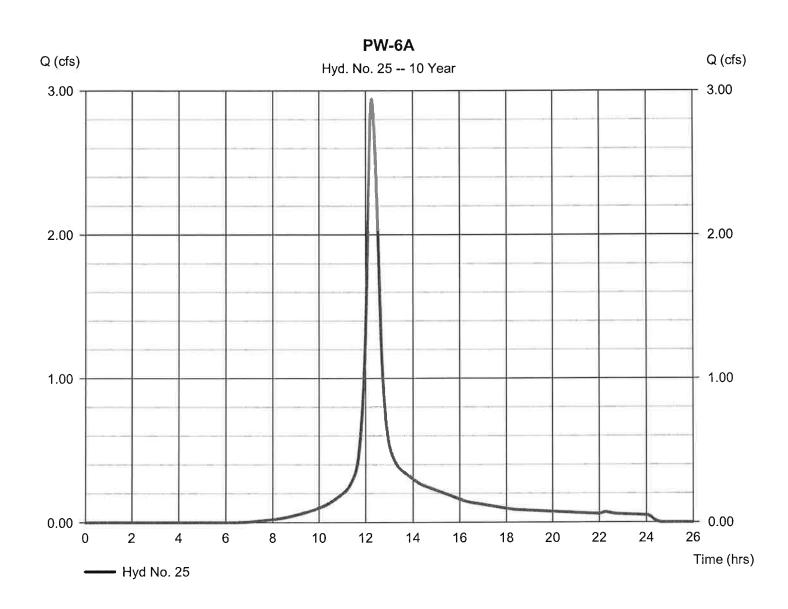
#### Hyd. No. 25

PW-6A

Hydrograph type= SCS RunoffPeak discharge= 2.941 cfsStorm frequency= 10 yrsTime to peak= 12.28 hrsTime interval= 1 minHyd. volume= 14,256 cuftDrainage area= 1.350 acCurve number= 85\*

Tc method = TR55 Time of conc. (Tc) = 24.74 min
Total precip. = 4.50 in Distribution = Type III
Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) =  $[(0.380 \times 39) + (0.650 \times 98)] / 1.350$ 



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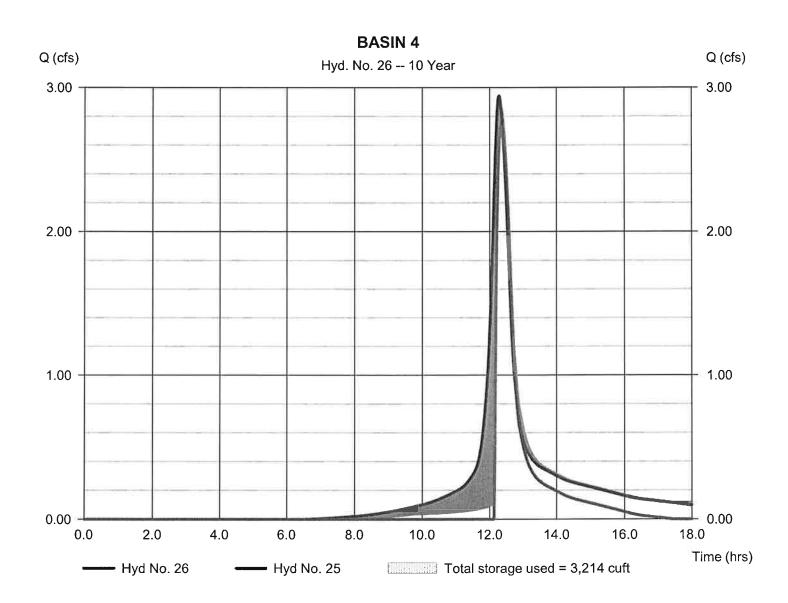
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#### Hyd. No. 26

BASIN 4

Hydrograph type = Reservoir
Storm frequency = 10 yrs
Time interval = 1 min
Inflow hyd. No. = 25 - PW-6A
Reservoir name = BASIN 4

Peak discharge = 2.731 cfs
Time to peak = 12.33 hrs
Hyd. volume = 6,961 cuft
Max. Elevation = 130.06 ft
Max. Storage = 3,214 cuft



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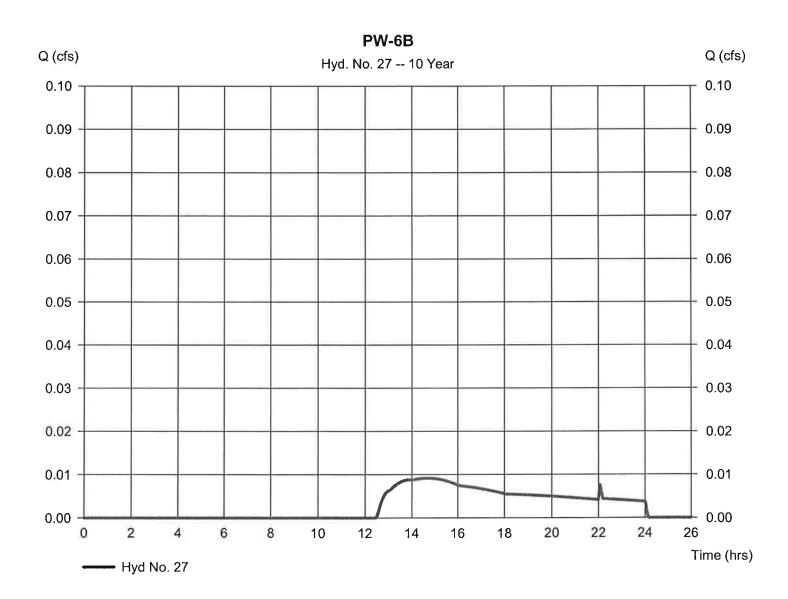
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#### Hyd. No. 27

PW-6B

Peak discharge = 0.009 cfsHydrograph type = SCS Runoff Storm frequency Time to peak  $= 14.68 \, hrs$ = 10 yrsTime interval = 1 min Hyd. volume = 248 cuft = 39\* Drainage area = 0.600 acCurve number Hydraulic length = 0 ftBasin Slope = 0.0 %Time of conc. (Tc) = 6.00 minTc method = USER Total precip. = 4.50 inDistribution = Type III = 484 Storm duration = 24 hrs Shape factor

<sup>\*</sup> Composite (Area/CN) = [(1.610 x 39)] / 0.600



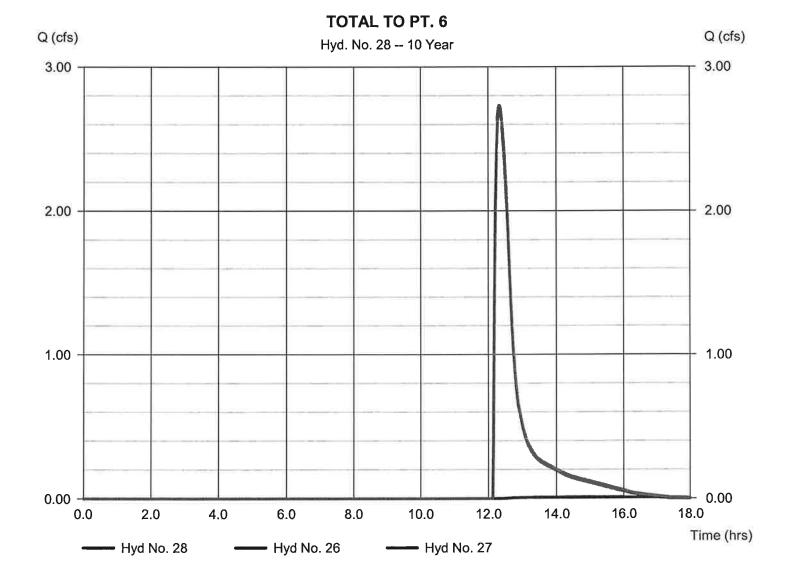
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### Hyd. No. 28

TOTAL TO PT. 6

Hydrograph type = Combine Storm frequency = 10 yrs Time interval = 1 min Inflow hyds. = 26, 27 Peak discharge = 2.731 cfs Time to peak = 12.33 hrs Hyd. volume = 7,210 cuft Contrib. drain. area= 0.600 ac



Hydrograph Summary Report
Hydrographs Extension for AutoCAD® Civil 3D® 2008 by Autodesk, Inc. v6.052

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	91.48	1	728	345,180			(aucure)	EW-1 (PT. 1)
2	SCS Runoff	23.83	1	725	79,704		*****		EW-2 (PT. 2)
3	SCS Runoff	13.92	1	746	83,057				EW-3
4	Combine	120.33	1	727	507,942	1, 2, 3	22302		EXIST. TOTAL TO RIVER (PT. 3)
5	SCS Runoff	6.070	1	729	22,821				EW-4
6	Reservoir	0.000	1	768	0	5	120.10	12,018	EXIST. BASIN (PT. 4)
7	SCS Runoff	4.778	1	733	23,917		1	-22-0-	EW-5A
8	SCS Runoff	3.796	1	735	18,482	*****		*****	E-5B
9	Combine	8.554	1	734	42,399	7, 8	THE REPORT OF THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TO THE PERSON NAM	(Abares	E-5A + E-5B (PT. 5)
10	SCS Runoff	10.68	1	721	27,323			213112	EW-6 (PT. 6)
11	SCS Runoff	82.29	1	732	354,916	*****	· · · · · · · · · · · · · · · · · · ·	) AND	PW-1A
12	SCS Runoff	8.803	1	725	27,183	Serence	HARRAS.		PW-1B
13	Reservoir	4.011	1	733	14,267	12	127.96	8,308	WATER QUALITY SWALE
14	Combine	86.29	1	732	369,183	11, 13			TOTAL TO BASIN 2
15	Reservoir	65.82	1	741	336,563	14	123.29	63,332	BASIN 2
16	Diversion1	1.025	1	741	23,696	15		4	BASIN 2 INFILTRATION
17	Diversion2	64.79	1	741	312,865	15	******	: *****	BASIN 2 OUTFLOW (PT. 1)
18	SCS Runoff	1.683	1	749	10,491			I <del>nterna</del> .	PW-2
19	Reservoir	0.035	1	815	215	18	119.08	4,292	BASIN 1 (PT.2)
20	SCS Runoff	7.448	1	737	39,243		*****	******	PW-3
21	SCS Runoff	26.40	1	740	134,167		<del></del>	eeeene.	PW-5A
22	Reservoir	17.27	1	757	106,346	21	130.69	31,280	BASIN 3
23	Combine	80.60	1	743	443,123	15, 19, 22	******	******	PROP. TOTAL TO RIVER (PT. 3)
24	SCS Runoff	2.021	1	727	6,929			I <del>stanto</del> .	PW-5B (PT. 5)
25	SCS Runoff	5.210	1	736	25,740		•	1	PW-6A
26	Reservoir	5.006	1	739	16,969	25	130.19	3,527	BASIN 4
27	SCS Runoff	0.275	1	728	1,726	S	*******	( <del>1)122-14</del>	PW-6B
28	Combine	5.237	1	739	18,695	26, 27			TOTAL TO PT. 6
Hydro_SPR_REV.gpw				Return Period: 100 Year			Tuesday, Jun 3, 2008		

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= 484

Shape factor

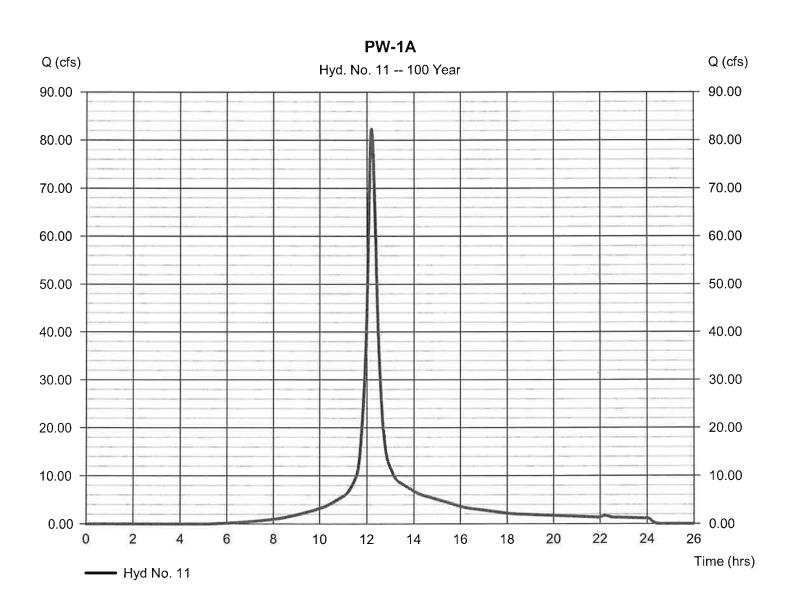
#### Hyd. No. 11

Storm duration

PW-1A

= SCS Runoff Peak discharge = 82.29 cfsHydrograph type Storm frequency = 100 yrs Time to peak = 12.20 hrsTime interval Hyd. volume = 354,916 cuft = 1 minCurve number = 83\* Drainage area = 19.670 acHydraulic length = 0 ftBasin Slope = 0.0 % Time of conc. (Tc) = 18.50 minTc method = TR55 Total precip. = 7.00 inDistribution = Type III

= 24 hrs



<sup>\*</sup> Composite (Area/CN) = [(13.300 x 98) + (5.150 x 39)] / 19.670

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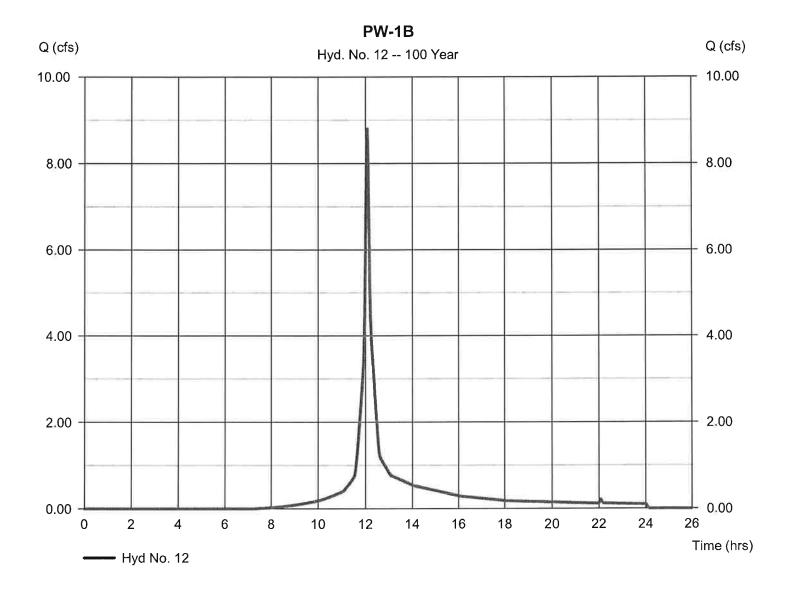
### Hyd. No. 12

PW-1B

= SCS Runoff Hydrograph type Storm frequency = 100 yrsTime interval = 1 min Drainage area = 1.750 acBasin Slope = 0.0 %Tc method = USER Total precip. = 7.00 inStorm duration = 24 hrs

Peak discharge = 8.803 cfs
Time to peak = 12.08 hrs
Hyd. volume = 27,183 cuft
Curve number = 75
Hydraulic length = 0 ft
Time of conc. (Tc) = 6.00 min

Distribution = Type III Shape factor = 484



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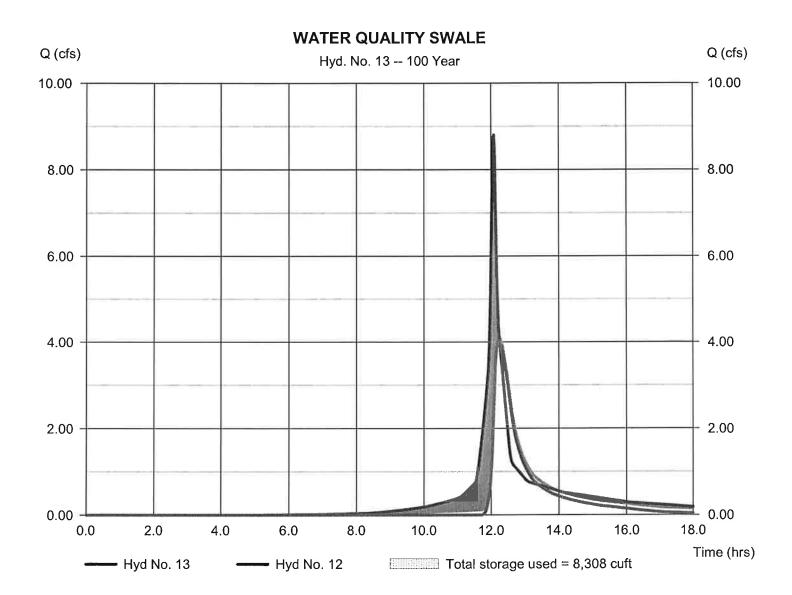
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### Hyd. No. 13

### WATER QUALITY SWALE

Hydrograph type Peak discharge = 4.011 cfs= Reservoir Storm frequency = 100 yrsTime to peak = 12.22 hrs Time interval Hyd. volume = 14,267 cuft = 1 min Inflow hyd. No. = 12 - PW-1B Max. Elevation = 127.96 ftReservoir name Max. Storage **= WATER QUALITY SWALE** = 8,308 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



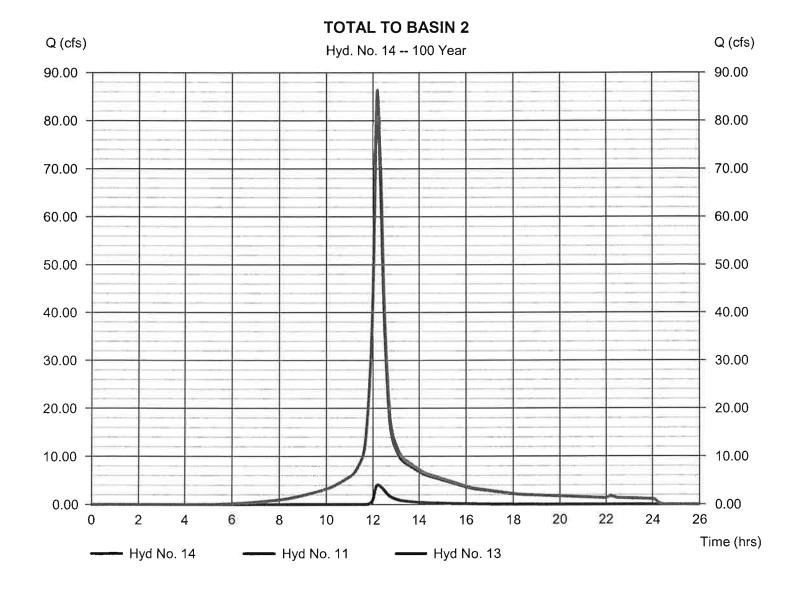
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### Hyd. No. 14

**TOTAL TO BASIN 2** 

Hydrograph type = Combine Storm frequency = 100 yrs Time interval = 1 min Inflow hyds. = 11, 13 Peak discharge = 86.29 cfs
Time to peak = 12.20 hrs
Hyd. volume = 369,183 cuft
Contrib. drain. area= 19.670 ac



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### Hyd. No. 15

### **BASIN 2**

Hydrograph type = Reservoir Storm frequency = 100 yrs Time interval = 1 min

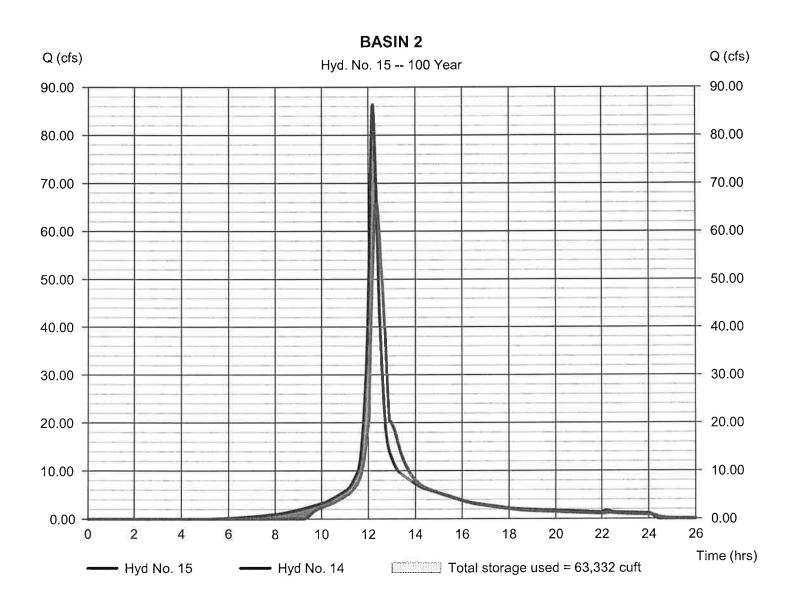
Inflow hyd. No. = 14 - TOTAL TO BASIN 2

Reservoir name = BASIN 2

Peak discharge = 65.82 cfs
Time to peak = 12.35 hrs
Hyd. volume = 336,563 cuft
Max. Elevation = 123.29 ft

Max. Storage = 63,332 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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### Hyd. No. 16

### **BASIN 2 INFILTRATION**

Hydrograph type = Diversion1 Storm frequency = 100 yrsTime interval = 1 min

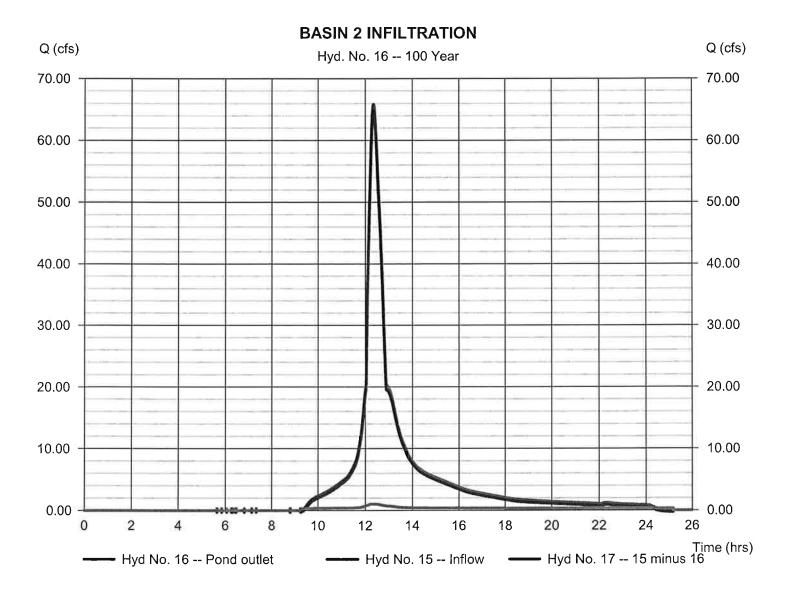
Inflow hydrograph = 15 - BASIN 2

Diversion method = Pond - BASIN 2

Peak discharge = 1.025 cfsTime to peak  $= 12.35 \, hrs$ Hyd. volume = 23,696 cuft

2nd diverted hyd. = 17

= Exfiltration Pond structure



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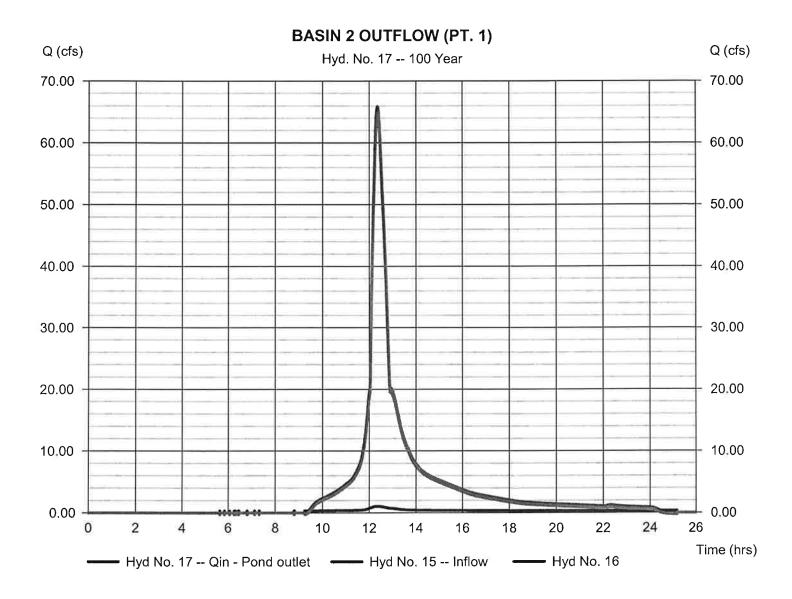
### Hyd. No. 17

BASIN 2 OUTFLOW (PT. 1)

Hydrograph type= Diversion2Peak discharge= 64.79 cfsStorm frequency= 100 yrsTime to peak= 12.35 hrsTime interval= 1 minHyd. volume= 312,865 cuft

Inflow hydrograph = 15 - BASIN 2 2nd diverted hyd. = 16

Diversion method = Pond - BASIN 2 Pond structure = Exfiltration



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### Hyd. No. 18

Storm duration

PW-2

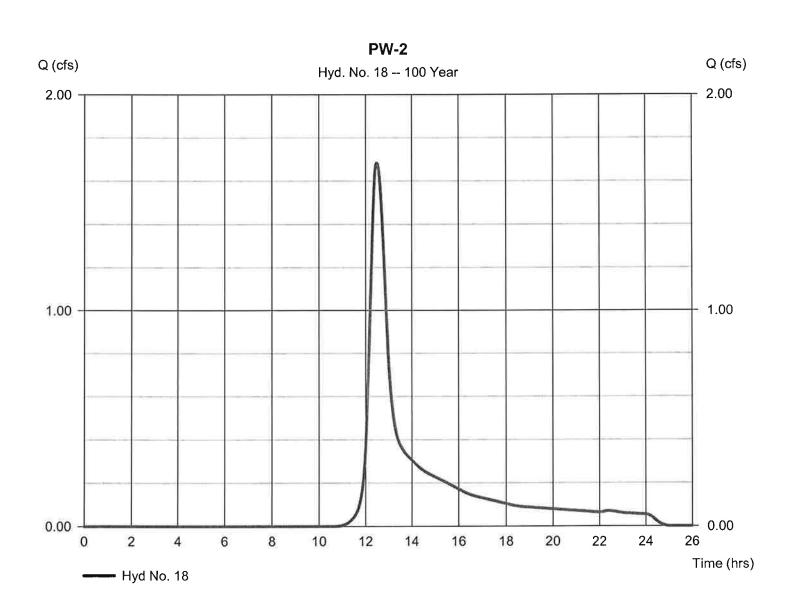
Hydrograph type = SCS Runoff
Storm frequency = 100 yrs
Time interval = 1 min
Drainage area = 1.310 ac
Basin Slope = 0.0 %
Tc method = TR55
Total precip. = 7.00 in

Peak discharge = 1.683 cfs
Time to peak = 12.48 hrs
Hyd. volume = 10,491 cuft

Curve number  $= 56^*$ Hydraulic length = 0 ft

Time of conc. (Tc) = 37.52 min
Distribution = Type III
Shape factor = 484

= 24 hrs



<sup>\*</sup> Composite (Area/CN) =  $[(7.230 \times 98) + (0.300 \times 39)] / 1.310$ 

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= 0.035 cfs

 $= 13.58 \, hrs$ 

= 215 cuft

= 119.08 ft

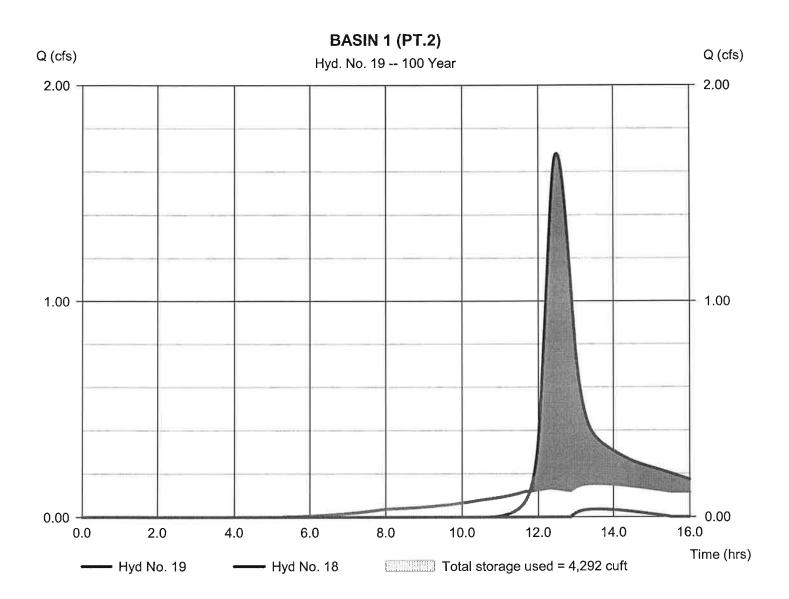
= 4,292 cuft

### Hyd. No. 19

BASIN 1 (PT.2)

Hydrograph type= ReservoirPeak dischargeStorm frequency= 100 yrsTime to peakTime interval= 1 minHyd. volumeInflow hyd. No.= 18 - PW-2Max. ElevationReservoir name= UPGRADED BASINMax. Storage

Storage Indication method used. Exfiltration extracted from Outflow.



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### Hyd. No. 20

PW-3

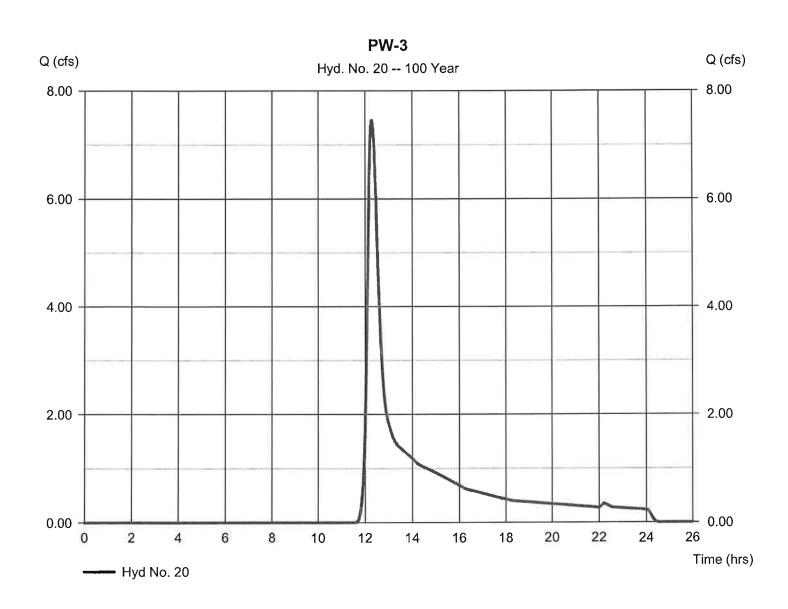
= SCS Runoff Hydrograph type Storm frequency = 100 yrsTime interval = 1 min Drainage area = 7.250 acBasin Slope = 0.0 % Tc method = TR55 Total precip. = 7.00 inStorm duration = 24 hrs

Peak discharge = 7.448 cfs
Time to peak = 12.28 hrs
Hyd. volume = 39,243 cuft

Curve number  $= 48^*$ Hydraulic length = 0 ft

Time of conc. (Tc) = 18.81 min
Distribution = Type III
Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(7.240 x 39)] / 7.250



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### Hyd. No. 21

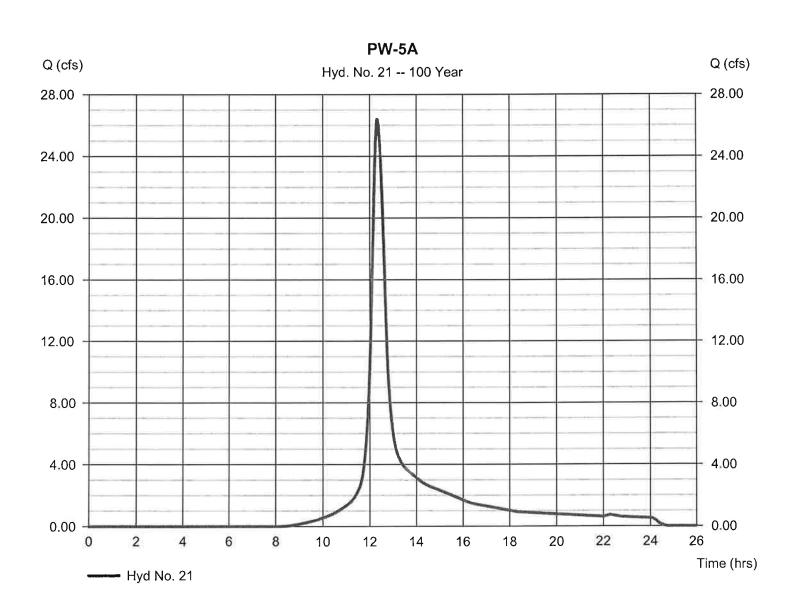
PW-5A

= 26.40 cfs= SCS Runoff Peak discharge Hydrograph type Storm frequency = 100 yrs Time to peak  $= 12.33 \, hrs$ Hyd. volume = 134,167 cuft Time interval = 1 min Curve number = 71\* Drainage area = 10.000 ac= 0 ft

Basin Slope = 0.0 % Hydraulic length = 0 ft
Tc method = TR55 Time of conc. (Tc) = 27.26 min
Total precip. = 7.00 in Distribution = Type III

Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(0.880 x 98) + (3.950 x 39)] / 10.000



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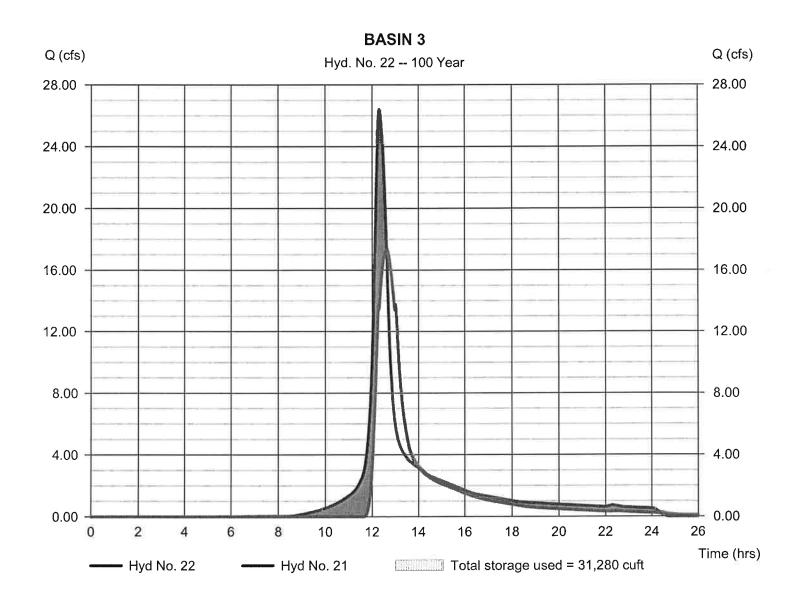
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### Hyd. No. 22

BASIN 3

Peak discharge = 17.27 cfsHydrograph type = Reservoir Time to peak Storm frequency = 100 yrs $= 12.62 \, hrs$ Time interval Hyd. volume = 106,346 cuft = 1 min Inflow hyd. No. = 21 - PW-5A Max. Elevation = 130.69 ftMax. Storage = 31,280 cuft Reservoir name = BASIN 3

Storage Indication method used. Exfiltration extracted from Outflow.



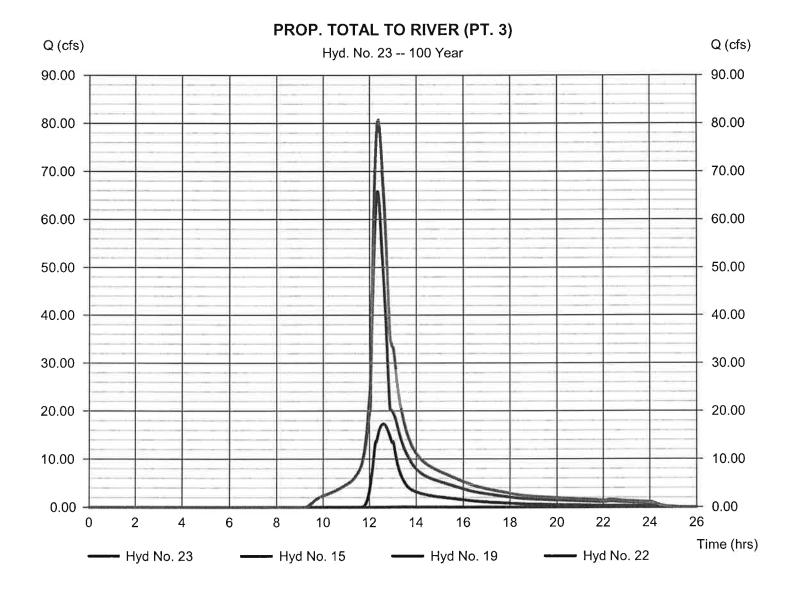
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### Hyd. No. 23

PROP. TOTAL TO RIVER (PT. 3)

Hydrograph type = Combine Storm frequency = 100 yrs Time interval = 1 min Inflow hyds. = 15, 19, 22 Peak discharge = 80.60 cfs Time to peak = 12.38 hrs Hyd. volume = 443,123 cuft Contrib. drain. area= 0.000 ac



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= 24 hrs

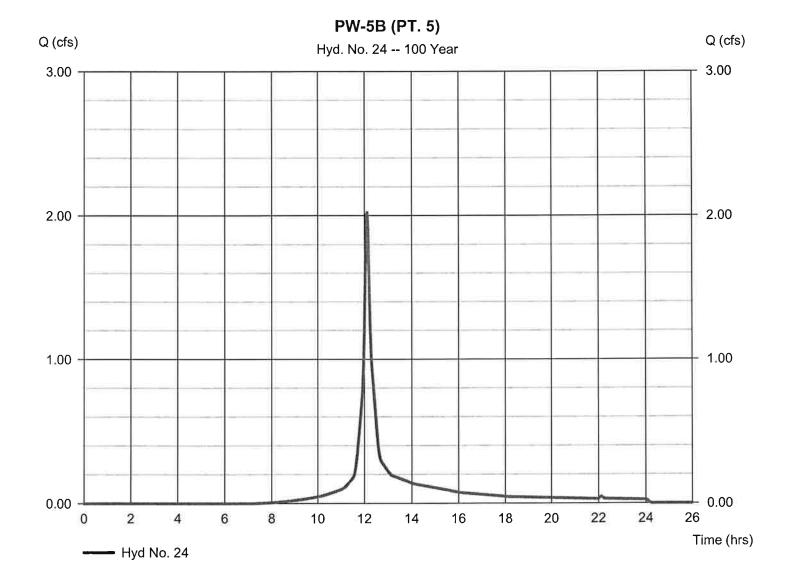
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### Hyd. No. 24

PW-5B (PT. 5)

Hydrograph type = SCS Runoff Peak discharge = 2.021 cfsTime to peak = 12.12 hrsStorm frequency = 100 yrsTime interval Hyd. volume = 6,929 cuft= 1 min Drainage area = 0.460 acCurve number = 75 Basin Slope Hydraulic length = 0 ft= 0.0 %

Tc method Time of conc. (Tc) = 10.01 min= TR55 Total precip. = Type III Distribution = 7.00 in= 484 Storm duration Shape factor



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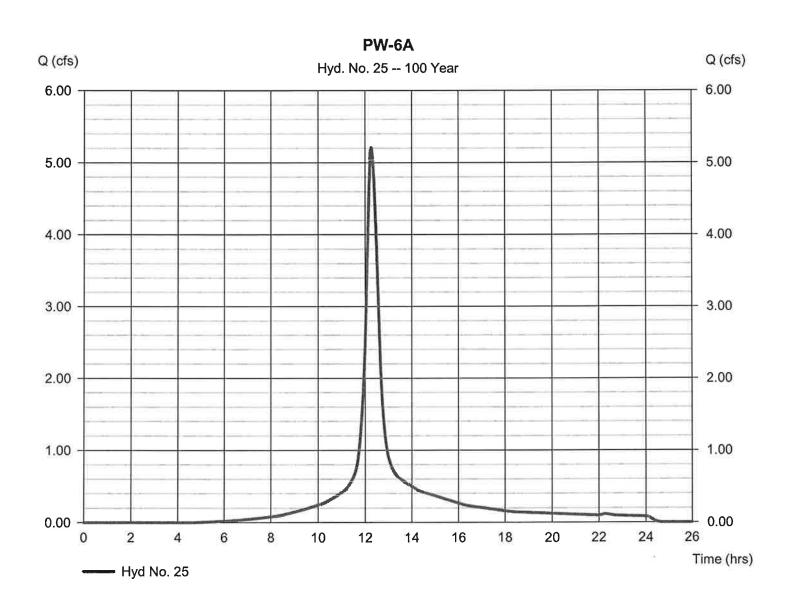
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### Hyd. No. 25

PW-6A

= SCS Runoff Peak discharge = 5.210 cfsHydrograph type Time to peak  $= 12.27 \, hrs$ Storm frequency = 100 yrs = 25,740 cuftTime interval = 1 min Hyd. volume Drainage area = 1.350 acCurve number = 85\* Basin Slope Hydraulic length = 0 ft= 0.0 %Tc method = TR55 Time of conc. (Tc) = 24.74 minTotal precip. = Type III Distribution = 7.00 inStorm duration = 484 Shape factor = 24 hrs

<sup>\*</sup> Composite (Area/CN) = [(0.380 x 39) + (0.650 x 98)] / 1.350



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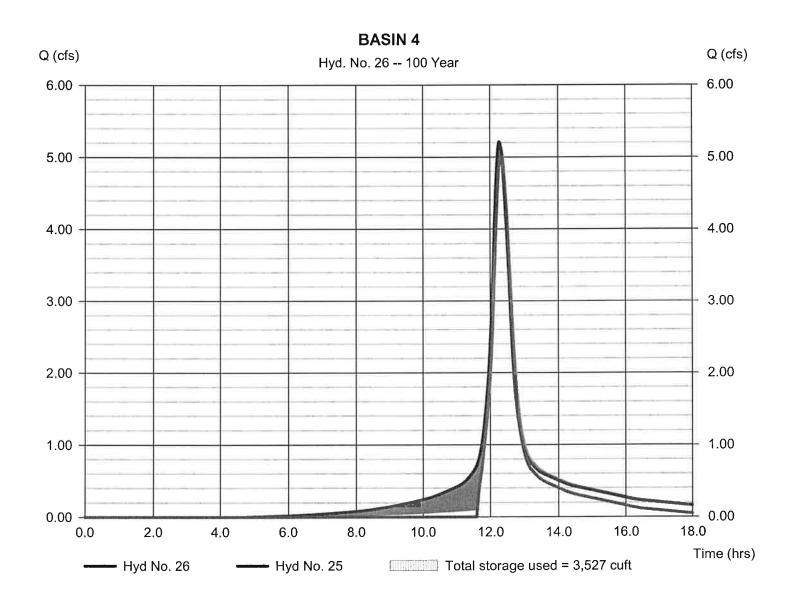
### Hyd. No. 26

**BASIN 4** 

Hydrograph type = Reservoir
Storm frequency = 100 yrs
Time interval = 1 min
Inflow hyd. No. = 25 - PW-6A
Reservoir name = BASIN 4

Peak discharge = 5.006 cfs
Time to peak = 12.32 hrs
Hyd. volume = 16,969 cuft
Max. Elevation = 130.19 ft
Max. Storage = 3,527 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



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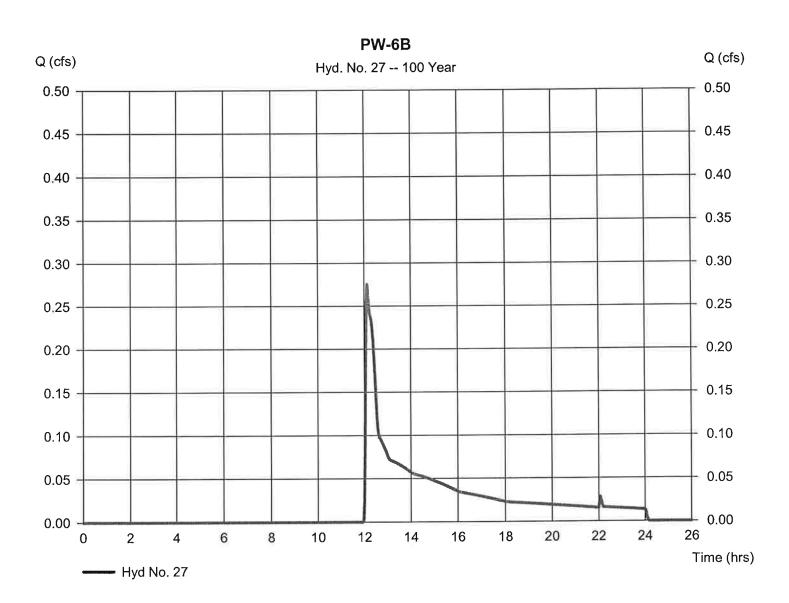
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### Hyd. No. 27

PW-6B

= 0.275 cfsPeak discharge Hydrograph type = SCS Runoff = 12.13 hrs Time to peak = 100 yrsStorm frequency = 1.726 cuft Hyd. volume Time interval = 1 min = 39\*Curve number = 0.600 acDrainage area Hydraulic length = 0 ftBasin Slope = 0.0 % Time of conc. (Tc) = 6.00 minTc method = USER Distribution = Type III Total precip. = 7.00 in= 484 Shape factor Storm duration = 24 hrs

<sup>\*</sup> Composite (Area/CN) = [(1.610 x 39)] / 0.600



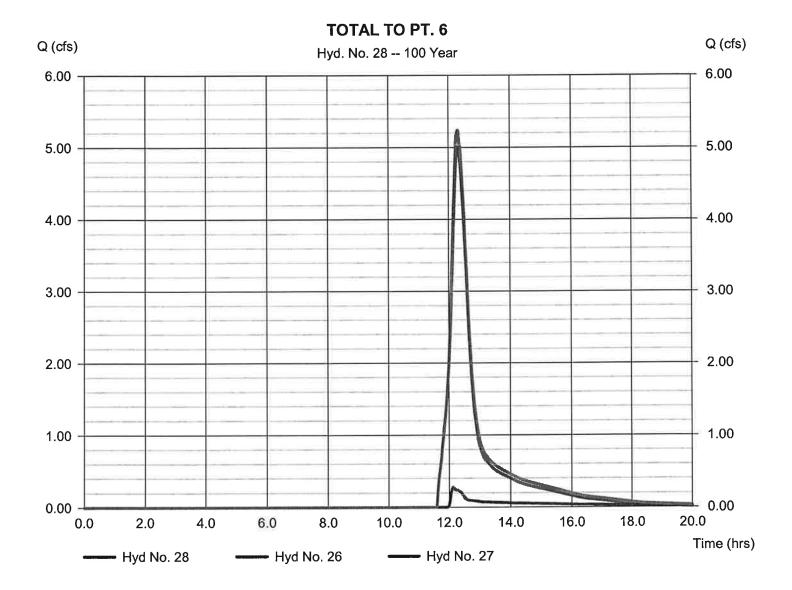
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### Hyd. No. 28

TOTAL TO PT. 6

Hydrograph type = Combine Storm frequency = 100 yrs Time interval = 1 min Inflow hyds. = 26, 27 Peak discharge = 5.237 cfs
Time to peak = 12.32 hrs
Hyd. volume = 18,695 cuft
Contrib. drain. area= 0.600 ac



### **APPENDIX D: HYDRAULIC CALCULATIONS**

																							_			4
HGL	(£)	122.21	123.08	123.42	124.31	123.80	124.29	124.31	123.08	126.21	127.59	123.08	126.21	125.14	125.81	126.28	125.14	125.81	126.28	125.64	126.95	127.92	128.69			
Gnd/Rim El Dn	(#)	121.50	127.15	128.30	125,30	127.15	128.30	125.30	127,15	127.25	130.50	127.15	127.25	131.05	129.20	127.10	131.05	129.20	127.10	130.00	131.20	132.60	132.10			
다 아	(£)	123.08	123.32	124.20	124.52	124.30	125.13	124.33	125.53	127.52	128.05	124.38	126.34	125.59	126.13	126.35	125.64	125.85	126.29	126.85	127.69	128.43	130.25		5-27-2008	
3nd/Rim El Up	(ft)	127.15	128.30	125.30	125.70	127.00	128.25	125.60	127.25	130.50	130.50	131.05	127.00	129.20	127.10	127.05	130.00	128.90	127.05	131.20	132.60	132.10	133.20		Date: 0	
Invert	(ft)	120.00	120.50	121.25	122.70	123.50	124.00	122.70	120.50	122.75	126.55	120.50	122.75	121.60	122.25	122.95	121.60	124.50	122.95	124.10	125.05	125.85	126.20			
Invert	(ft)	121.00	121.25	122.70	123.20	123.75	124.25	122,80	122.75	126.55	127.50	121.60	123.00	122.25	122.95	123.35	124.10	124.90	123.05	125.05	125.85	126.20	127.40		12	
Line Slope	(%)	0.51	0.48	0.49	0.54	1.97	3.47	1.21	1.81	1.49	0.50	0.50	1,47	0.50	0.50	0.91	2.56	1.12	96.0	1.12	0.51	0.48	0.52		f lines: 1	
Line Size	(in)	36	18	15	12	12	12	12	12	12	12	30	12	18	18	12	24	12	12	12	15	12	12		umber of	
Vel	(ft/s)	7.86	2.54	2.91	2.34	3.92	4.42	2.34	6.90	3.69	2.70	7.00	4.22	3.81	3.09	1.89	6.62	1.81	1.39	5.88	3.90	4.12	4.05		Ž	
Capac Full	(cfs)	51.62	7.85	4.88	2.84	5.42	7.18	4.24	5.18	4.71	2.72	31.56	4.68	8.06	8.04	3.68	39.20	4.09	3.77	4.09	4.98	2.66	2.79			
Flow Rate	(cfs)	42.41	4.49	3.57	1.84	1.09	1.35	1.84	5.42	2.88	1.53	34.34	3.31	6.74	5.46	1.49	18.79	1.41	1.09	4.62	4.79	3.23	3.18			
T <sub>C</sub>	(min)	23.8	2.6	5.6	5.0	2.0	5.0	5.0	15.1	6.3	5.0	22.3	15.0	21.5	20.5	5.0	20.2	5.0	5.0	<u> </u>	10.1	9.6	8.0			
Inlet	(min)	0.0	0.0	0.0	2.0	5.0	5.0	5.0	0.0	5.0	5.0	0.0	15.0	0.0	0.0	5.0	5.0	5.0	5.0	0.0	5.0	5.0	5.0			
Total CxA		12.16	0.80	0.58	0.29	0.17	0.22	0.29	1.25	0.49	0.24	9.53	92.0	1,83	1.45	0.24	4.96	0.22	0.17	0.94	0.94	0.62	0.58			
Incr		00.00	00.00	00.00	0.29	0.17	0,22	0,29	00.00	0.24	0.24	00.00	92.0	00.00	00.00	0.24	0.09	0.22	0.17	00.00	0.32	0.05	0.14			
Runoff Coeff	(C)	00.00	00.00	00.00	0.86	0.58	0.86	0.86	00.00	06.0	06'0	00.00	0.50	0.00	00.00	0.55	06.0	0.56	0.56	0.00	06:0	0.90	06.0			
Total Area	(ac)	16.59	0.93	0.68	0.34	0.30	0.25	0.34	2.06	0.54	0.27	12.84	1.52	2.83	2.23	0.43	6.20	0.40	0.31	1.04	1.04	0.69	0.64			
Drng Area	(ac)	00.00	00.00	00.00	0.34	0:30	0.25	0.34	00.00	0.27	0.27	00.00	1.52	00.00	00.00	0.43	0.10	0.40	0.31	00.0	0.35	0.05	0.16			
Line Length	(#)	195.900	157.480	298.520	92.140	12.690	7.210	8.280	124.580	254.990	190.960	218.000	16.960	129.520	140.160	44.000	97.680	35.580	10.470	84.710	158.000	73.640	230.000			
DnStm Ln No		Outfall	_	7	က	-	2	က	_	00	თ	-	80	Ξ	13	14	Ξ	13	4	16	19	20	21		and TC.str	
Line		DMH-12	DMH-25	DMH-23	CB-28	CB-27	CB-30	CB-29	DMH-28	DMH-27	DMH-26	DMH-11	CB-31	DMH-22	DMH-21	CB-23	DMH-20	CB-25	CB-24	DMH-19	DMH-18	DMH-17	DMH-16		t File: Wayla	
Line No.		+	7	က	4	5	9	7	00	6	10	7	12	13	4	15	16	17	18	19	28	2	52		Project	
	Line DnStm Line Drng Total Runoff Incr Total Inlet Tc Flow Capac Vel Line Line Invert Invert Gnd/Rim HGL Gnd/Rim HGL Gnd/Rim HGL Gnd/Rim ID Ln No Length Area Coeff CxA Time Rate Full Ave Size Slope Up Dn El Up Up El Dn	Line DnStm Line Drng Total Runoff Incr Total Inlet Tc Flow Capac Vel Line Line Invert Invert Gnd/Rim HGL Gnd/Rim H	Line DnStm Line and Area Area Coeff CxA CxA Time In (#1) (cfs) (cf	Line         DnStm         Line         Total         Total         Total         Inlet         Total         Inlet         Total         Inlet         Total         Inlet         Full         Ave         Size         Line         Line         Invert         Invert         Gnd/Rim         HGL         Gnd/Rim           ID         Ln No         Length         Area         Coeff         CxA         Time         Time         Full         Ave         Size         Slope         Up         Dn         HGL         BID         Up         BID         Up         BID         Up         BID         Time         <	Line         DnStm         Line         Drag Area         Coeff Coe	Line         DnStm         Line         Area         Coeff         CxA         Tine         Tine         Full         Ave         Size         Slope         Up         Invert         Invert         Gnd/Rim         HGL         Gnd/Rim           IDM+12         Ln No         Length         Area         Coeff         CxA         Tine         Tine	Line         DnStm         Line         Drug         Area         Coeff         CxA         Tine         Tine         Full         Ave         Size         Line         Line         Invert         Invert	Line         DnStm         Line         Area         Coeff         CxA         Time         Flow         Size         Slope         Invert         Invert         Gnd/Rim         HGL         Gnd/Rim           LDAH-12         Ln No         Length         Area         Coeff         CxA         Time         (Time)         (Time)	Line         DnStm         Line         Total         Inle         Total         Inle         Total         Inle         Total         Inle         Full         Ave         Size         Line         Size         Size         Size         Invert         Invert	Line   DnSth   Line   Area   Area   Area   Coeff   CxA   CxA   Time   Trine   Trine   Trine   Trine   Full   Area   Size   Siope   Up   Dn   Trine   Trine	Line   DnStm   Line   Line   Area   Coeff   CxA   Time   Trotal   Inlet   Inlet   Trotal   Inlet   Inlet	Line   Doctor   Line   Line   Court   Court	Line   DiStri	Link   District   Link   Area   Area   Area   Area   Coeff   Coef   Coeff   Coef   Time   T	Link   Link   Link   Area   Coeff CxA   CxA   Time   Total   Inite   Total   Inite   Total   Link   Full   Ave   Full   Ave   Size   Size   Inite   Link   Link   Total   Inite   Total   Link   Full   Ave   Size   Size	Line   Diright   Line   Line	Line   Line	Harmonian   Line   Line   Area   Area   Coad   Coad   Time   Time   Time   Flow   Fl	UHH         CHOR         LINE         CHOR         CHOR	Line   Line   Line   Line   Area   Coart   C	Harmonian   Harm	Line   Diskin   Line   Aria   Aria   Aria   Ruard   Cad   Cad   Cad   Cad   Time   T	Line   Dishi   Line   Dishi   Line   Dishi   Line   Line	Link   Link	Links   Diesis   Links   Aria   Aria   Coord   Coord   Coord   Time   Coord   Coord   Coord   Time   Coord   Coord   Coord   Time   Coord   Coord   Coord   Time   Coord   Coord   Time   Coord   Coord   Time   Coord   Coord   Time   Ti	Line         Discrite         Line         Area         Area         Chan         Chan

Hydraflow Storm Sewers Extension

	Rim HGL On Dn	(ft)	20 130.51	90 131.17	60 131.67	05 125,14	20 125.81	125.64	05 126.28	00 126.77	80 126.93	00 128.20	80 127.86	50 128.51	20 129.27	00 126.80	05 127.26	00 126.77	80 126.93	.00 127.86	.80 127.86	50 128.34	20 129.27	50 129.53	
	HGL Gnd/Rim Up El Dn	(ft) (ft)	131.02 133.20	131.66 133.90	131.74   134.60	126.28 j   131.05	125.83   129.20	126.25   130.00	126,93 j   131.05	127.86 j   130.00	127.35   131.80	129.98   132.00	127.95   131.80	129.27   133.50	129.59   132.20	127.85   130.00	128.88   131.05	126.94   130.00	127.72 J 131.80	128.87   132.00	127.79 131.80	129.49 j 133.50	129.22 j   132.20	130.43 134.50	0000
	Gnd/Rim H El Up	£)	133.90 13	134.60 13	134.55 13	131.05   126	128.80   12	130.00 126	131.80   126	132.00   127	131.80   12	131.00   12	133.50   12	132.20 12	132.20 129	129.90	131.00 12	129.50 12	131.30   127	131.00   12	131.30   12	134.50 129	132.20   129	134.60 13	
	Invert G Dn	(£	127.40	128.05	128.95	121.60	124.00	124.10	125.00	124.90	125.70	126.70	126.15	128.00	128.70	126.50	127.00	125.00	126.50	127.50	127.00	127.20	128.70	128.40	
	Invert Up	(#)	128.05	128.95	130.55	125.00	124.80	124.90	125.70	126.70	126.15	128.00	126.70	128.70	129.20	126.90	127.50	125.50	127.30	128.00	127.30	128.40	128.80	129.30	
	Line Slope	(%)	0.52	0.50	1.07	2.63	3,12	0.51	0.52	0.50	0.51	0.49	0.50	0.80	95.0	3,93	7.53	4.44	3.94	4.71	1.40	0.92	1.21	0.53	
	Line	(in)	12	12	12	24	12	24	24	24	24	18	24	12	12	12	12	12	12	12	12	18	12	18	
	Vel	(tus)	3.14	2.55	1.08	5.18	1.25	5.96	5.81	4.60	5.70	5.28	4.32	4.16	2,42	4.80	5.75	6.08	3.03	5.23	2.65	5.80	2.63	5.32	
	Capac Full	(cfs)	2.78	2.73	3.98	39.71	6.81	17.42	17.65	17.28	17.47	7.97	17.38	3.45	2.88	7.64	10.59	8.13	7.66	8.38	4.56	10.91	4.24	8.29	
	Flow Rate	(cfs)	2.47	2.00	0.85	13.14	0.98	14.35	12.08	10.75	11,39	9.33	10.36	1,78	0,85	1.54	1.52	4.78	96.0	1.98	1.32	8.18	0.98	7.59	
	<del>ا</del> ر	(min)	7.2	0.9	5.0	11.9	5.0	19.2	11.0	16.8	10.4	15.0	2.6	5.6	5.0	5.0	10.0	15.0	10.0	15.0	10.0	8.8	5.0	7.7	
	Inlet Time	(min)	5.0	5.0	5.0	0.0	5.0	0.0	0.0	0.0	0.0	15.0	0.0	0.0	5.0	2.0	10.0	15.0	10.0	15.0	10.0	0.0	5.0	0.0	
	Total		0.43	0.33	0.14	2.74	0.16	3.69	2.44	2.59	2.26	2.14	2.00	0.29	0.14	0.24	0.30	1.10	0.19	0.45	0.26	1.53	0.16	1.36	
	Incr		0.10	0.20	0.14	00:00	0.16	00:00	00:00	00.00	00.0	2.14	00.00	00:00	0.14	0.24	0:30	1.10	0.19	0.45	0.26	00.00	0.16	0.00	
	Runoff	(C)	06.0	06.0	06.0	00.00	0.78	00.00	00.00	00.00	00.00	0.81	00.00	00.00	06.0	0.68	0.58	0.73	0.55	0.81	0.56	00.00	0.87	0.00	
	Total Area	(ac)	0.48	0.37	0.15	3.81	0.20	4.70	3.30	3.20	2.96	2.64	2.50	0,33	0.15	0.36	0.51	1.50	0.34	0.56	0.46	1.96	0.18	1.76	
	Drng Area	(ac)	0.11	0.22	0.15	00.0	0.20	00.0	0.00	00.0	00.0	2.64	00.0	00.0	0.15	0.36	0.51	1.50	0.34	0.56	0.46	0.00	0.18	0.00	
	Line	(ft)	125.000	180.000	150.000	129.460	25.640	158.350	134.970	361.870	88.540	265.180	109.350	87.500	89.670	10.190	6.640	11.260	20.310	10.610	21.440	130.560	8.280	169,460	
	DnStm Ln No		22	23	24	7	5	16	26	28	29	30	33	33	34	16	26	28	29	99	31	33	35	42	
	Line		DMH-15	DMH-14	DMH-13	DMH-10	CB-26	DMH-54	6-НМО	DMH-53	DMH-8	CB-19	DMH-7	DMH-7A	CB-18	CB-22	CB-14	CB-21	CB-13	CB-20	CB-12	9-HWQ	CB-15	DMH-5	
2	Line No.		23	24	25	56	27	28	59	30	31	32	33	34	35	36	37	38	39	40	4	42	43	4	

Hydraflow Storm Sewers Extension

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--|---|--|
| HGL<br>Dn        | (ft)   | 130.86   | 131.28   | 132.10  | 132.69  | 132.84  | 129.00   
   
   
   
   | 130.05   | 130.86  | 131.28   | 132.10  | 132.69  
  | 132.84   | 132.78   | 128.99   | 130.05  | 130.86  
   | 132.69  | 132.78   | 126.28  | 123.65  | 122.71   
  | 124.29   
   |  |   |  
   |
| Gnd/Rim<br>El Dn | (#)  | 134.60   | 134.80   | 135.20  | 134.80  | 135.05  | 133.50   
   
   
   
   | 134.50   | 134.60  | 134.80   | 135.20  | 134.80  
  | 135.05   | 135.90   | 133.50   | 134.50  | 134.60  
   | 134.80  | 135.90   | 127.10  | 127.15  | 00.00  
  | 126.90   
   |  |   |  
   |
| HGL              | (£)  | 131.07   | 131.79   | 132.46  | 132.80  | 132.86  | 129.33   
   
   
   
   | 130.31   | 130.87  | 131.29   | 132.59  | 132.69  
  | 132.87   | 132.98   | 129.31   | 130.31  | 130.87  
   | 132.69  | 132.79   | 127.16  | 125.18  | 123.74   
  | 124.76   
   |  | 5-27-2008   |  
   |
| Snd/Rim<br>El Up | (#)  | 134.80   | 135.20   | 134.80  | 135.05  | 134.30  | 133.00   
   
   
   
   | 134.00   | 134.30  | 134.00   | 135.90  | 134.50  
  | 134.30   | 134.70   | 133.00   | 134.00  | 134.30  
   | 134.50  | 134.50   | 0.00  | 130.50  | 126.90   
  | 127.50   
   |  | Date: 0   |  
   |
| Invert           | (£)  | 129.30   | 129.70   | 130.10  | 130.40  | 130.90  | 128.70   
   
   
   
   | 129.80   | 129.30  | 129.70   | 130.10  | 130.40  
  | 130.90   | 130.70   | 128.70   | 129.80  | 129.30  
   | 130.40  | 130.70   | 122.95  | 123.15  | 121.50   
  | 122.40   
   |  |   |  
   |
| Invert<br>Up     | (#)  | 129.70   | 130.10   | 130,40  | 130.90  | 131.30  | 129.00   
   
   
   
   | 130.00   | 130.00  | 130.00   | 130.70  | 130.70  
  | 131,30   | 131.40   | 129.00   | 130.00  | 130.00  
   | 130.60  | 131.00   | 126.00  | 124.50  | 122.40   
  | 122.90   
   |  | 12  |  
   |
| Line<br>Slope    | (%)  | 0.48   | 0.49   | 0.49  | 0.83  | 62.0  | 0.59   
   
   
   
   | 96.0   | 3,33  | 1.34   | 0.62  | 1.10  
  | 0.83   | 0.48   | 0.59   | 26.0  | 3.36  
   | 2.62  | 3.07   | 3.71  | 1,77  | 0.73   
  | 0.62   
   |  | lines: 1  |  
   |
| Line             | (in)   | 18   | 15   | 12  | 12  | 12  | 12   
   
   
   
   | 12   | 12  | 12   | 12  | 12  
  | 12   | 12   | 12   | 12  | 12  
   | 12  | 12   | 12  | 12  | 18   
  | 15   
   |  | imber of  |  
   |
| Vel              | (t/s)  | 3,55   | 4.51   | 3.80  | 2,09  | 1.01  | 2.78   
   
   
   
   | 2,98   | 0.98  | 1.01   | 3.49  | 0.68  
  | <u>£</u>   | 1,82   | 2.70   | 2.99  | 1.40  
   | 1.13  | 1.83   | 5,06  | 5.55  | 6.29   
  | 4.33   
   |  | ž   |  
   |
| Capac<br>Full    | (cfs)  | 7.84   | 4.89   | 2.71  | 3,52  | 3.43  | 2.95   
   
   
   
   | 3,78   | 7.04  | 4.47   | 3.05  | 4.04  
  | 3.52   | 2,67   | 2.95   | 3.81  | 70.7  
   | 6.25  | 92.9   | 7.43  | 5.14  | 9.70   
  | 5.50   
   |  |   |  
   |
| Flow<br>Rate     | (cfs)  | 6.14   | 5.54   | 2.98  | 1.64  | 0.79  | 0.59   
   
   
   
   | 0.53   | 0.73  | 0.79   | 2.74  | 0.53  
  | 0.87   | 1,43   | 0.53   | 0.54  | 1.06  
   | 0.88  | 1.44   | 3.98  | 2.60  | 10.02  
  | 5.32   
   |  |   |  
   |
| Tc               | (min)  | 7.2  | 9.9  | 5.7   | 5,3   | 5.0   | 5.0  
   
   
   
   | 5.0  | 5.0   | 5.0  | 0.9   | 5.0   
  | 5.0  | 5.0  | 5.0  | 5.0   | 5.0   
   | 5.0   | 5.0  | 20.0  | 5.0   | 9.0  
  | 8.5  
   |  |   |  
   |
| Inlet<br>Time    | (min)  | 0.0  | 0.0  | 0.0   | 0.0   | 5.0   | 5.0  
   
   
   
   | 5.0  | 5.0   | 5.0  | 0.0   | 5.0   
  | 5.0  | 5.0  | 5.0  | 5.0   | 5.0   
   | 5.0   | 5.0  | 20.0  | 5.0   | 0.0  
  | 0.0  
   |  |   |  
   |
| Total<br>CxA     |  | 1.07   | 0.95   | 0,49  | 0.27  | 0.13  | 0.09   
   
   
   
   | 0.09   | 0.12  | 0.13   | 0,46  | 0.09  
  | 0.14   | 0.23   | 60.0   | 0.09  | 0.17  
   | 0.14  | 0.23   | 1.04  | 0.41  | 1.89   
  | 0.98   
   |  |   |  
   |
| Incr             |  | 00.00  | 00.00  | 00.00   | 00.00   | 0.13  | 0.09   
   
   
   
   | 0.09   | 0.12  | 0.13   | 00.00   | 60.0  
  | 0.14   | 0.23   | 0.09   | 0.09  | 0.17  
   | 0,14  | 0.23   | 1.04  | 0.41  | 00.00  
  | 00.00  
   |  |   |  
   |
| Runoff           | ()   | 00.0   | 00'0   | 00.00   | 00.00   | 0.79  | 0.85   
   
   
   
   | 0.85   | 06.0  | 62:0   | 00'0  | 0.85  
  | 0.63   | 0.71   | 0.85   | 0.86  | 0.84  
   | 0.67  | 0.88   | 0.70  | 06.0  | 00.00  
  | 00:00  
   |  |   |  
   |
| Total<br>Area    | (ac)   | 1.43   | 1.27   | 69.0  | 0.38  | 0.16  | 0.11   
   
   
   
   | 0.10   | 0,13  | 0.16   | 0.58  | 0.10  
  | 0.22   | 0.32   | 0.10   | 0.10  | 0.20  
   | 0.21  | 0.26   | 1.49  | 0.46  | 2.91   
  | 1.45   
   |  |   |  
   |
| Drng<br>Area     | (ac)   | 00:00  | 00.00  | 00:00   | 00.00   | 0.16  | 0.11   
   
   
   
   | 0.10   | 0.13  | 0.16   | 00:00   | 0.10  
  | 0.22   | 0.32   | 0.10   | 0.10  | 0.20  
   | 0.21  | 0.26   | 1.49  | 0.46  | 00.00  
  | 00.00  
   |  |   |  
   |
| Line<br>Length   | (ft)   | 84.140   | 81.710   | 60.670  | 60.000  | 50.700  | 51.140   
   
   
   
   | 20.790   | 21.040  | 22.340   | 96.280  | 27.340  
  | 47.960   | 145.680  | 51.140   | 20.560  | 20.820  
   | 7.620   | 9.770  | 82.240  | 76.133  | 123.910  
  | 80.790   
   |  | _   |  
   |
| DnStm<br>Ln No   |  | 44   | 45   | 46  | 47  | 48  | 33   
   
   
   
   | 42   | 44  | 45   | 46  | 47  
  | 48   | 42   | 33   | 42  | 4   
   | 47  | 54   | 4   | _   | Outfall  
  | 99   
   |  | and TC.stn  |  
   |
| Line<br>ID       |  | DMH-4  | DMH-3  | DMH-2   | DMH-1   | CB-2  | CB-10  
   
   
   
   | CB-8   | CB-6  | CB-5   | DMH-52  | CB-3  
  | CB-1   | CB-17  | CB-11  | CB-9  | CB-7  
   | CB-4  | CB-16  | FES-16  | DMH-55  | DMH-34   
  | DMH-33   
   |  | t File: Wayla   |  
   |
| Line<br>No.      |  | 45   | 46   | 47  | 48  | 49  | 20   
   
   
   
   | 51   | 52  | 53   | 54  | 55  
  | 26   | 22   | 58   | 59  | 09  
   | 61  | 62   | 63  | 64  | 65   
  | 99   
   |  | Projec  |  
   |
|                  | Line DnStm Line Drng Total Runoff Incr Total Inlet Tc Flow Capac Vel Line Line Invert Invert Gnd/Rim HGL Gnd/Rim H | Line DnStm Line Drng Total Runoff Incr Total Inlet Tc Flow Capac Vel Line Line Invert Gnd/Rim HGL Gnd/ | Line DnStm Line Drigth Area Coeff CxA CxA Time To (ft) (min) (min) (cfs) (cfs) (cfs) (ft/s) (in) (cfs) | Line         DnStm         Line         Total         Runoff         Total         Inlet         Total         Inlet         Total         Inlet         Total         Inlet         Full         Ave         Size         Line         Line         Invert         Invert         Gnd/Rim         HGL         Gnd/Rim           ID         Ln No         Length         Area         Coeff         CxA         Time         Full         Ave         Size         Size         Size         Dn         Pn         Pn | Line         DnStm         Line         Total         Total         Inlet         Total         Inlet         Total         Inlet         Total         Inlet         Full         Ave         Size         Line         Line         Invert         Invert         Gnd/Rim         HGL         Gnd/Rim           ID         Ln No         Length         Area         Coeff         CxA         Time         Full         Full         Ave         Size         Size         Size         Up         Dn         Fill         Pull         Pull         Ave         Size         Size | Line         DnStm         Line         Area         Coeff         CxA         Time         Total         Index         Fill         Ave         Size         Siope         Up         Dn         HGL         Gnd/Rim           ID         Ln No         Length         Area         Coeff         CxA         Time         Time         Full         Ave         Size         Siope         Up         Dn         HGL         Ave         Time         Full         Ave         Size         Siope         Up         Dn         HGL         Bright         Bright< | Line         DnStm         Line         Area         Coeff         CXA         Time         Trine         Full         Ave         Size         Line         Line         Invert         Invert </th <th>Line         DnStm         Line         Area         Area         Cod         CXA         Time         Fine         Fine         Line         Fine         Fine         Fine         Fine         Fine         Line         Line</th> <th>Line DnStm Line Area Area Coeff CxA Time Time Time Time Time Time Time Time</th> <th>Line DnStm Line Area Area Area Coeff CxA Time Trine Tr</th> <th>  Line   Diskin   Line   Area   Total   Total</th> <th>  Line   District   Line   Line   Line   Line   Line   Cari   Cari   Cari   Line   Cari   Line   Lin</th> <th>  Link   District   Link   Aria   Aria   Aria   Aria   Aria   Aria   Codf   CxA   Time   Time   Time   Flow   Capa   Flow   Size   Slope   Up   Div   El Up   Div   El Up   El</th> <th>  Link   District   Link   Area   Area   Area   Coeff   CxA   CxA   Time   To   Fale   Full   Area   Sign   Link   Invert   Sign   Invert   Sign   Si</th> <th>  Line   District Lange   Line   Line   Area   Coeff   Coeff  </th> <th>  Line   Diskip   Line   Line</th> <th>  Line   Diskin   Line   Line</th> <th>  Line   Line   Line   Line   Line   Area   Area   Cond   Cond   Line   Cond   Line   Line  </th> <th>Unit         Line         Area         Cond         Total         Total         Total         Total         Total         Total         Total         Area         Cond         Cond         Area         Cond         Total         Area         Cond         Cond         Cond         Total         Total         Total         Total         Total         Area         Cond         Cond         Cond         Total         Total</th> <th>Line         Long         Area         Cond         Total         Tot</th> <th>  Line   Diskin   Line   Aria   Aria</th> <th>Line         DNSM         Line         Total         Face         Total         Inside         Total         Area         Conf.         Conf.         Total         Inside         Total         Invent         Line         Line         Line         Line         Line         Conf.         Conf.         Total         Timel         Timel         Area         Conf.         Conf.         Timel         Timel         Timel         Area         Line         Timel         Timel<th>Up.         Ling         Ling         Area         Cond.         Col.         <th< th=""><th>Line         Line         <th< th=""><th>  Link   Dissip   Link   Aria   Aria   Aria   Aria   Link   Aria   Link   Aria   Aria</th><th>Unine   Dissip   Line   Area   Area   Area   Conf   Con</th></th<></th></th<></th></th> | Line         DnStm         Line         Area         Area         Cod         CXA         Time         Fine         Fine         Line         Fine         Fine         Fine         Fine         Fine         Line         Line | Line DnStm Line Area Area Coeff CxA Time Time Time Time Time Time Time Time | Line DnStm Line Area Area Area Coeff CxA Time Trine Tr | Line   Diskin   Line   Area   Total   Total | Line   District   Line   Line   Line   Line   Line   Cari   Cari   Cari   Line   Cari   Line   Lin | Link   District   Link   Aria   Aria   Aria   Aria   Aria   Aria   Codf   CxA   Time   Time   Time   Flow   Capa   Flow   Size   Slope   Up   Div   El Up   Div   El Up   El | Link   District   Link   Area   Area   Area   Coeff   CxA   CxA   Time   To   Fale   Full   Area   Sign   Link   Invert   Sign   Invert   Sign   Si | Line   District Lange   Line   Line   Area   Coeff   Coeff | Line   Diskip   Line   Line | Line   Diskin   Line   Line | Line   Line   Line   Line   Line   Area   Area   Cond   Cond   Line   Cond   Line   Line | Unit         Line         Area         Cond         Total         Total         Total         Total         Total         Total         Total         Area         Cond         Cond         Area         Cond         Total         Area         Cond         Cond         Cond         Total         Total         Total         Total         Total         Area         Cond         Cond         Cond         Total         Total | Line         Long         Area         Cond         Total         Tot | Line   Diskin   Line   Aria   Aria | Line         DNSM         Line         Total         Face         Total         Inside         Total         Area         Conf.         Conf.         Total         Inside         Total         Invent         Line         Line         Line         Line         Line         Conf.         Conf.         Total         Timel         Timel         Area         Conf.         Conf.         Timel         Timel         Timel         Area         Line         Timel         Timel <th>Up.         Ling         Ling         Area         Cond.         Col.         <th< th=""><th>Line         Line         <th< th=""><th>  Link   Dissip   Link   Aria   Aria   Aria   Aria   Link   Aria   Link   Aria   Aria</th><th>Unine   Dissip   Line   Area   Area   Area   Conf   Con</th></th<></th></th<></th> | Up.         Ling         Ling         Area         Cond.         Col.         Col. <th< th=""><th>Line         Line         <th< th=""><th>  Link   Dissip   Link   Aria   Aria   Aria   Aria   Link   Aria   Link   Aria   Aria</th><th>Unine   Dissip   Line   Area   Area   Area   Conf   Con</th></th<></th></th<> | Line         Line <th< th=""><th>  Link   Dissip   Link   Aria   Aria   Aria   Aria   Link   Aria   Link   Aria   Aria</th><th>Unine   Dissip   Line   Area   Area   Area   Conf   Con</th></th<> | Link   Dissip   Link   Aria   Aria   Aria   Aria   Link   Aria   Link   Aria   Aria | Unine   Dissip   Line   Area   Area   Area   Conf   Con |

Hydraflow Storm Sewers Extension

2																					
Line No.	Line ID	DnStm Ln No	Line Length	Drng Area	Total Area	Runoff	CXA	Total	Inlet	JC	Flow Rate	Capac	Vel	Line Size	Line	Invert	Invert	Gnd/Rim EI Up	HGL	Gnd/Rim El Dn	HGL
			(ft)	(ac)	(ac)	(C)			(min)	(min)	(cfs)	(cfs)	(£/,s)	(ii)	(%)	(£)	£	£	(#)	(#)	(H)
29	DMH-32	99	128.490	00:00	1.07	0.00	00.00	0.73	0.0	7.7	4.12	7.17	3.37	15	1.05	124.25	122.90	129.05	125.47	127.50	125.05
89	DMH-31	29	116.930	00:00	0.89	0.00	00.00	0.62	0.0	6.9	3.59	4.80	3.01	15	0.47	124.80	124.25	129.05	125.92	129.05	125.64
69	DMH-30	89	100.600	00.00	99'0	0.00	0.00	0.43	0.0	6.2	2.53	2.85	3,22	12	0.55	125.35	124.80	130.05	126.50	129.05	126.07
20	DMH-29	69	103.790	00.00	0.50	0.00	0.00	0.32	0.0	5,5	1.94	2.81	2,47	12	0.53	125.90	125.35	130.05	126.90	130.05	126.66
71	CB-32	70	76.360	0.37	0.37	0.62	0.23	0.23	5.0	2.0	1.44	3.42	2.43	12	62.0	126.50	125.90	130.50	127.08	130.05	126.99
72	CB-42	65	27.220	0.35	0.35	0.61	0.21	0.21	5.0	5.0	1.34	5.73	1,71	12	2.20	123.00	122.40	126.50	124.32	126.90	124.29
73	CB-37	99	13.920	0.38	0.38	0.65	0,25	0.25	5.0	5.0	1.55	3,27	1,98	12	0.72	123.00	122.90	126.50	125.07	127.50	125.05
74	CB-36	29	7.110	0.18	0.18	0.63	0.11	0,11	5.0	5.0	0.71	10.23	4.28	12	2.03	126.00	125.50	129.00	126.78	129.05	125.68
75	CB-35	89	6.070	0.23	0.23	0.85	0.20	0.20	5.0	5.0	1.23	7.00	1.56	12	3,29	125.00	124.80	129.00	126.07	129.05	126.07
92	CB-34	69	5,850	0.16	0.16	0.68	0.11	0.11	5.0	5.0	0,68	7.13	1.10	12	3,42	126.00	125.80	130.00	126.66	130.05	126.66
77	CB-33	70	6.770	0.13	0.13	0.67	0.09	0.09	5.0	5.0	0.55	4.69	0.70	12	1.48	126.00	125.90	130.00	126.99	130.05	126.99
78	DMH-38	65	61.040	00:00	1.11	0.00	00.00	69"0	0.0	8.5	3.76	5.95	4.80	72	2.38	123.85	122.40	127.50	124.84	126.90	124.29
79	DMH-37	78	124.040	00:00	1.	0.00	00.00	69.0	0.0	7.6	3.89	5.06	3.57	15	0.52	124.50	123.85	129.05	125.43	127.50	125.10
80	DMH-36	79	138.400	00:00	0.82	0.00	0.00	0.50	0.0	6.7	2.94	2.74	3.74	12	0.51	125.20	124.50	129.55	126.48	129.05	125.68
	DMH-35	80	127.250	00:00	09.0	0.00	00'0	0.36	0.0	5.9	2.18	2.76	2.78	12	0.51	125.85	125.20	130.05	127.10	129.55	126.70
82	CB-38	8	130.000	0.39	0.39	0.55	0.21	0.21	5.0	5.0	1.35	2.73	1.79	12	0.50	126.50	125.85	130.50	127.37	130.05	127.22
83	CB-41	79	6,460	0.29	0.29	0.65	0.19	0.19	5.0	5.0	1.18	10.73	1.87	12	7.74	125.00	124.50	129.00	125.64	129.05	125.68
84	CB-40	80	6.460	0.22	0.22	0.65	0.14	0.14	5.0	5.0	0.90	8.31	1.14	12	4.64	125.50	125.20	129.50	126,70	129.55	126.70
82	CB-39	8	5.350	0.21	0.21	0.70	0.15	0.15	5.0	5.0	0.92	6.46	1.18	12	2.80	126.00	125.85	130.00	127.23	130.05	127.22
86	DMH-50	Outfall	67.160	00:00	0.75	0.00	00.00	0.43	0.0	5.4	2.64	3.80	4.58	12	76.0	121.65	121.00	125.75	122.34	123.50	121.69
87	CB-53	86	11.130	0.43	0.43	0.55	0.24	0.24	5.0	5.0	1.49	6.33	3.10	12	2.70	121.95	121.65	125.95	122.47 j	125.75	122.34
88	CB-52	86	57.410	0.32	0.32	09.0	0.19	0.19	5.0	5.0	1.21	2.79	2.71	12	0.52	121.95	121.65	125.95	122.42	125.75	122.34
Proje	Project File: Wayland TC.stm	and TC.st	E										Ž	mber of	Number of lines: 112	2		Date: 0	05-27-2008		

NOTES: \*\* Critical depth

Hydraflow Storm Sewers Extension

Line No.	Line ID	DnStm Ln No	Line	Drng Area	Total Area	Runoff	CxA	Total	Inlet	J 2	Flow (Rate	Capac Full	Vel L Ave	Line 1 Size S	Line	Invert	Invert Dn	Gnd/Rim El Up	HGL Up	Gnd/Rim El Dn	HGL
			(ft)	(ac)	(ac)	(0)			(min)	(min)	(cfs)	(cfs)	(£/s)	(in)	(%)	(#)	£	(£)	(#)	(£)	(H)
89	DMH-45	Outfall	137.320	0.00	3.34	0.00	00.00	2.65	0.0	9.3	13.92	17.49	6.18	24	0.51	127.60	126.90	131.25	128.98	128.90	128.22
06	DMH-44	89	155.480	00'0	3,22	0.00	0.00	2.57	0.0	80	14.05	17.58	5.64	24	0.51	128.40	127.60	133.50	129.73 j	131.25	129.29
91	DMH-43	06	96.530	0.00	2,77	0.00	00.00	2.28	0.0	9.7	12.77	10.36	7.23	8	0,83	129.20	128.40	133.40	131.57	133.50	130.35
92	DMH-43A	91	142.390	00.00	1.94	00.0	00.00	1.53	0.0	6.7	8.92	15.91	2.84	24	0,42	129.80	129.20	133.80	132.57	133.40	132.38
93	CB-43	92	108.000	0.00	1.07	0.00	0.00	06.0	0.0	0.9	5.38	11.99	3.05	18	1.	131.00	129.80	134.50	132.93	133.80	132.69
94	CB-44A	93	145.150	0.95	0.95	0.86	0.82	0.82	5.0	5.0	5.13	11.37	3.25	18	1.00	132.20	130.75	134.50	133.33	134.50	133.08
95	CB-54	88	108.680	0.12	0.12	0.65	0.08	0.08	5.0	5.0	0.49	2.98	0.62	12	09.0	128.25	127.60	132.25	129.31	131.25	129.29
96	CB-46	06	69.590	0.45	0.45	0.65	0.29	0.29	5.0	5.0	1.84	2.74	2.34	12	0.50	128.75	128.40	132.25	130.51	133.50	130.35
26	CB-43	92	21.710	0.87	0.87	0.73	0.64	0.64	5.0	5.0	3.99	4.75	3.25	15	0.46	129.90	129.80	133,40	132.76	133.80	132.69
86	CB-45	91	35.992	0.20	0.83	06.0	0.18	0.75	2.0	7.3	4,25	7.34	2.41	8	0.42	129.35	129.20	133.55	132.43	133.40	132.38
66	DMH-42	86	61.058	0.19	0.63	06.0	0.17	0.57	5.0	6.9	3.28	8.61	1.86	8	0.57	129.70	129.35	133.80	132.53	133.55	132.48
100	DMH-41	66	278.000	0.44	0.44	06.0	0.40	0.40	5.0	5.0	2,49	5.63	2.03	15	0,65	131.50	129.70	135.50	132.93	133.80	132.58
101	CB-44	93	30.312	0.12	0.12	0.65	0.08	0.08	2.0	5.0	0.49	13.02	0.40	15	3,46	131.80	130.75	0.00	133.08	134.50	133.08
102	DMH-47	Outfall	29.170	0.00	3.00	0.00	00.00	1.80	0.0	20.3	6.82	11.54	3.86	9	1.03	128.50	128.20	133.55	130.34	130.20	130.23
103	DMH-46	102	112.150	0.00	0.59	0.00	00.00	0.45	0.0	5.3	2.82	2.82	3.59	12	0.54	129.10	128.50	132.05	131.15	133.55	130.56
104	CB-50	103	068'9	0.27	0.27	06.0	0.24	0.24	5.0	5.0	1.53	4.65	1.94	12	1.45	129.20	129.10	132.00	131.36	132.05	131.34
105	FES-13	102	46.210	2.41	2.41	0.56	1.35	1.35	20.0	20.0	5.14	7.28	4.19	15	1.08	129.00	128.50	131.00	130.81	133.55	130,56
106	CB-49	103	42.330	0.32	0.32	99.0	0.21	0.21	5.0	5.0	1.33	2.65	1.69	12	0.47	129.30	129.10	132.00	131.40	132.05	131.34
107	CB-47	Outfall	18.000	0.53	0.53	0.13	0.07	0.07	10.0	10.0	0.35	7.04	0.45	12	3.33	127.60	127.00	130.60	128.84	129.00	128.84
108	FES-12	Outfall	54.680	1.58	1.58	0.64	1.01	1.01	15.0	15.0	4.41	4.67	6.01	12	1.46	129.00	128.20	131.00	129.88	130.50	129.08
109	CB-48	Outfall	000.9	0.62	0.62	0.58	0.36	0.36	5.0	5.0	2.26	4.98	4.27	12	1.67	128.30	128.20	131.30	128.94	130.50	128.84
110	DMH-49	Outfall	17.390	0.00	0.49	0.00	00.00	0.42	0.0	5.4	2.59	5.07	3.92	12	1.73	127.70	127.40	132.25	128.38 j	129.00	128.38
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Hydraflow Storm Sewers Extension

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Hydraflow Storm Sewers Extension

## APPENDIX E: LONG TERM POLLUTION PREVENTION PLAN

# LONG TERM POLLUTION PREVENTION PLAN (LTPPP) MATERIALS MANAGEMENT PLAN

Applicant: Twenty Wayland, LLC

260 Boston Post Road, Suite 9

Wayland, MA 02109

Prepared by: R.J. O'Connell & Associates, Inc.

80 Montvale Avenue Stoneham, MA

### A. PROGRESS DRAWING

The Civil Construction plan set includes an Erosion and Sediment Control Plans which shall be posted inside the job trailer wall. This plan will be used to record the locations of the Job Trailer, Sanitary Waste Facilities, Solid Waste Facilities, Fuel Storage Area, Equipment Service Area, and Concrete Washout Pit. Any time any of these facilities are relocated on the site, a new location will be noted on the drawing.

### **B. MATERIALS COVERED**

The following materials or substances are expected to be present onsite during construction:

Concrete/Additives/Wastes Cleaning solvents

Detergents Petroleum based products

Paints/Solvents Pesticides
Acids Fertilizers
Solid and construction wastes Sanitary wastes

Soil stabilization additives

### C. MATERIALS MANAGEMENT PRACTICES

The following are the material management practices that will be used to reduce the risk of spills or other accidental exposure of materials and substances to stormwater runoff. The Contractor's Superintendent will be responsible for ensuring that these procedures are followed:

### 1. Good Housekeeping

The following good housekeeping practices will be followed onsite during construction:

- a) An effort will be made to store only enough products required to do the job.
- b) All materials stored onsite will be stored in a neat, orderly manner and, if possible, under a roof or in a containment area. At a minimum, all containers will be stored with their lids on when not in use. Drip pans shall be provided under all dispensers.
- c) Products will be kept in their original containers with the original manufacturer's label in legible condition.
- d) Substances will not be mixed with one another unless recommended by the manufacturer.
- e) Whenever possible, all of a product will be used up before disposing of the container.
- f) Manufacturer's recommendations for proper use and disposal will be followed.

g) The Contractor's Superintendent will be responsible for daily inspections to ensure proper use and disposal of materials.

### 2. Hazardous Substances

These practices will be used to reduce the risks associated with Hazardous Substances. Material Safety Data Sheets (MSDS's) for each product with hazardous properties that is used at the Project will be obtained and used for the proper management of potential wastes that may result from these products. An MSDS will be posted in the immediate area where such product is stored and/or used and another copy of each MSDS will be maintained in the job trailer at the Project. Each employee who must handle a Hazardous Substance will be instructed on the use of MSDS sheets and the specific information in the applicable MSDS for the product he/she is using, particularly regarding spill control techniques.

- a) Products will be kept in original containers with the original labels in legible condition.
- b) Original labels and MSDS's will be procured and used for each product.
- c) If surplus product must be disposed manufacturer's and local/state/federal required methods for proper disposal must be followed.

### 3. Hazardous Waste

It is imperative that all Hazardous Waste be properly identified and handled in accordance with all applicable Hazardous Waste Standards, including the storage, transport and disposal of the Hazardous Wastes. There are significant penalties for the improper handling of Hazardous Wastes. It is important that the Site Superintendent seeks appropriate assistance in making the determination of whether a substance or material is a Hazardous Waste. For example, Hazardous Waste may include certain Hazardous Substances, as well as pesticides, paints, paint solvents, cleaning solvents, pesticides, contaminated soils, and other materials, substances or chemicals that have been discarded (or are to be discarded) as being out-of-date, contaminated, or otherwise unusable, and can include the containers for those substances; other materials and substances can also be or become Hazardous Wastes, however. The Contractor's Superintendent is also responsible for ensuring that all site personnel are instructed as to these Hazardous Waste requirements and also that the requirements are being followed.

### 4. Product Specific Practices

The following product specific practices will be followed on the job site:

### **Petroleum Products**

All onsite vehicles will be monitored for leaks and receive regular preventative maintenance to reduce the chance of leakage. Petroleum products will be stored in tightly sealed containers which are clearly labeled. Petroleum storage tanks shall be located at minimum 100 linear feet from drainage ways, inlets and surface waters. Any petroleum storage tanks stored onsite will be located within a containment area that is designed with an impervious surface between the tank and the ground. The secondary containment must be designed to provide a containment volume that is equal to 110% of the volume of the largest tank. Any mobile petroleum tank shall be parked in a vehicular service area surrounded by a berm that provides a containment volume that is equal to 110% of the volume of the largest tank. Containment must provide sufficient volume to contain expected precipitation and 110% volume of the largest tank.

Accumulated rainwater or spills from containment areas are to be promptly pumped into a containment device and disposed of properly by a licensed Hazardous Waste transporter. Drip pans shall be provided for all dispensers. Any asphalt substances used onsite will be applied according to the manufacturer's recommendations. The location of any fuel tanks and/or equipment storage areas must be identified on the Erosion Control Plan by the Contractor once the locations have been determined.

### **Fertilizers**

Fertilizers will be applied only in the minimum amounts recommended by the manufacturer. Once applied, fertilizer will be worked in the soil to limit exposure to storm water. Storage will be in a covered shed. The contents of any partially used bags of fertilizer will be transferred to a sealable plastic bin to avoid spills.

### Paints, Paint Solvents, and Cleaning Solvents

All containers will be tightly sealed and stored when not in use. Excess paint and solvents will not be discharged to the storm sewer system but will be properly disposed of according to manufacturer's instructions or state and federal regulations.

### Concrete Wastes

Concrete trucks will be allowed to wash out or discharge surplus concrete or drum wash water on the site, but only in specifically designated diked and impervious washouts which have been prepared to prevent contact between the concrete wash and storm water. Waste generated from concrete wash water shall not be allowed to flow into drainage ways, inlets, receiving waters or highway right of ways, or any location other than the designated concrete washout. Waste concrete may be poured into forms to make riprap or other useful concrete products. Proper signage designating the "Concrete Washout" shall be placed near the facility. Concrete Washouts shall be located at minimum 100 linear feet from drainage ways, inlets and surface waters.

The hardened residue from the concrete wash out diked areas will be disposed of in the same manner as other non-hazardous construction waste materials or may be broken up and used on site as deemed appropriate by the Contractor. Maintenance of the washout is to include removal of hardened concrete. Facility shall have sufficient volume to contain all the concrete waste resulting from washout and a minimum freeboard of 12 inches. Facility shall not be filled beyond 95% capacity and shall be cleaned out once 75% full unless a new facility is constructed. The Contractor's Superintendent will be responsible for seeing that these procedures are followed.

Saw-cut Portland Cement Concrete (PCC) slurry shall not be allowed to enter storm drains or Watercourses. Saw-cut residue should not be left on the surface of pavement or be allowed to flow over and off pavement. Residue from saw-cutting and grinding shall be collected by vacuum and disposed of in the concrete washout facility.

The Project may require the use of multiple concrete wash out areas. These concrete wash out areas are to be made available to all trades and subcontractors working on the Project. The Contractor may designate certain wash out areas for particular trades or subcontractors, but the Contractor is responsible for the management of all concrete washout

areas on the Project. All concrete wash out areas will be located in an area where the likelihood of the area contributing to storm water discharges is negligible. If required, additional BMPs must be implemented to prevent concrete wastes from contributing to storm water discharges. The location of concrete wash out area(s) must be identified on the Civil plans by the Contractor once the locations have been determined. In addition, a standard detail on the construction of the concrete wash out is included in the Civil detail sheets.

### 5. Solid and Construction Wastes

All waste materials will be collected and stored in an appropriately covered container and/or securely contained metal dumpster rented from a local waste management company which must be a licensed solid waste management company. The dumpster will comply with all local and state solid waste management regulations.

All trash and construction debris from the site will be deposited in the dumpster. The dumpster will be emptied a minimum of once per week or more often if necessary. Once building construction has commenced, the dumpster will be emptied a minimum of once per week or when 95% full, or more often if necessary to prevent over-flow and the trash will be hauled to a landfill. No construction waste materials will be buried on site. All personnel will be instructed regarding the correct procedures for waste disposal.

All waste dumpsters and roll-off containers will be located in an area where the likelihood of the containers contributing to storm water discharges is negligible. Solid waste containers shall be located no less than 50 feet from any storm inlet, drainage way, or surface water. If required, additional BMPs must be implemented, such as gravel bags, wattles, Dikes, berms, and fences around the base, to prevent wastes from contributing to storm water discharges. The location of waste dumpsters and roll-off containers must be identified on the Civil plans by the Contractor once the locations have been determined.

### 6. Sanitary Wastes

A minimum of one portable sanitary unit will be provided for every ten (10) workers on the site. All sanitary waste will be collected from the portable units a minimum of one time per week by a licensed portable facility provider in complete compliance with local and state regulations.

All sanitary waste units will be located in an area where the likelihood of the unit contributing to storm water discharges is negligible. Additional containment BMPs must be implemented, such as gravel bags or specially designed plastic skid containers around the base, to prevent wastes from contributing to storm water discharges. The location of sanitary waste units must be identified on the Civil plans by the contractor once the locations have been determined

### 7. Contaminated Soils

Any contaminated soils (resulting from spills of Hazardous Substances or Oil or discovered during the course of construction) which may result from Construction Activities will be contained and cleaned up immediately in accordance with the procedures given in the Materials Management Plan and in accordance with applicable state and federal regulations. Contaminated soils not resulting from Construction Activities, or which pre-existed Construction Activities, but which are discovered by virtue of Construction Activities, should be reported in the same manner as spills, but with sufficient information to indicate that the discovery of an existing condition is being

reported. If there is a release that occurs by virtue of the discovery of existing contamination, this should be reported as a spill, if it otherwise meets the requirements for a reportable spill.

### D. SPILL PREVENTION AND RESPONSE PROCEEDURES

The Contractor will train all personnel in the proper handling and cleanup of spilled Hazardous Substances or Oil. No spilled Hazardous Substances or Oil will be allowed to come in contact with storm water discharges. If such contact occurs, the storm water discharge will be contained on site until appropriate measures in compliance with state and federal regulations are taken to dispose of such contaminated storm water. It shall be the responsibility of the Contractor's Superintendent to be properly trained, and to train all personnel in spill prevention and clean up procedures.

- 1. In order to prevent or minimize the potential for a spill of Hazardous Substances or Oil to come into contact with storm water, the following steps will be implemented:
  - a) All Hazardous Substances or Oil (such as pesticides, petroleum products, fertilizers, detergents, construction chemicals, acids, paints, paint solvents, cleaning solvents, additives for soil stabilization, concrete curing compounds and additives, etc.) will be stored in a secure location, with their lids on, preferably under cover, when not in use.
  - b) The minimum practical quantity of all such materials will be kept at the Project.
  - c) A spill control and containment kit (containing, for example, absorbent materials, acid neutralizing powder, brooms, dust pans, mops, rags, gloves, goggles, plastic and metal trash containers, etc.) will be provided at the storage site.
  - d) Manufacturer's recommended methods for spill cleanup will be clearly posted and site personnel will be trained regarding these procedures and the location of the information and cleanup supplies.
  - e) It is the Contractors responsibility to ensure that all Hazardous Waste discovered or generated at the Project site is disposed of properly by a licensed hazardous material disposal company. The Contractor is responsible for not exceeding Hazardous Waste storage requirements mandated by the EPA or state and local authority.
- 2. In the event of a spill of Hazardous Substances or Oil, the following procedures must be followed:
  - a) All measures must be taken to contain and abate the spill and to prevent the discharge of the Hazardous Substance or Oil to storm water or off-site. (The spill area must be kept well ventilated and personnel must wear appropriate protective clothing to prevent injury from contact with the Hazardous Substances.)
  - b) For spills of less than five (5) gallons of material, proceed with source control and containment, clean-up with absorbent materials or other applicable means unless an imminent hazard or other circumstances dictate that the spill should be treated by a professional emergency response contractor.
  - c) For spills greater than five (5) gallons of material immediately contact the MA DEP Hazardous Waste Incident Response Group at (617) 792-7653 and an approved emergency response contractor. Provide information on the type of material spilled, the location of the spill, the quantity spilled, and the time of the spill to the emergency response contractor or coordinator, and proceed with prevention, containment and/or clean-up if so desired.
  - d) If there is a Reportable Quantity (RQ) release during the construction period, then the National Response Center will be notified immediately at (800) 424-8802; within 14 days a report will be submitted to the EPA regional office describing the release, the date and circumstances of the

release and the steps taken to prevent another release. This Stormwater Pollution Prevention Plan must be updated to reflect any such steps or actions taken and measures to prevent the same from reoccurring.

3. The Contractor's Superintendent will be the spill prevention and response coordinator. He will designate the individuals who will receive spill prevention and response training. These individuals will each become responsible for a particular phase of prevention and response. The names of these personnel will be posted in the material storage area and in the office trailer onsite.

# E. ILLICIT DISCHARGE STATEMENT- CONTROL OF NON-STORMWATER DISCHARGES

Certain types of discharges are allowable under the U.S. Environmental Protection Agency Construction General Permit, and it is the intent of this LTPPP to allow such discharges. These types of discharges will be allowed under the conditions that no pollutants will be allowed to come in contact with the water prior to or after its discharge. The control measures which have been outlined previously in this LTPPP will be strictly followed to ensure that no contamination of these non-storm water discharges takes place.

# APPENDIX F: CONSTRUCTION PERIOD POLLUTION PREVENTION AND SEDIMENTATION PLAN

# CONSTRUCTION PERIOD POLLUTION PREVENTION AND SEDIMENTATION PLAN

### CONTACT INFORMATION/ RESPONSABLE PARTIES

### **Operators:**

Owner

Twenty Wayland, LLC 260 Boston Post Road, Suite 9 Wayland, MA 02109

Contractor

Not selected at this time

*Plan Prepared by* 

R.J. O'Connell & Associates, Inc. 80 Montvale Avenue Stoneham, MA 02180

### I. PROJECT DESCRIPTION

The project site has an area of approximately 56.9 acres and is located at 400 Boston Post Road, in Wayland, MA (See Figure 1 - Locus Map). The site is bound by Route 20 (Boston Post Road) to the south, the Wayland Business Center property to the North, Sudbury River to the west and the Wayland meadows property and Route 27 (Old Sudbury Road) to the East. There are wetland areas on the site. The larger wetland is located at the western portion of the site adjacent to Sudbury River, two smaller wetland areas are at the north east portion of the site adjacent to the Wayland Business Center property, and on the south east portion of site adjacent to Route 20.

Approximately 25 acres of the site is currently developed. The existing development contains a building formerly occupied by Raytheon with a footprint area of  $\pm 272,700$  square feet and a  $\pm 10,500$  square foot building formerly utilized as a daycare center and associated parking. There is a Wastewater Treatment facility on site which is owned and operated by the Town of Wayland. The existing topography of the project site generally slopes east to west and ranges from elevation  $\pm 146$  at the eastern property line adjacent to the Wayland Meadows Property to elevation  $\pm 116$  at the western side of the site in the large wetland area adjacent to Sudbury River.

The proposed development program consists of demolishing the existing ±272,700 square foot building and constructing a mixed use development consisting of residential, municipal and retail use buildings, with associated parking facilities, utilities, and stormwater collection system (See Figure 2 - Site Plan). The stormwater management system for the proposed project has been designed in accordance with the MADEP's Stormwater Management Policy and Standards and the Town of Wayland's Wetlands and Water Resources Bylaw Chapter 194 Rules and Regulations.

Stormwater quality control will be achieved through a program of Best Management Practices (BMP's). The proposed stormwater management system will significantly improve the quality of the stormwater runoff. The existing pavement runoff drains to catch basins which direct runoff to wetland resource areas without additional

water quality treatment. The proposed stormwater management system for the project will include new catch basins with deep sumps and hoods, and the use of innovative low impact development (LID) techniques.

Low Impact Development is a stormwater management approach with the goal to mimic the site's predevelopment hydrology. This is done by using design techniques that infiltrate, filter, store, and detain water throughout the site using decentralized micro-scale controls. LID includes structural and non-structural strategies such as retention areas, reduction of impervious surfaces, lengthening of flow paths, and the preservation of existing vegetation and landscape features. Redevelopment and improving stormwater quality of existing sites, and energy and water conservation are also examples of LID techniques.

LID techniques proposed for the project include the use of water quality swales, rain gardens, and bio-retention basins to increase times of concentration, promote groundwater recharge, and enhance water quality. The water quality swales will be planted with grass on the bottom and sides to slow the runoff velocity and filter pollutants. The rain gardens and bio-retention basins will be planted with a combination of grasses, perennials, shrubs, and small trees. The clean stormwater runoff from the building rooftops will be directed to the water quality swales and bio-retention basins to provide additional groundwater recharge.

### II. EROSION AND SEDIMENT CONTROL BMPS

### A. MINIMIZE DISTURBED AREA AND PROTECT NATURAL FEATURES AND SOIL

Prior to any construction activity, silt fence shall installed at the limits of the work area and filter bags installed in existing catch basins within the construction site area as shown on the plans. All construction activities shall occur within the limits of the silt fence as shown on the attached Erosion Control Plans. See Appendix B Drawings C-2A and C-2B for Erosion Control Plans.

### B. PHASE CONSTRUCTION ACTIVITY

The following phasing is one possible sequence of construction. The contractor, upon approval from the owner's on-site erosion control monitor, may divert from this sequence in order to accommodate specific situations that may occur once construction has commenced. Any changes shall be approved by the owner's on site erosion control monitor and conform to the DEQE's (D.E.P.) Erosion and Sedimentation Control Guidelines, August 1983 and USDA S.C.S. Erosion and Sediment Control in Site Development, Massachusetts Conservation Guide, September 1983 and all local municipal regulations.

### Phase I

Phase 1 erosion controls will be installed prior to initiating the major earthwork activity at the site. The following measures will be installed and maintained:

- Prior to any construction activity, silt fencing shall be installed at the limits of the work area as shown
  on the plans. The silt fence may be installed in stages, but must be in place prior to disturbance of soils
  within the area draining to the silt fence.
- Stabilized construction entrances shall be installed at the pavement limits as shown on the drawings. The construction entrance locations shall be adjusted as necessary as construction proceeds.
- Install filter bags on all existing catch basins within the construction area until the site is stabilzed.

• Phase 1 erosion controls must remain in place during clearing and grubbing activities and the preliminary cut and fill operation. Cuts and fills shall be performed in a manner such that runoff will continue to be directed toward erosion and sediment controls. Fill shall be placed in lifts sloping towards the control measures until it becomes practical and necessary to relocate them. As the excavated and filled surfaces reach subgrade, Phase 2 erosion control measures will be installed.

### Phase II

Phase 2 erosion controls shall consist of similar controls to Phase 1, but with new locations. The following measures shall be applied:

- All silt fence shall remain in place until the final stabilization of the site.
- As side slopes reach final subgrade, and where these slopes are outside the limits of paving or other structural surfacing, the slopes shall be topsoiled, seeded for permanent vegetative cover and mulched. All proposed slopes steeper than 3:1 shall be stabilized with erosion control matting and protected from erosion. Topsoil placement and seeding shall take place within 30 days of completion of subgrade at these locations, unless the time of year prevents application of permanent seed. In that case, the exposed slopes shall be mulched for winter protection, and if seasonal conditions permit, a temporary seed mix applied.

### Phase III

Phase 3 erosion controls comprise measures required to control erosion from surfaces that are near to final grade and are waiting final stabilization by pavement, permanent landscaping, or other surfacing. These measures shall include the following:

• Silt fence shall remain until the tributary drainage areas are stabilized.

### **General Measures During All Phases:**

In addition to the erosion controls listed for in Phases 1, 2, and 3, the following measures shall be employed throughout all phases:

- The contractor shall minimize the area of disturbed soil and efforts shall be made to limit the time of exposure of disturbed areas.
- Erosion control measures shall be routinely inspected and cleaned, repaired or replaced as necessary. The proponent will monitor the measures for proper maintenance and operation throughout the construction period will retain a professional environmental scientist or other qualified professional.
- Where construction activities have permanently ceased or have temporarily been suspended for more than seven days, or when final grades are reached in any portion of the site, stabilization practices shall be implemented within three days. Areas which remain disturbed but inactive for at least thirty days shall receive temporary seeding in accordance with the DEP Erosion and Sedimentation Control Guidelines, August 1983 and USDA S.C.S. Erosion and Sediment Control in Site Development, Massachusetts Conservation Guide, September 1983 and all local municipal regulations.
- Stockpiled soil materials shall be contained within staked haybales and/or silt fence.

• Any dewatering activities in which water will be released to a resource area or to a storm drain shall use a settling pond or similar device to remove sediment before water is released.

### **Structural Practices:**

Structural practices which will be used on this site to divert stormwater flows away from exposed soils, store stormwater runoff, and discharge stormwater from the site include but are not limited to; silt fences, stacked haybales, drainage swales, sediment traps, check dams, catch basins, drainage pipe, manholes, temporary sediment basins, outlet control structure, permanent seeding and landscaping treatments (including permanent mulches, as applicable), and structural surfaces such as pavements. The site work drawings detail and show locations of these structural practices.

### C. CONTROL STORMWATER FLOWING ONTO AND THROUGH THE PROJECT

BMP Description: Sedimenta	tion filter bag
Installation Schedule:	At commencement of construction activities
Maintenance and	Once weekly and within 24 hours of the end of a rainfall event
Inspection:	that is 0.5 inches or greater

### D. ESTABLISH PERIMETER CONTROLS AND SEDIMENT BARRIERS

BMP Description: Silt fence	
Installation Schedule:	Prior to any construction activity
Maintenance and	Once weekly and within 24 hours of the end of a rainfall event
Inspection:	that is 0.5 inches or greater

### E. STABILIZE SOILS

BMP Description: Mulch, I	hay or seeding for temporary vegetation of disturbed or exposed
areas	
Permanent	☐ Temporary
Installation Schedule:	As needed. No areas shall be left disturbed for longer than
	necessary to complete the work associated with that area.
Maintenance and	Once weekly and within 24 hours of the end of a rainfall event
Inspection:	that is 0.5 inches or greater

### F. PROTECT SLOPES

BMP Description: Erosion co	ontrol matting for slopes steeper than 3:1
Installation Schedule:	During construction activities associated with the slope
Maintenance and	Once weekly and within 24 hours of the end of a rainfall event
Inspection:	that is 0.5 inches or greater

### G. PROTECT STORM DRAIN INLETS

BMP Description: Sedimenta	ution filter bag
Installation Schedule:	At commencement of construction activities
Maintenance and	Once weekly and within 24 hours of the end of a rainfall event
Inspection:	that is 0.5 inches or greater

### H. RETAIN SEDIMENT ON-SITE

BMP Description: Sedimento	ution filter bag
Installation Schedule:	At commencement of construction activities
Maintenance and	Once weekly and within 24 hours of the end of a rainfall event
Inspection:	that is 0.5 inches or greater

### I. ESTABLISH STABILIZED CONSTRUCTION EXITS

BMP Description: Construction entrance vehicle tracking pads		
Installation Schedule:	Prior to the commencement of any earthwork operations	
Maintenance and	Once weekly and within 24 hours of the end of a rainfall event	
Inspection:	that is 0.5 inches or greater	

### III. GOOD HOUSEKEEPING BMPS

### A. MATERIAL HANDLING AND WASTE MANAGEMENT

BMP Description: Solid waste containers / dumpsters	
Installation Schedule:	At commencement of construction activities
Maintenance and	As required
Inspection:	

### B. ESTABLISH PROPER BUILDING MATERIAL STAGING AREAS

BMP Description: Silt fences and haybales at all stockpile areas of construction and ex	cavated
material	

Installation Schedule:	At the commencement of construction activities
Maintenance and	Once weekly and within 24 hours of the end of a rainfall event
Inspection:	that is 0.5 inches or greater

### C. DESIGNATE WASHOUT AREAS

BMP Description: Equipment	washing shall occur only within drainage areas with temporary
sedimentatio	on basins.

Installation Schedule:	At the commencement of construction activities
Maintenance and	Once weekly and within 24 hours of the end of a rainfall event
Inspection:	that is 0.5 inches or greater

# D. ESTABLISH PROPER EQUIPMENT/VEHICLE FUELING AND MAINTENANCE PRACTICES

BMP Description: Fueling operations, including the service and storage of equipment associated with fueling, shall occur a minimum of 100 feet from the edge of a resource area and within a drainage areas with temporary sedimentation basins.

Installation Schedule:	At the commencement of construction activities
Maintenance and	Once weekly and within 24 hours of the end of a rainfall event
Inspection:	that is 0.5 inches or greater

### E. CONTROL EQUIPMENT/VEHICLE WASHING

BMP Description: Vehicle washing shall occur	r only within drainage areas with temporary
sedimentation basins.	

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Installation Schedule:	At the commencement of construction activities
Maintenance and	Once weekly and within 24 hours of the end of a rainfall event
Inspection:	that is 0.5 inches or greater

### F. SPILL PREVENTION AND CONTROL PLAN

A spill contingency plan will be implemented during construction, including the following provisions:

- Equipment necessary to quickly attend to inadvertent spills or will be stored on-site in a secure but accessible location. Such equipment will include:
  - 1. safety goggles
  - 2. chemically resistant gloves and overshoe boots
  - 3. water and chemical fire extinguishers
  - 4. sand and shovels
  - 5. suitable absorbent materials
  - 6. storage containers
  - 7. first aid equipment
- Spills or leaks will be treated properly in accordance with material type, volume of spillage and location of the spill. Mitigation will include:
  - 1. preventing further spillage

- 2. containing the spilled material in the smallest practical area
- 3. removing spilled material immediately in a safe and environmentally sound manner
- 4. mitigating any damage to the environment
- For spills of less than 5 gallons of material, proceed with source control and containment and clean up with absorbent materials or other applicable means, unless an imminent hazard or other circumstances dictate that the spill should be treated by a professional response contractor.
- Spills of toxic or hazardous materials will be reported to the appropriate federal, state and/or local government agency, regardless of the size of the spill. Spills of amounts that exceed reportable quantities of certain substances specifically mentioned in federal regulations 40 CFR 110, 40 CFR 117 and 40 CFR 302 must be immediately reported to the EPA National Response Center, telephone 1-800-424-8802.

### G. ANY ADDITIONAL BMPS

BMP Description: Adequate sanitation facilities for on-site construction crews		
Installation Schedule:	on Schedule: At the commencement of construction activities	
Maintenance and	As required	
Inspection:		

BMP Description: Dust control through watering	
Installation Schedule:	As required throughout earthwork operations
Maintenance and	As required
Inspection:	

### H. ALLOWABLE NON-STORMWATER DISCHARGE MANAGEMENT

BMP Description: All measures used to mitigate sedimentation shall be used to control water associated with dust control activities

Installation Schedule:	As outlined in above measures
Maintenance and	Once weekly and within 24 hours of the end of a rainfall event
Inspection:	that is 0.5 inches or greater

# APPENDIX G: STORMWATER MANAGEMENT SYSTEM OPERATION AND MAINTENANCE PLAN

### STORMWATER MANAGEMENT SYSTEM (SMS) OPERATION AND MAINTENANCE PLAN

Applicant: Twenty Wayland, LLC

260 Boston Post Road, Suite 9

Wayland, MA 02109

Prepared by: R.J. O'Connell & Associates

80 Montvale Avenue Stoneham, MA

### A. SMS DESCRIPTION

The on-site drainage system, which collects and conveys storm water runoff from the parking lot consists of deep sump catch basins with oil/grease hoods on the outlets, drain manholes, closed drainage piping, water quality swales, rain gardens, bioretention basins and curbing along pavement edges.

### **B. OPERATION AND MAINTENANCE RESPONSIBILITY**

**During construction:** 

Site Contractor (Not Selected at this time)

Post construction:

Twenty Wayland, LLC

### C. INSPECTION AND MAINTENANCE SCHEDULE

### **Schedule During Construction:**

See Erosion Control Notes (below). These notes are also included on the site design plans. The NPDES general permit which is prepared prior to construction will also include schedule information for the inspection and maintenance of erosion controls during and immediately following construction.

### **EROSION CONTROL NOTES:**

- 1. ALL EROSION AND SEDIMENTATION CONTROL MEASURES SHALL BE CONSTRUCTED IN ACCORDANCE WITH D.E.Q.E.'S (DEP) EROSION AND SEDIMENTATION CONTROL GUIDELINES, AUGUST 1983, THE U.S.D.A. S.C.S. EROSION AND SEDIMENT CONTROL IN SITE DEVELOPMENT, MASSACHUSETTS CONSERVATION GUIDE, SEPTEMBER 1983 AND ALL LOCAL MUNICIPAL REGULATIONS.
- 2. EROSION AND SEDIMENTATION CONTROL MEASURES SHALL BE IN PLACE PRIOR TO THE COMMENCEMENT OF ANY SITE WORK OR EARTHWORK OPERATIONS,

- SHALL BE MAINTAINED DURING CONSTRUCTION, AND SHALL REMAIN IN PLACE UNTIL ALL SITE WORK IS COMPLETE AND GROUND COVER IS ESTABLISHED.
- 3. STOCKPILES SHALL BE SURROUNDED ON THEIR PERIMETERS WITH STAKED HAY BALES AND/OR SILTATION FENCES TO PREVENT AND/OR CONTROL SILTATION AND EROSION.
- 4. TOPS OF STOCKPILES SHALL BE COVERED IN SUCH A MANNER THAT STORMWATER DOES NOT INFILTRATE THE MATERIALS AND THEREBY RENDER THE SAME UNSUITABLE FOR FILL USE.
- 5. ALL DISTURBED OR EXPOSED AREAS SUBJECT TO EROSION SHALL BE STABILIZED WITH MULCH OR SEEDED FOR TEMPORARY VEGETATIVE COVER. WHERE CONSTRUCTION ACTIVITIES HAVE PERMANENTLY CEASED OR HAVE TEMPORARILY BEEN SUSPENDED FOR MORE THAN FOURTEEN DAYS, OR WHEN FINAL GRADES ARE REACHED IN ANY PORTION OF THE SITE, STABILIZATION PRACTICES SHALL BE IMPLEMENTED WITHIN THREE DAYS. AREAS WHICH REMAIN DISTURBED BUT INACTIVE FOR AT LEAST FOURTEEN DAYS SHALL RECEIVE TEMPORARILY SEEDING IN ACCORDANCE WITH MASSACHUSETTS DEP EROSION AND SEDIMENT CONTROL GUIDELINES. IN ALL CASES, STABILIZATION MEASURES SHALL BE IMPLEMENTED AS SOON AS POSSIBLE.
- 6. EARTHWORK ACTIVITY ON THE SITE SHALL BE DONE IN A MANNER SUCH THAT RUNOFF IS DIRECTED TO THE TEMPORARY DRAINAGE SWALES & SEDIMENT BASINS.
- 7. THE LOCATION OF TEMPORARY DRAINAGE SWALES AND SEDIMENTATION TRAPS SHALL BE REVISED AS REQUIRED AS CONSTRUCTION PROGRESSES
- 8. HAYBALES AND/OR FILTER BAGS SHALL BE PLACED AROUND CATCH BASINS AS REQUIRED DURING CONSTRUCTION.
- 9. ALL EROSION CONTROL MEASURES SHALL BE ROUTINELY INSPECTED OR A WEEKLY BASIS (ONCE EVERY SEVEN DAYS), CLEANED AND REPAIRED OR REPLACED AS NECESSARY THROUGHOUT ALL PHASES OF CONSTRUCTION. IN ADDITION, INSPECTION SHALL TAKE PLACE AFTER EACH RAINFALL EVENT. THE CONTRACTOR SHALL STRICTLY ADHERE TO THE STORMWATER POLLUTION PREVENTION PLAN (SWPPP) DURING CONSTRUCTION OPERATIONS.
- 10. ALL PROPOSED SLOPES (EXCLUDING RIP RAP SLOPES) STEEPER THAN 3H:1V SHALL BE STABILIZED WITH A CURLEX EROSION CONTROL MATTING BY AMERICAN EXCELSIOR COMPANY (OR EGINEER APPROVED EQUAL) PRIOR TO HYDROSEEDING AND PROTECTED FROM EROSION.
- 11. THE CONTRACTOR SHALL KEEP ON SITE AT ALL TIMES ADDITIONAL HAYBALES AND EXTRA SILTATION FENCING FOR INSTALLATION AT THE DIRECTION OF THE ENGINEER AND/OR CONSERVATION COMMISSION AGENT TO MITIGATE ANY EMERGENCY CONDITION.

- 12. THE CONTRACTOR IS RESPONSIBLE FOR OBTAINING AND PAYING FOR ANY PERMITS AND/OR CONNECTION FEES REQUIRED TO CARRY OUT THE WORK INCLUDING BUT NOT LIMITED TO DEMOLITION.
- 13. THE LIMIT OF WORK LINE FOR THE AREA TO BE CLEARED AND GRUBBED SHALL BE THE SAME AS THE LIMIT OF WORK LINE NECESSARY FOR GRADING PURPOSES, (I.E., THE GRADING LIMITS AROUND THE PERIMETER OF THE PROJECT AREA).
- 14. THE AREA OR AREAS OF ENTRANCE AND EXIT TO AND FROM THE SITE SHALL BE CLEARED OF ALL VEGETATION, ROOTS, AND OTHER OBJECTIONABLE MATERIAL AS DETERMINED BY THE ENGINEER OR OWNER'S REPRESENTATIVE.
- 15. THE AREA OR AREAS OF ENTRANCE AND EXIT TO AND FROM THE SITE SHALL BE MAINTAINED IN A CONDITION WHICH WILL PREVENT TRACKING OR FLOWING OF SEDIMENT ONTO PUBLIC RIGHT-OF-WAY. ALL SEDIMENT SPILLED, DROPPED, WASHED OR TRACKED ONTO PUBLIC RIGHT-OF-WAY MUST BE REMOVED IMMEDIATELY.
- 16. CATCH BASINS WHICH SERVE AS TEMPORARY SEDIMENT TRAPS MUST BE INSPECTED ON A WEEKLY BASIS AND AFTER EACH RAINFALL EVENT. SEDIMENT WILL BE REMOVED FROM EACH BASIN WHEN SEDIMENT HAS ACCUMULATED TO WITHIN 1' BELOW THE INVERT ELEVATION OF THE OUTFALL PIPE.
- 17. UPON COMPLETION OF ALL SITE WORK CONSTRUCTION SITE CONTRACTOR SHALL INSPECT ALL ON-SITE CATCH BASINS, DRAINAGE SWALES, FOREBAYS, & THE DETENTION POND AND REMOVE ALL SEDIMENT AND TRASH DEBRIS THAT HAS ACCUMULATED WITHIN EACH STRUCTURE DURING THE COURSE OF CONSTRUCTION.
- 18. ALL CONSTRUCTION SHALL MEET OR EXCEED THE TOWN OF WAYLAND'S ENGINEERING DEPARTMENT SPECIFICATIONS.
- 19. ALL SLOPES EXCEEDING FIFTEEN (15) PERCENT RESULTING FROM THE SITE GRADING SHALL BE EITHER COVERED WITH SIX (6) INCHES OF TOPSOIL AND PLANTED WITH A VEGETATIVE COVER SUFFICIENT TO PREVENT EROSION OR BE STABILIZED BY A RETAINING WALL.
- 20. DUST CONTROL SHALL BE USED DURING GRADING OPERATIONS. DUST CONTROL METHODS SHALL CONSIST OF DAMPENING THE GROUND WITH WATER. IF WATER DOES NOT PROVIDE ADEQUATE DUST CONTROL, AN EMULSION SOIL STABLIZER SHALL BE APPLIED TO SUSCEPTIBLE SOILS.
- 21. THE CONTRACTOR SHALL BE AWARE THAT SOIL, GRADES AND WETLANDS PROXIMITY AT THIS SITE MAKE IT PARTICULARLY SUSCEPTIBLE TO SOIL EROSION AND SENSITIVE TO IT'S CONSEQUENCES. IT SHOULD BE NOTED THAT THE EROSION CONTROL MEASURES AS SHOWN ON THE DRAWINGS DEPICT THE MINIMUM REQUIRED CONTROL AND ARE REPRESENTATIVE OF A SINGLE STAGE OF CONSTRUCTION FOR EACH PHASE. THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE SITING, RELOCATION AND AUGMENTATION OF EROSION CONTROL DEVICES AS THE PROJECT PROGRESSES AND SITE DRAINAGE CONDITIONS CHANGE.

- 22. THE CONTRACTOR SHALL ANTICIPATE AND MODIFY EROSION CONTROL MEASURES BASED ON PAST AND CURRENT WEATHER CONDITIONS, SEASON AND EXPECTED FUTURE CONSTRUCTION ACTIVITIES.
- 23. THE CONTRACTOR SHALL MINIMIZE THE AREA OF DISTURBED SOIL. EFFORTS SHALL BE MADE TO LIMIT THE TIME OF EXPOSURE OF DISTURBED AREAS.
- 24. THE CONTRACTOR SHALL AT HIS EXPENSE SURVEY AND MARK OUT IN THE FIELD THE LIMITS OF CLEARING (I.E. HAYBALE/SILTFENCE LINE) AND THE WETLAND BUFFER BOUNDARY FOR APPROVAL BY THE TOWN PRIOR TO COMMENCEMENT OF CLEARING AND GRUBBING ACTIVITIES.
- 25. THE CONTRACTOR SHALL NOTIFY THE TOWN'S PLANNING STAFF AND CONSERVATION AGENT AT LEAST 48 HOURS PRIOR TO COMMENCEMENT OF SITEWORK.
- 26. PRIOR TO COMMENCEMENT OF CONSTRUCTION ACTIVITIES AT THE SITE, THE CONTRACTOR SHALL ENGAGE AN INDIVIDUAL WITH SPECIFIC PROFESSIONAL TRAINING AND EXPERTISE IN EROSION AND SEDIMENT CONTROL. THE EROSION CONTROL MONITOR SHALL PREPARE A WEEKLY REPORT WHICH SHALL BE KEPT ON SITE AT ALL TIMES AND SHALL BE SHOWN TO LOCAL, STATE AND FEDERAL AGENTS UPON REQUEST. THIS REPORT SHALL INDICATE THE STATUS OF THE EROSION CONTROLS AND ANY MAINTENANCE REQUIRED AND PERFORMED. THIS REPORT SHALL CONFORM TO THE REQUIREMENTS OF THE EPA'S NATIONAL POLLUTANT DISCHARGE ELIMINATION SYSTEM (NPDES) PERMIT.
- 27. HAYBALE DIKES SHALL BE CONSTRUCTED AT ALL EXISTING & PROPOSED CATCH BASINS LOCATED IN FILL AREAS & SUBJECT TO STORMWATER RUN-OFF FROM PROPOSED FILL AREAS DURING CONSTRUCTION, OR AS DIRECTED BY THE OWNER/ENGINEER. NO SEDIMENTS SHALL ENTER THE ON-SITE DRAINAGE SYSTEM AT ANY TIME.
- 28. THE FOREBAY BASINS SHALL BE USED AS SEDIMENTATION BASINS THROUGHOUT CONSTRUCTION AND SHALL BE PERIODICALLY CLEANED DURING CONSTRUCTION, AND AT THE COMPLETION OF CONSTRUCTION. ALL TEMPORARY SWALES SHALL BE DIRECTED TO THE FOREBAY LOCATION WHEN POSSIBLE.
- 29. THE LOCATION OF HAYBALE CHECK DAMS SHALL BE FIELD VERIFIED DURING SITE PREPARATION OPERATIONS BY THE CONTRACTOR.
- 30. UPON COMPLETION OF ALL SITE WORK CONSTRUCTION SITE CONTRACTOR SHALL INSPECT ALL ON-SITE CATCH BASINS, DRAINAGE SWALES, FOREBAYS, & THE DETENTION POND AND REMOVE ALL SEDIMENT AND TRASH DEBRIS THAT HAS ACCUMULATED WITHIN EACH STRUCTURE DURING THE COURSE OF CONSTRUCTION.

### Post Construction Schedule

- 1. A checklist of all maintenance items will be developed and used for each stormwater treatment component. Each time an inspection is completed or a maintenance procedure is performed, it will be documented on the checklist. The checklist will be kept on the project site.
- 2. The property owner will be financially responsible for the implementation of this plan and for future system repairs as needed.
- 3. Sweep parking lot and driveway areas to remove sediments before they can enter the stormwater management system, twice annually, in the early spring and late fall, and on an as needed basis at other times.
- 4. Inspect and clean deep sump catch basins including the oil/grease traps to prevent blockage and to remove accumulated sediments on an annual basis in the spring and in general if the depth of accumulated sediment is greater than one-half the depth of the sump.
- 5. Inspect and clean water quality swales and rain gardens an annual basis in the spring and on an as needed basis at other times.
- 6. Inspect and clean bioretention basins an annual basis in the spring and on an as needed basis at other times.
- 7. Inspect dumpster and compactor areas for spillage and clean as necessary.
- 8. Inspect landscape areas and edges of paved areas for any signs of erosion. Perform any necessary curb replacement, earth repair, reseeding or mulching upon identification.
- 9. Routinely pick up and remove litter from the parking areas and perimeter landscape areas. Clean leaves or trash from catch basin grates when observed.